NI 43-101 Technical Report

Iberian Belt West Project, Spain

Emerita Resources Corp

Prepared by:

SLR Consulting Limited

SLR Project No.: 415.065290.00001

Effective Date:

October 8, 2026

Signature Date:

October 14, 2026

Revision: 1

Qualified Persons:
Frank Browning, MSc, FGS, CGeol
James W.G. Turner, MCSM, MIMMM, CEng
Christopher Penna, CEng
Liam Johnson, RPEQ, MAusIMM CP (Geotech)
Christopher Paul Stinton, CEng IMMM
Arturo Gutierrez del Olmo, PhD. (Mining), Eur Ing, MIMMM
Alison Brianna Allen, BSc, MSc, CEnv, FIMMM, MISEP
Veronika Luneva, MAussIMM, MSc, IMC (CFA UK Level 4)

NI 43-101 Technical Report for the Iberian Belt West Project, Spain

SLR Project No.: 415.065290.00001

Prepared by

SLR Consulting Limited

3rd Floor, Summit House, 12 Red Lion Square

London, UK WC1R 4QH

for

Emerita Resources Corp

301-217 Queen Street West

Toronto

Ontario

M5V OR 2

Effective Date – October 8, 2026

Signature Date – October 14, 2026

Prepared by:
Frank Browning, MSc, FGS, CGeol
James W.G. Turner, MCSM, MIMMM, CEng
Christopher Penna, CEng
Liam Johnson, RPEQ, MAusIMM CP (Geotech)
Christopher Paul Stinton, CEng IMMM
Arturo Gutierrez del Olmo, PhD. (Mining), Eur Ing, MIMMM
Alison Brianna Allen, BSc, MSc, CEnv, FIMMM, MISEP
Veronika Luneva, MAussIMM, MSc, IMC (CFA UK Level 4)

Approved by:

Project Manager
Nicky Vlok, MPM.

Project Director
Bryan Pullman, P.Eng.

Peer Reviewed by:
Alan Clarke, CGeol.
Bryan Pullman, P.Eng.
Frank Palkovits P.Eng
Huw Edmunds CGeol

Revision Record

Revision	Date	Prepared by	Checked by	Authorized by
A	October 9, 2026	Nicky Vlok	Rebecca Parcell	Bryan Pullman
0	October 14, 2026	Nicky Vlok	Rebecca Parcell	Bryan Pullman
1	October 27, 2026	Nicky Vlok	Rebecca Parcell	Bryan Pullman

Table of Contents

1.0 Summary 1-1
1.1 Executive Summary 1-1
1.2 Economic Analysis 1-15
1.3 Technical Summary 1-16
2.0 Introduction 2-1
2.1 Sources of Information 2-1
2.2 Acknowledgements 2-3
2.3 List of Abbreviations 2-4
3.0 Reliance on Other Experts 3-1
4.0 Property Description and Location 4-1
4.1 Location 4-1
4.2 Ownership 4-4
4.3 Mineral Tenure 4-4
4.4 Royalties 4-7
4.5 Surface Rights 4-7
4.6 Permitting Considerations 4-7
4.7 Environmental Considerations 4-8
4.8 Existing Environmental Liabilities 4-10
5.0 Accessibility, Climate, Local Resources, Infrastructure and Physiography 5-1
5.1 Accessibility 5-1
5.2 Climate 5-1
5.3 Local Resources and Infrastructure 5-3
5.4 Physiography 5-4
6.0 History 6-1
6.1 Prior Ownership 6-1
6.2 Exploration History 6-2
6.3 Historical Resource Estimates 6-6
6.4 Production History 6-6
7.0 Geological Setting and Mineralisation 7-1
7.1 Regional Geology 7-1
7.2 Local Geology 7-4
7.3 Property Geology 7-9
7.4 Mineralisation 7-19

8.0 Deposit Types 8-1
9.0 Exploration 9-1
9.1 Introduction 9-1
9.2 Geological Mapping 9-1
9.3 Soil Chemistry 9-1
9.4 Soil Vapour Geochemistry 9-4
9.5 Geophysics 9-6
10.0 Drilling 10-1
10.1 Historical Drilling (Prior to 2021) 10-1
10.2 Emerita Drilling (2021 to Present) 10-1
10.3 Drilling Procedures 10-10
10.4 Interpretation of Relevant Results 10-13
11.0 Sample Preparation, Analyses, and Security 11-1
11.1 Sampling Methods 11-1
11.2 Bulk Density 11-3
11.3 Sample Security 11-5
11.4 Laboratories 11-6
11.5 Sample Preparation and Analysis 11-6
11.6 QA/QC Protocol 11-10
11.7 QA/QC Results 11-12
11.8 Adequacy of Procedures 11-28
12.0 Data Verification 12-1
12.1 Data Verification by Emerita 12-1
12.2 Database Cut-Off Dates 12-1
12.3 Data Verification by the QP 12-1
13.0 Mineral Processing and Metallurgical Testing 13-1
13.1 Introduction 13-1
13.2 Phase I Testwork 13-1
13.3 Phase II Testwork 13-7
13.4 Metallurgical Testwork Summary 13-20
14.0 Mineral Resource Estimates 14-1
14.1 Introduction 14-1
14.2 Mineral Resource Estimate Data 14-1
14.3 Geological Interpretation and Domaining 14-2

14.4 Boundary Analysis 14-12
14.5 Compositing 14-13
14.6 Grade Capping 14-14
14.7 Metal Correlations 14-19
14.8 Variography 14-20
14.9 Block Modelling 14-26
14.10 Estimation Methodology 14-26
14.11 Model Validation 14-32
14.12 Mineral Resource Classification 14-44
14.13 Reasonable Prospects for Eventual Economic Extraction 14-44
14.14 Mineral Resource Reporting 14-49
14.15 Comparison with Previous Mineral Resource Estimate 14-51
15.0 Mineral Reserve Estimates 15-1
15.1 Summary 15-1
15.2 Resource Model 15-3
15.3 Dilution 15-3
15.4 Extraction 15-4
15.5 Cut-off Value 15-4
16.0 Mining Methods 16-1
16.1 Introduction 16-1
16.2 Geotechnical Studies 16-1
16.3 Hydrogeological Considerations 16-6
16.4 Mine Design 16-10
16.5 Life of Mine Plan 16-31
16.6 Mine Backfill 16-41
16.7 Mine Infrastructure 16-43
16.8 Mine Equipment 16-54
16.9 Mine Personnel 16-56
17.0 Recovery Methods 17-1
17.1 Process Description 17-1
17.2 Process Flowsheet 17-1
17.3 Key Process Design Criteria 17-4
17.4 Plant Description 17-6
17.5 Reagents 17-16

17.6 Key Process Reagents 17-16
17.7 Tailings Dewatering Area 17-17
17.8 Utilities - Processing and Surface Infrastructure 17-17
17.9 Sampling Protocol 17-20
17.10 Process Control 17-20
18.0 Project Infrastructure 18-1
18.2 Power Infrastructure 18-3
18.3 Water Management 18-6
18.4 Process Plant Infrastructure 18-7
18.5 Tailings and Waste Management 18-7
18.6 Building and Site Facilities 18-9
18.7 Workforce Accommodation 18-10
18.8 Fuel and Utilities 18-10
19.0 Market Studies and Contracts 19-1
19.1 Zinc Market Studies and Contracts 19-1
19.2 Lead Concentrate 19-3
19.3 Copper Concentrate 19-4
19.4 Pyrite Concentrate 19-6
19.5 Commodity Prices Selected for the Economic Analysis 19-8
19.6 Conclusion 19-9
20.0 Environmental, Permitting and Social Impact 20-1
20.1 Project Status 20-1
20.2 Environmental and Social Setting and Risks 20-9
20.3 Environmental and Social Management 20-29
20.4 Future Work (Environmental and Social Roadmap) 20-39
21.0 Capital and Operating Costs 21-1
21.1 Capital Costs 21-1
21.2 Operating Costs 21-11
22.0 Economic Analysis 22-1
22.1 Forward-Looking Information 22-1
22.2 Financial Model Parameters 22-1
22.3 Cash Flow Analysis 22-9
22.4 Sensitivity Analysis 22-16
23.0 Adjacent Properties 23-1

24.0 Other Relevant Data and Information 24-1
24.1 Post-Flotation Process (PFP) 24-1
25.0 Interpretation and Conclusions 25-1
25.1 Geology and Mineral Resources 25-1
25.2 Mining and Mineral Reserves 25-2
25.3 Mineral Processing 25-3
25.4 Infrastructure 25-3
25.5 Environment 25-4
25.6 Capital and Operating Costs 25-4
25.7 Risks 25-6
26.0 Recommendations 26-1
26.1 Geology and Mineral Resources 26-1
26.2 Mining and Mineral Reserves 26-1
26.3 Mineral Processing 26-3
26.4 Infrastructure 26-3
26.5 Environment 26-5
26.6 Capital and Operating Costs 26-6
27.0 References 27-1
28.0 Date and Signature Date 28-1
29.0 Certificate of Qualified Person 29-1
29.1 Frank Browning 29-1
29.2 James W.G. Turner 29-2
29.3 Christopher Penna 29-3
29.4 Liam Johnson 29-4
29.5 Christopher Paul Stinton 29-5
29.6 Arturo Gutierrez del Olmo 29-6
29.7 Alison Brianna Allen 29-8
29.8 Veronika Luneva 29-10

Tables

Table 1-1: Life-of-Mine Capital Cost Summary 1-5
Table 1-2: OPEX by cost category 1-6
Table 1-3: Life-of-Mine Unit Operating Costs (Year 1 – Year 21) 1-7
Table 1-4: Summary of Mineral Resources – July 17, 2026 1-19
Table 1-5: Summary of Mineral Reserves –July 17, 2026 1-21
Table 1-6: Base Metal Price Assumptions Used in the PFS Financial Model (US$/t). 1-24
Table 1-7: Pyrite Concentrate Price Assumptions Used in the PFS Financial Model 1-24
Table 2-1: Qualified Persons and Responsibilities 2-2
Table 2-2: Abbreviations for Units 2-4
Table 2-3: Abbreviations for Acronyms 2-5
Table 4-1: IBW Project Exploration Permit Details 4-4
Table 4-2: IBW Project Exploration Permit Coordinates (ETRS89 Zone 29N) 4-5
Table 6-1: Ownership History of the La Romanera Deposit 6-1
Table 6-2: Ownership History of the La Infanta Deposit 6-1
Table 6-3: Ownership History of the El Cura Deposit 6-2
Table 6-4: Historical Drillhole Databases 6-2
Table 6-5: Historical Mineral Resource Estimates 6-6
Table 7-1: La Romanera – Major Lithostratigraphic Units 7-12
Table 7-2: La Infanta – Major Lithostratigraphic Units 7-15
Table 7-3: El Cura – Major Lithostratigraphic Units 7-18
Table 10-1: Emerita Diamond Drilling by Year and in Total at Each Deposit (MRE Databases) 10-1
Table 10-2: Summary of Downhole Survey Tools 10-11
Table 11-1: Sample Length Depending on Core Diameter 11-1
Table 11-2: Summary Statistics for Density Reanalysis Results 11-4
Table 11-3: Summary Statistics for Density Reanalysis Results By Lithology 11-4
Table 11-4: Analytical Laboratories 11-6
Table 11-5: ALS Sevilla Sample Preparation Procedures 11-6
Table 11-6: Elements and Ranges of Analysis for the ME-ICPORE Method from ALS Global 11-7
Table 11-7: Gold Analysis Range for the Au-AA23 and Au-GRA21 Methods from ALS Global 11-7
Table 11-8: Elements and Range of Analysis for the ME-MS61L Method from ALS Global. 11-8

Table 11-9: AGQ Sample Preparation Procedures 11-8
Table 11-10: Elements and Range of Analysis for the PE-4042 Method from AGQ 11-9
Table 11-11: Elements and Range of Analysis for the PE-4043 Method from AGQ 11-9
Table 11-12: Gold Analysis for the PE-4014 Method from AGQ 11-10
Table 11-13: Certified Mean Value and Standard Deviation of Emerita CRMs 11-10
Table 11-14: Emerita Quality Control Rules 11-11
Table 11-15: Summary of La Romanera Samples Analysed by ALS 11-12
Table 11-16: Summary of La Romanera CRM Submissions to ALS 11-13
Table 11-17: Summary Statistics for La Romanera Field Duplicate Submissions to ALS .. 11-16
Table 11-18: Summary Statistics for La Romanera Pulp Duplicate Submissions to ALS ... 11-16
Table 11-19: Summary of La Romanera Blank Submissions to ALS 11-18
Table 11-20: Summary of La Infanta Samples Analysed by ALS 11-18
Table 11-21: Summary of La Infanta CRM Submissions to ALS 11-19
Table 11-22: Summary Statistics for La Infanta Field Duplicate Submissions to ALS 11-21
Table 11-23: Summary Statistics for La Infanta Pulp Duplicate Submissions to ALS 11-21
Table 11-24: Summary of La Infanta Blank Submissions to ALS 11-23
Table 11-25: Summary of El Cura Samples Analysed by ALS 11-23
Table 11-26: Summary of El Cura CRM Submissions to ALS 11-24
Table 11-27: Summary Statistics for El Cura Field Duplicate Submissions to ALS 11-26
Table 11-28: Summary Statistics for El Cura Pulp Duplicate Submissions to ALS 11-27
Table 11-29: Summary of El Cura Blank Submissions to ALS 11-28
Table 13-1: Phase I Sample Details 13-2
Table 13-2: Phase I Head Assays 13-5
Table 13-3: SMC Test Results 13-5
Table 13-4: Bond Abrasion Index Test Results 13-6
Table 13-5: Bond Ball Mill Work Index (BWi) Test Results 13-6
Table 13-6: La Romanera MET-1 LCT Result 13-6
Table 13-7: La Romanera MET-2 LCT Result 13-7
Table 13-8: La Romanera MET-3 LCT Result 13-7
Table 13-9: La Infanta MET-4 LCT Result 13-7
Table 13-10: Phase II Sample Details 13-9
Table 13-11: Phase II Head Assays 13-12
Table 13-12: SMC Results – El Cura 13-13
Table 13-13: Bond Abrasion (Ai) Results – El Cura 13-13

Table 13-14: Bond Ball Mill Work Index (BWi) Results – El Cura 13-13
Table 13-15: La Romanera MET-6 Locked Cycle Test Results 13-15
Table 13-16: La Infanta MET-7 Locked Cycle Test Results 13-15
Table 13-17: El Cura MET-9 Locked Cycle Test Results 13-15
Table 13-18: La Romanera/La Infanta MET-8 Locked Cycle Test Results 13-15
Table 13-19: Penalty Elements in LCT Final Concentrates 13-16
Table 13-20: Final Tails Pyrite Flotation Test Results 13-19
Table 13-21: Metallurgical Balance 13-22
Table 14-1: Summary of MRE Drillhole Databases 14-1
Table 14-2: Sulphur-Density Regressions per Deposit 14-14
Table 14-3: La Romanera Composite Capping Statistics by Domain 14-15
Table 14-4: La Infanta Composite Capping Statistics by Domain 14-17
Table 14-5: El Cura Composite Capping Statistics by Domain 14-18
Table 14-6: Correlation Matrix for Metals and Density for La Romanera 14-19
Table 14-7: Correlation Matrix for Metals and Density for La Infanta 14-19
Table 14-8: Correlation Matrix for Metals and Density for El Cura 14-19
Table 14-9: La Romanera Variogram Model Parameters 14-24
Table 14-10: La Infanta Variogram Model Parameters 14-25
Table 14-11: El Cura Variogram Model Parameters 14-25
Table 14-12: Block Model Parameters 14-26
Table 14-13: La Romanera Grade Estimation Parameters 14-27
Table 14-14: La Infanta Grade Estimation Parameters 14-29
Table 14-15: El Cura Grade Estimation Parameters 14-31
Table 14-16: La Romanera Mean Grade Comparison by Domain 14-39
Table 14-17: La Infanta Mean Grade Comparison by Domain 14-39
Table 14-18: El Cura Mean Grade Comparison by Domain 14-39
Table 14-19: Mineral Resource Estimate Technical and Economic Parameters 14-45
Table 14-20: Summary of Mineral Resources – July 17, 2026 14-50
Table 14-21: Percentage Change from the Previous IBW Project Mineral Resources 14-52
Table 15-1: Summary of Mineral Reserves – July 17, 2026 15-2
Table 15-2: Stope Dilution Summary 15-4
Table 15-3: Operating Costs Used to Define Break-Even Cut-Off Values 15-4
Table 15-4: Mineral Reserve Estimate Technical and Economic Parameters Used for NSR Calculation 15-5
Table 16-1: Q' Values from Geotechnical Logging of Core Photographs 16-2

Table 16-2: Selected DSO Parameters 16-3
Table 16-3: Summary of Crown Pillar Thickness and Probability of Failure 16-5
Table 16-4: Underground LOM Lateral Development Summary 16-19
Table 16-5: Raise Bore Vertical Development Summary 16-22
Table 16-6: DSO Inputs for Underground Stope Delineation 16-23
Table 16-7: DSO Stope Inventory Tonnage Summary 16-28
Table 16-8: Drill-and-Blast Design Parameters 16-30
Table 16-9: Stope Dilution and Mining Recovery Summary 16-31
Table 16-10: LOM Development Scheduled Metres Split by Cost Centre 16-33
Table 16-11: Stope Productivity Analysis Input Assumptions 16-35
Table 16-12: LOM Stope Production Summary (Diluted and Recovered Tonnes) 16-38
Table 16-13: LOM Global Production Summary (Diluted and Recovered Tonnes) 16-39
Table 16-14: Primary Fan Duties 16-48
Table 16-15: Operating Metrics for Major Equipment Used in Fleet Estimation 16-55
Table 17-1: Key Process Design Criteria 17-4
Table 17-2: Average Head Grades for La Romanera, La Infanta, and El Cura 17-5
Table 17-3: Concentrate Recoveries and Grades 17-5
Table 17-4: Summary of Main Crushing Criteria 17-9
Table 17-5: Summary of Main Milling Criteria 17-11
Table 17-6: Summary of Main Flotation Criteria 17-11
Table 17-7: Summary of Main Concentrate Dewatering Criteria 17-14
Table 17-8: Key Process Reagents 17-16
Table 17-9: Installed Power and Annual Power Consumption – Processing and Surface Infrastructure 17-18
Table 17-10: Plant Distribution Voltage 17-18
Table 18-1: Additional Traffic due to Product Shipment 18-3
Table 18-2: Power Requirements by Area for the Project 18-5
Table 19-1: SLR Zinc Pricing for PFS Financial Model 19-2
Table 19-2: SLR Lead Pricing for PFS Financial Model 19-3
Table 19-3: SLR Copper Pricing for PFS Financial Model 19-5
Table 19-4: SLR Sulphur Concentrate Pricing for PFS Financial Model 19-7
Table 19-5: Commodity Price Assumptions for the Economic Analysis 19-9
Table 20-1: Applicable National E&S Requirements 20-3
Table 20-2: GIIP International Standards 20-4
Table 20-3: E&S Studies Undertaken to Date 20-8

Table 20-4: Baseline Noise Levels (24-hour) 20-11
Table 20-5: Noise Level Guidelines (dBA) 20-14
Table 20-6: Communities Located Proximally to the Project 20-22
Table 20-7: Interviewed Stakeholders as part of the Karungen Study 20-24
Table 20-8: Human Rights Challenges 20-26
Table 20-9: Progressive Rehabilitation and Closure Activities 20-36
Table 20-10: Activities Included in Project AROs 20-38
Table 21-1: Project Capital Cost Summary 21-2
Table 21-2: Mining Capital Cost Summary by Deposit and Cost Category 21-5
Table 21-3: Processing Capital Cost Summary by Major Cost Category 21-6
Table 21-4: Tailings, Waste, and Water Management Capital Cost Summary 21-8
Table 21-5: Off-Site Infrastructure Capital Cost Summary 21-8
Table 21-6: Indirect Costs and EPCM Summary 21-9
Table 21-7: Summary of Closure and Rehabilitation Cost Estimate 21-10
Table 21-8: Progressive Rehabilitation and Closure Cost Schedule 21-11
Table 21-9: Life-of-Mine Operating Costs 21-12
Table 21-10: Benchmark Treatment and Refining Charges Adopted in the Financial Model 21-14
Table 21-11: Summary of Deleterious Element Penalty Assumptions Applied in the Economic Analysis 21-15
Table 21-12: Life-of-Mine Unit Operating Costs (Year 1 – Year 21) 21-16
Table 22-1: Project Timeline 22-1
Table 22-2: Summary of Concentrate Production, Grades, and Metallurgical Recoveries 22-3
Table 22-3: Long-Term Pyrite Concentrate Price Assumptions 22-4
Table 22-4: Long-Term Metal Price Assumptions 22-4
Table 22-5: Summary of Concentrate Payability Assumptions Applied in the Financial Model 22-5
Table 22-6: Life-of-Mine Capital Cost Summary 22-7
Table 22-7: Life-of-Mine On-site Operating Cost Summary 22-8
Table 22-8: Life-of-Mine Off-site and Commercial Cost Summary 22-9
Table 22-9: Summary of Base Case Economic Results 22-10
Table 22-10: After-Tax Cash Flow Summary 22-12
Table 22-11: Project Sensitivity to the Pyrite Concentrate Prices 22-17
Table 22-12: Project Sensitivity to Metal Prices (keeping Pyrite at Consensus Price level) 22-18
Table 22-13: After-Tax Sensitivity Analyses 22-20

Figures

Figure 4-1: Map of Spain Highlighting the Huelva Province of Andalusia 4-2
Figure 4-2: Location of the IBW Project Within Huelva Province 4-3
Figure 4-3: Project Exploration Permit Map (ETRS89 Zone 29N) 4-6
Figure 4-4: Environmentally Protected Areas 4-9
Figure 4-5: Historical Surface Workings at La Romanera 4-10
Figure 5-1: IBW Project Access Map 5-2
Figure 5-2: IBW Project Infrastructure Map, Permit Area, and Proposed Mine Facilities 5-5
Figure 6-1: La Romanera Historical Drilling 6-3
Figure 6-2: La Infanta Historical Drilling 6-4
Figure 6-3: El Cura Historical Drilling 6-5
Figure 7-1: Schematic Section of the Suture Zone Between the SPT and OMZ 7-1
Figure 7-2: Regional Geological Map 7-2
Figure 7-3: General Stratigraphic Column of the Iberian Pyrite Belt 7-3
Figure 7-4: Local Geological Map 7-5
Figure 7-5: Relationship between Deposit Scale Lithostratigraphic Columns and IBW Project Geological Model Chronology 7-6
Figure 7-6: Plan View of the Structural Framework and Lithology Model 7-7
Figure 7-7: 3D View of the Geological Model 7-8
Figure 7-8: 3D View of the La Romanera Geological Model 7-10
Figure 7-9: Example La Romanera Geological Model Cross-section 7-11
Figure 7-10: 3D View of the La Infanta Geological Model 7-13
Figure 7-11: Example La Infanta Geological Model Cross-section 7-14
Figure 7-12: 3D View of the El Cura Geological Model 7-16
Figure 7-13: Example El Cura Geological Model Cross-section 7-17
Figure 7-14: Examples of La Romanera Upper and Lower Lens Massive Sulphide Mineralisation (LR003) 7-19
Figure 7-15: Examples of La Infanta Sulphide Mineralisation 7-20
Figure 7-16: Examples of La Infanta Sulphide Mineralisation (EC014 and EC022) 7-21
Figure 8-1: Schematic Diagram of a Siliciclastic Felsic VMS Deposit 8-1
Figure 8-2: Stages of IPB VMS Mineralisation 8-2
Figure 9-1: Soil Geochemical Sample Data for Select Elements 9-2
Figure 9-2: Comparison of Rubidium in Soil versus Geological Map for the La Romanera Area 9-3
Figure 9-3: Soil Vapour Mercury Anomalies 9-5

Figure 9-4: Bouguer Anomaly Map from Historical Survey Data 9-7
Figure 9-5: Total Magnetic Intensity Map from Historical Survey Data 9-8
Figure 9-6: Enhanced Residual Bouguer Gravity Map from Emerita Survey Data 9-10
Figure 9-7: Surface TEM and Gravimetric Anomalies 9-11
Figure 9-8: Helicopter Transient Electromagetics Early Channel Conductivity 9-13
Figure 9-9: Total Magnetic Intensity Map from Emerita Survey Data 9-14
Figure 9-10: La Romanera Chargeability Pseudosections and Interpreted Trends 9-16
Figure 9-11: La Infanta Chargeability Pseudosections and Interpreted Trends 9-17
Figure 10-1: Monthly Drilling Statistics (2021-2025) 10-2
Figure 10-2: La Romanera Drill Plan 10-4
Figure 10-3: Representative La Romanera Drill Section 10-5
Figure 10-4: La Infanta Drill Plan 10-6
Figure 10-5: Representative La Infanta Drill Section 10-7
Figure 10-6: El Cura Drill Plan 10-8
Figure 10-7: Representative El Cura Drill Section 10-9
Figure 10-8: Diamond Drilling Operations at La Romanera 10-10
Figure 10-9: GyroLogic SPT Downhole Survey Tool and Optical Depth Counter 10-11
Figure 10-10: Emerita Core Processing Facility 10-12
Figure 10-11: Procedure for Measuring and Calculating RQD 10-13
Figure 11-1: Soil Sampling Process 11-2
Figure 11-2: Olympus Vanta pXRF 11-2
Figure 11-3: U.S. Solid USS-DBS28-30 Balance Taking a Wet Weight for Bulk Density Calculation 11-3
Figure 11-4: Scatter Plots for Density Reanalysis Results (Coloured by Lithology) 11-5
Figure 11-5: Example CRM Control Charts for OREAS 620 (La Romanera - ALS) 11-14
Figure 11-6: Example Internal Laboratory CRM Control Charts for Sulphur (La Romanera - ALS) 11-15
Figure 11-7: Example Duplicate Scatter Plots for Zinc (La Romanera - ALS) 11-17
Figure 11-8: Example CRM Control Charts for OREAS 623 (La Infanta - ALS) 11-20
Figure 11-9: Example Duplicate Scatter Plots for Zinc (La Infanta - ALS) 11-22
Figure 11-10: Example CRM Control Charts for OREAS 620 (El Cura - ALS) 11-25
Figure 11-11: Example Internal Laboratory CRM Control Charts for Sulphur (El Cura - ALS). 11-26
Figure 11-12: Example Duplicate Scatter Plots for Copper (El Cura - ALS) 11-27
Figure 13-1: La Romanera – Phase I Sample Locations 13-3

Figure 13-2: La Infanta – Phase I Sample Locations 13-4
Figure 13-3: La Romanera – Phase II Sample Locations 13-10
Figure 13-4: La Infanta – Phase II Sample Locations 13-11
Figure 13-5: El Cura – Phase II Sample Locations 13-12
Figure 13-6: Phase II LCT Testwork Flowsheet 13-14
Figure 14-1: Example of Interval Selection (IS_Romanera) Using Leapfrog Drillhole Correlation Tool 14-3
Figure 14-2: La Romanera Cross-section: Mineralisation Domains vs. Lithology (Left) and Assay NSR Value (Right) 14-4
Figure 14-3: 3D View of La Romanera Mineralisation Domains and Input Interval Selections (Excluding LG Envelopes) 14-5
Figure 14-4: La Infanta Cross-section: Mineralisation Domains vs. Lithology (Left) and Assay NSR Value (Right) 14-6
Figure 14-5: 3D View of La Infanta Domain Wireframes and Input Interval Selections (Excluding LG Envelopes) 14-7
Figure 14-6: El Cura Cross-section: Mineralisation Domains vs. Lithology (Left) and Assay NSR Value (Right) 14-8
Figure 14-7: 3D View of El Cura Domain Wireframes and Input Interval Selections (Excluding LG Envelope) 14-9
Figure 14-8: La Romanera Density Sample Histograms 14-10
Figure 14-9: La Romanera Cross-section: Mineralisation Style Domains vs. Lithology (Left) and Sulphur (Right) 14-11
Figure 14-10: La Romanera Cu-Zn Sample Scatter Plots Coloured by Mineralisation Style (Left) and Ag Grade (Right) 14-12
Figure 14-11: Zn Boundary Analysis for the La Romanera Lower Lens 14-13
Figure 14-12: Sulphur Density Scatter Plot and Regression (Red Line and Equation) for La Romanera 14-14
Figure 14-13: La Romanera - Zn Normal Score Down-Dip Continuity Maps and Directional Variograms 14-21
Figure 14-14: La Infanta – Zn Normal Score Down-Dip Continuity Maps and Directional Variograms 14-22
Figure 14-15: El Cura – Cu Normal Score Down-Dip Continuity Maps and Directional Variograms 14-23
Figure 14-16: La Romanera Cross Section - Zn Estimate vs. Composite Grades 14-33
Figure 14-17: La Romanera Long Sections - Zn Estimate vs. Full Domain Width Composite Grades (Excluding LG Envelopes) 14-34
Figure 14-18: La Infanta Cross Section - Zn Estimate vs. Composite Grades 14-35
Figure 14-19: La Infanta Long Sections - Zn Estimate vs. Full Domain Width Composite Grades (Excluding LG Envelopes) 14-36

Figure 14-20: El Cura Cross-section - Cu Estimate vs. Composite Grades 14-37
Figure 14-21: El Cura Long Section - Cu Estimate vs. Full Domain Width Composite Grades (Excluding LG Envelope)..... 14-38
Figure 14-22: Swath Plots for the Main La Romanera Domains (OK Grade Profile in Orange and NN Grade Profile in Dark Red) 14-41
Figure 14-23: Swath Plots for Main La Infanta Domains (OK Grade Profile in Orange and NN Grade Profile in Dark Red) 14-42
Figure 14-24: Swath Plots for El Cura Top Lens (OK Grade Profile in Orange and NN Grade Profile in Dark Red)..... 14-43
Figure 14-25: La Romanera Long Sections – Mineral Resource Classification, Underground Reporting Shapes and Mineralisation Domain Intersections..... 14-46
Figure 14-26: La Infanta Long Sections – Mineral Resource Classification, Underground Reporting Shapes and Mineralisation Domain Intersections..... 14-47
Figure 14-27: El Cura Long Section – Mineral Resource Classification, Underground Reporting Shapes and Mineralisation Domain Intersections 14-48
Figure 15-1: Schematic of Planned and Unplanned Dilution..... 15-3
Figure 16-1: Location of Water Sampling Points..... 16-7
Figure 16-2: Longitudinal View of the La Romanera Mine Workings..... 16-12
Figure 16-3: View of the La Romanera Mine Workings with DSO Stope Set 16-13
Figure 16-4: Isometric View of the El Cura and La Infanta Mine Workings with DSO Stope Set 16-14
Figure 16-5: Typical Plan View Layout of a Production Level at Romanera (Level 405) ... 16-15
Figure 16-6: La Romanera Decline Access Locations Relative to the NSR High Value Areas of the Orebody (top) and Designated Mining Horizons (bottom)..... 16-16
Figure 16-7: Transverse Stope Primary-Secondary Mining Sequence (left) with Isometric Illustration of the Sequence in Progress (right)..... 16-18
Figure 16-8: Mining Sequence for Longitudinal Long-hole Open Stoping 16-18
Figure 16-9: Schematic Cross-sectional Profile of a CAPEX Heading with a MT436B Haul Truck..... 16-20
Figure 16-10: Schematic Cross-sectional Profile of an Ore Drive / Drawpoint Heading with an ST14S LHD..... 16-21
Figure 16-11: La Romanera DSO Optimisation Results Global NSR Distribution (looking north) 16-25
Figure 16-12: El Cura (top) and La Infanta (bottom) DSO Optimisation Results Showing Stope NSR per Tonne (looking north)..... 16-26
Figure 16-13: Romanera DSO Tonnes Distribution by Stope Width 16-27
Figure 16-14: Romanera DSO Global NSR Distribution by Stope Width..... 16-27
Figure 16-15: Drill-and-Blast Design for an Adjacent Transversal Primary and Secondary Stope at La Romanera 16-29

Figure 16-16: Drill-and-Blast Designs for Longitudinal Stopes at Each Deposit 16-30
Figure 16-17: LOM Development Metres Distribution 16-33
Figure 16-18: Annual LOM Vertical Development 16-34
Figure 16-19: Annual LOM Ore Production by Source 16-36
Figure 16-20: Annual LOM Production by Mining Horizon with Global Average NSR 16-37
Figure 16-21: Twin Decline Ventilation Strategy 16-45
Figure 16-22: Romanera Ventilation Network 16-46
Figure 16-23: El Cura Ventilation Network 16-47
Figure 16-24: La Infanta Ventilation Network 16-48
Figure 16-25: Overview of Mine Dewatering Strategy at the Project (looking north) 16-50
Figure 16-26: Railveyor Decline Profile Showing Standard Section (left) and Drive Station and Bypass Section (right) 16-51
Figure 16-27: Mobile Mining Fleet by Production Year 16-56
Figure 16-28: Mining Personnel by Production Year 16-57
Figure 17-1: Comminution Block Flow Diagram 17-2
Figure 17-2: Base Metals Flotation Block Flow Diagram 17-3
Figure 17-3: Pyrite Flotation Block Flow Diagram 17-4
Figure 17-4: PFD Colour Flow Sheet 17-7
Figure 17-5: Process Plant Main Area Overview 17-8
Figure 17-6: Crushing and Stockpile Areas 17-10
Figure 18-1: General Layout 18-2
Figure 18-2: Grid Power Supply 18-4
Figure 18-3: Water Supply 18-7
Figure 20-1: IBW Project Exploration Permit Boundary 20-1
Figure 20-2: Project Ventilation Shafts (Denoted by PVR) 20-7
Figure 20-3: Noise Monitoring Locations at the Proposed Mine Facilities 20-12
Figure 20-4: Noise Monitoring Locations at the La Romanera Ventilation Shafts 20-13
Figure 20-5: Habitat Mapping in the Project Area 20-15
Figure 20-6: Watercourses Within the Project Area 20-19
Figure 20-7: Known Archaeological Areas in and around the Project Footprint 20-28
Figure 22-1: LOM Ore Feed Production by Deposit and Sulphur Grade 22-3
Figure 22-2: Project NSR Contribution by Concentrate Type 22-6
Figure 22-3: Project Initial Capital Cost Distribution 22-7
Figure 22-4: Project Direct Capital Cost Distribution 22-8
Figure 22-5: LOM On-site Operating and Off-site Commercial Costs Split 22-9

Figure 22-6: Project Post-Tax-Free Cash Flow and Cumulative Cash Flow 22-11
Figure 22-7: Pyrite Concentrate Price Impact Analysis - NPV 8% (Post-tax) US$ m 22-19
Figure 22-8: Metal Price Sensitivity. Pyrite concentrate Price @ $274/dmt - NPV 8% (Post-tax) US$ m 22-19
Figure 22-9: After-Tax Sensitivity Analysis (NPV @8%) 22-21
Figure 22-10: After-Tax Sensitivity Analysis (IRR) 22-21
Figure 24-1: Neutral Albion Schematic Block Flow Diagram 24-2

1.0 Summary

1.1 Executive Summary

SLR Consulting Limited (SLR) was retained by Emerita Resources Corp (Emerita or the Company) to prepare an independent Technical Report on the Iberian Belt West (IBW) Project (the IBW Project or the Project), located in the Huelva Province of Andalusia, Spain. The purpose of this Technical Report is to present the results of a Pre-Feasibility Study (PFS) of the Project. This Technical Report conforms to NI 43-101 Standards of Disclosure for Mineral Projects.

Emerita is an exploration and development company focused on the discovery and development of high-grade polymetallic deposits in Spain. Emerita is a Canadian public company and its common shares are listed on the TSX Venture Exchange (TSX-V: EMO).

Emerita holds 100% ownership in the 1,545.6 hectare (ha) IBW Project, which is hosted in the Iberian Pyrite Belt (IPB). Three greenfield polymetallic deposits are located within the Project boundary: La Romanera, La Infanta, and El Cura. Mining is envisaged as underground long-hole open stoping (LHOS) and supports a 1-year ramp up and sustainable production rate of 1.2 million tonnes per annum (Mtpa) over an 18-year steady-state operating life, followed by 2 years of resource depletion. The pre-production development period lasts approximately 5 years. The saleable products produced at the Project are copper, lead, zinc, and pyrite concentrates, together with payable gold and silver by-products.

The effective date of the Mineral Resource and Mineral Reserve estimates in the Technical Report is July 17, 2026. Other information in this report is current as of the effective date of October 8, 2026.

1.1.1 Conclusions

The Qualified Persons (QP) have the following conclusions by area.

1.1.1.1 Geology and Mineral Resources

- There is a good understanding of the geology and the nature of the polymetallic mineralization at the IBW Project. The drill assays, logging, and geological model have enabled the three-dimensional (3D) delineation of the volcanogenic massive sulphide (VMS) lenses that form the basis of the Mineral Resource estimate.
- The samples used in modelling and estimation are representative of the mineralization and there is no evidence that the drilling or sample collection process has introduced a bias that could materially impact the accuracy and reliability of the results.
- The sample preparation, analysis, and security procedures have been conducted in accordance with acceptable industry standards, and the assay results are suitable for use in Mineral Resource estimation.
- Database verification procedures for the IBW Project comply with industry standards and are adequate for the purposes of Mineral Resource estimation.
- Canadian Institute of Mining, Metallurgy and Petroleum (CIM) Definition Standards for Mineral Resources and Mineral Reserves (CIM (2014) definitions) were used for Mineral Resource classification.

- Mineral Resource reporting is based on a conceptual operating scenario comprising underground mining via long-hole open stoping (LHOS), on-site selective flotation of copper (Cu), lead (Pb), zinc (Zn), and pyrite concentrates, and off-site third-party treatment and refining of the flotation concentrates.
- Mineral Resources are reported within underground reporting shapes using a net smelter return (NSR) cut-off value of US$69.30/t for La Romanera, US$79.20/t for El Cura, and US$85.30/t for La Infanta.
- As of July 17, 2026, the IBW Project Mineral Resources are estimated as follows:
    - Indicated Mineral Resources total approximately 26.1 million tonnes (Mt) grading approximately 2.27% Zn, 1.12% Pb, 0.45% Cu, 52 grams per tonne (g/t) silver (Ag), 1.04 g/t gold (Au), and 33.2% sulphur (S) and containing approximately 593 thousand tonnes (kt) Zn, 292 kt Pb, 116 kt Cu, 43,525 thousand ounces (koz) Ag, 871 koz Au, and 8,663 kt S.
    - Inferred Mineral Resources total approximately 9.9 Mt grading approximately 2.13% Zn, 1.00% Pb, 0.50% Cu, 36 g/t Ag, 0.50 g/t Au, and 22.7% S and containing approximately 212 kt Zn, 100 kt Pb, 50 kt Cu, 11,547 koz Ag, 161 koz Au, and 2,256 kt S.
- This updated Mineral Resource estimate supersedes the previous February 26, 2025, Mineral Resource estimate for the IBW Project. The Indicated Mineral Resources provide a basis for mine planning and Mineral Reserve estimation.
- Emerita has continued to drill at the El Cura and La Infanta deposits through 2026. New results have been reported from 11 drillholes at El Cura and 7 drillholes at La Infanta since the MRE database cut-off date (January 16, 2026). The results show potential to upgrade portions of the current Inferred Resources to Indicated and increase Mineral Resources through extensions to interpreted higher-grade trends that remain open down-plunge.

1.1.1.2 Mining and Mineral Reserves

- Mineral Reserves were estimated in accordance with CIM (2014) definitions. The disclosure of the Mineral Reserve estimate uses the NI 43-101 guidelines and is exclusive of Inferred Mineral Resources.
- As of July 17, 2026, the IBW Project Mineral Reserves are estimated as follows:
    - Probable Mineral Reserves total approximately 23.4 Mt grading approximately 2.30% Zn, 1.13% Pb, 0.45% Cu, 53 g/t Ag, 1.07 g/t Au, and 33.85% S and containing approximately 539 kt Zn, 264kt Pb, 105 kt Cu, 40,109 koz Ag, 807 koz Au, and 7,938 kt S.
- The mining plan includes underground mining of the La Romanera, El Cura, and La Infanta deposits. The La Romanera and El Cura deposits lie beneath a Natura 2000 protected area, precluding open pit mining. The La Infanta deposit is better suited to underground mining because of the narrow width of the mineralisation, which would result in high open pit stripping ratios.
- The shape, thickness, orientation, and geotechnical competence of the deposits support the use of LHOS mining methods for all deposits, with cemented or uncemented backfill to maximise mining recoveries.

- The La Romanera deposit accounts for approximately 87% of the IBW Project Reserve base and is therefore responsible for sustaining the majority of production over the life-of-mine (LOM). El Cura and La Infanta account for 8% and 5% of the Reserve base, respectively, and are included to support and supplement the process feed from La Romanera at a limited capacity.
- Mining at El Cura and La Infanta is scheduled to occur sequentially, allowing equipment and resources to be shared between operations. Strategically, it is preferable to schedule mining at El Cura prior to La Infanta for operational and economic reasons.
- The mine plan can support a global combined production rate of 1.2 million tonnes per annum (Mtpa), which is sustainable for 18 complete years of full-scale operation before ramping down over the subsequent two years of resource depletion. Prior to achieving full production, approximately 5 years of pre-production development are necessary to develop La Romanera and El Cura to a point where production activities can commence, followed by one year of mine production ramp-up. Opportunities to increase production rates that were not evaluated as part of the PFS may exist.
- Access to the La Romanera and El Cura deposits can be achieved via a 6.3 kilometre (km) decline from a surface portal located outside the Natura 2000 protected area to minimise surface disturbance. Adherence to the mining plan and financial assessment presented herein is reliant on meeting (or exceeding) the development rate assumed for the La Romanera decline to ensure timely access to the deposit.
- Railveyor has been chosen as the primary bulk material handling system for the IBW project and is well-suited to the La Romanera and El Cura deposits, providing a cost-effective material haulage solution along the extensive haulage route.
- Trade-off studies confirmed that a twin decline to the La Romanera deposit (i.e., a service ramp running parallel to a haulage ramp to house the Railveyor) is preferable to a single decline for operational reasons and provides marginal capital cost savings.
- The La Romanera deposit is divided into three mining horizons to facilitate early access to high-value ore and maintain production flexibility. Approximately 85% of the La Romanera deposit lies within Horizons 1 and 2 and can be fed to the Railveyor via an orepass system. The remainder in Horizon 3 requires truck haulage to reach the Railveyor, which can be accommodated by a 5.0 mH x 5.0 mW service ramp. A 30-t truck and a 14-t load-haul-dump (LHD) were considered suitable for the required production intensity.
- The mine workings at La Romanera can be adequately ventilated with a single 5.0 m diameter fresh air raise and a single 4.0 m diameter exhaust raise extending to the surface above the deposit. The approval of the surface ventilation infrastructure within the Natura 2000 area needs to be addressed during permitting, or alternative ventilation measures will need to be investigated, which will likely incur additional cost.

1.1.1.3 Mineral Processing

- The process plant is designed to process 1.2 Mtpa using standard comminution and flotation to produce four saleable concentrates: copper, lead, zinc, and pyrite.
- The run of mine (ROM) feed will be delivered to the ROM stockpile by Railveyors. The ore will be blended by using a front-end loader (FEL).This FEL will feed the jaw crusher which will operate approximately 12 hours per day (h/d), 365 days per annum.

- The process plant, including semi-autogenous grinding (SAG) mill, ball mill, and tower mill; four flotation circuits; and dewatering of concentrates and tailings will be operated 24 h/d, 365 days per annum for approximately 8,000 hours per annum.

1.1.1.4 Infrastructure

- The proposed infrastructure has been designed to support the planned 1.2 Mtpa underground mining and processing operation through an integrated network of mining, processing, transportation, utilities, and support facilities.
- The site layout efficiently integrates the mine portals, process plant, residue storage facilities, water infrastructure, and site services, minimizing transport distances and supporting operational efficiency.
- Existing access via the HU-5401 road and proximity to regional infrastructure provide suitable logistical support for construction and operations.
- Electrical power requirements are expected to be met through a new grid connection to the Puebla de Guzmán electrical network, with available regional capacity significantly exceeding current Project demand.
- The proposed water supply strategy, supported by water recycling from process and tailings dewatering circuits, provides a practical basis for long-term operational water requirements.
- Mine waste and filtered tailings management strategies prioritize underground reuse, paste backfill, and dry-stack storage, reducing surface storage requirements and supporting responsible environmental management.
- The recovery of a saleable pyrite concentrate further reduces the quantity of final flotation tailings requiring management, complementing the underground paste backfill strategy and reducing the surface storage requirement.
- The Project incorporates modern process control, communications, utility, and support infrastructure that are expected to support safe, efficient, and reliable operations throughout the life of mine.
- Further work at Feasibility Study level is required to finalize water permitting, confirm waste management and tailings storage strategies, and complete detailed engineering design.
- Based on the current PFS design, no material infrastructure constraints have been identified that would prevent development of the Project as planned.
- Overall, the proposed infrastructure is considered technically feasible and adequate to support the planned mining and mineral processing operations over the life of the Project.

1.1.1.5 Environment, Permitting, and Social

- The Project's existing permit applications are based on the 2023 Project concept and will require updating to reflect the current PFS design.
- Although the Project's designation as being of Strategic Interest by the Government of Andalusia supports coordinated administrative review, the outstanding environmental, mining, water, discharge, restoration, road and municipal approvals, together with land access agreements, remain material to the Project schedule.
- The principal environmental risks relate to water management, historical acid rock drainage and metal contamination, biodiversity and the Natura 2000 designation, mining waste and closure. Although most surface infrastructure is outside the Andévalo Occidental Special Area of Conservation (ZEC), the proposed ventilation infrastructure within the protected area remains a material permitting risk.
- The environmental and social baseline is sufficiently developed to support the PFS, although additional work will be required to support permitting and the next stage of design.
- Local support is generally positive, reflecting anticipated employment and regional development benefits. Maintaining stakeholder confidence will depend on effective management of environmental performance, land access, local livelihoods and expectations regarding Project benefits. Cultural heritage, occupational health and safety, emergency response, rehabilitation and closure requirements have been identified and incorporated at a preliminary level, but will require further development as the Project design and permitting process advance.

1.1.1.6 Capital and Operating Costs

Initial capital costs are estimated at US$566.7 million, including mine development, process plant and infrastructure, indirect costs, Owner's costs, and contingency. Capital expenditures are scheduled in accordance with the Project development and construction schedules, with expenditure commencing in Year -5 to reflect the underground mine development required in advance of production. Process plant and associated infrastructure expenditure is concentrated principally over the subsequent construction period.

In addition to initial capital, the financial model includes approximately US$279.5 million of sustaining capital over the LOM and approximately US$12.0 million of post-mining closure costs, resulting in total Project capital expenditure of approximately US$858.2 million.

A summary of the LOM capital costs incorporated in the financial model is presented in Table 1-1.

Table 1-1: Life-of-Mine Capital Cost Summary

Category	Cost (US$ million)
Direct Costs	394.7
Indirect Costs and Engineering, Procurement and Construction Management (EPCM)	36.3
Owner's Costs	19.7
Contingency	63.6

Category	Cost (US$ million)
Other Costs	52.4
Total Initial Capital Costs	**566.7**
Sustaining Capital	279.5
Closure Costs (Post-mine activities)	12.0
TOTAL PROJECT CAPITAL	**858.2**
Note: Totals may not sum precisely due to rounding.	

LOM on-site operating costs are estimated at approximately US$2.03 billion, comprising mining, processing, G&A, water and waste management, and backfill, and progressive rehabilitation costs. Mining and processing represent the principal on-site operating cost components.

Approximately US$0.89 billion in off-site and commercial costs have been estimated over the LOM, comprising treatment and refining charges (TC/RC), concentrate penalties, transportation, and sales costs. These costs have been deducted in the calculation of Project NSR.

All operating costs incurred prior to the commencement of production are capitalised in the financial model and included within initial capital costs.

A summary of the LOM on-site operating costs incorporated in the financial model is presented in Table 1-2 shows.

Table 1-2: OPEX by cost category

Cost Category	Cost (US$ million)
On-site Costs	
Mining	882
Processing	708
General and Administrative	70
Water Treatment, Waste Management and Backfill	363
Progressive Rehabilitation	5
Total On-Site Operating Costs	**2,028**
Off-site Costs	
Treatment and Refining Charges (TC/RC)	92
Concentrate Penalties	506
Transportation and Sales	287
Total Off-Site Costs	**886**

At the LOM processing throughput of approximately 23.4 Mt, the Project's operating cost structure is summarised in Table 1-3. LOM operating cost is estimated at US$86.48/t ore processed.

Table 1-3: Life-of-Mine Unit Operating Costs (Year 1 – Year 21)

Cost Category	Cost (US$/t Ore Processed)
Mining Operating Costs	37.61
Processing Costs	30.20
Contact Water Treatment	3.52
Capital Recovery Charge For Water Treatment Plant	6.06
Mine waste / ATEM	0.15
Tailings / IPS	0.53
Paste Backfill	5.24
G&A	2.97
Progressive rehabilitation	0.22
Total Operating Costs	**86.49**

1.1.2 Recommendations

1.1.2.1 Geology and Mineral Resources

1 Optimise exploration and resource development drilling by focusing on the following tasks:

   a) Infill drilling underground reporting shapes containing Inferred Mineral Resources, to upgrade material to Indicated, prioritising areas according to mineable stope optimiser (MSO) stope NSR value.

   b) Testing open extensions to underground reporting shapes at depth and along strike.

2 Consider targeted close-spaced drilling in areas that are expected to have the greatest impact on early LOM production.

3 Confirm primary sulphide mineralogy of stopes at the base of the weathering profile, via diagnostic leach assays for pulps from key drillhole intersections. Consider targeted infill drilling to delineate the top of fresh rock contact, proximal to any stopes that are early in the LOM schedule.

4 Following variability testwork on the PFS flotation flowsheet, develop a geometallurgical model of metallurgical recovery, payability, and hardness variability to refine block NSR calculations and support future technical evaluations.

5 Expand duplicate sample types to include a coarse duplicate submitted to the primary laboratory and a pulp duplicate submitted to an umpire laboratory.

6 Refine IBW Project certified reference materials (CRMs) to include polymetallic sulphide materials with higher sulphur grades for La Romanera and El Cura, and higher copper grades for El Cura.

7 Complete chlorine (Cl) and fluorine (F) assays for a selection of pulps, to assess whether geochemical proxies can be developed to model these potential penalty elements.

1.1.2.2 Mining and Mineral Reserves

1 Conduct studies to increase mine production rates in support of higher mill throughput. Higher mining rates provide economies of scale and reduce unit costs, potentially leading to an increased Mineral Reserve base. If the increased cash flows from the elevated throughput can be supported by the higher CAPEX requirements, improvements in project net present value (NPV) may also result.

2 Undertake survey work on the historical mine workings close to the surface. Based on current information, the workings pose a negligible impact on the PFS mine design and Reserve estimate (only appearing to cross the delineated stope set at the very top of the La Romanera deposit at the end of the mine life). However, it is recommended that their position be accurately confirmed to eliminate doubt and remove any potential future safety hazard.

3 Following detailed metallurgical testwork, investigate mine scheduling strategies to optimise a ROM blend that stabilises ore feed grades and material types to the mill.

4 Following the acquisition of geotechnical and hydrogeological data, conduct a detailed analysis to define advance rates for the twin decline to La Romanera. The analysis should delineate areas of poor ground and/or expected water infiltration and advance rates should be reduced accordingly. Conversely, areas of favourable conditions should be identified to produce a comprehensive, qualified estimate of expected arrival time at the mining deposit.

5 Conduct material handling studies to guide detailed material pass design with the following objectives:

   a) Confirm current material pass geometries via rock fragmentation analysis (empirical or otherwise).

   b) Inform detailed material pass design, placement, and layout.

   c) Provide geotechnical assessments for support recommendations and rehabilitation requirements.

   d) Provide optimal strategies for material management (number of material passes, separate ore and waste passes, material blending opportunities, etc.).

6 Investigate more efficient and cost-effective ways to return waste material to the underground for backfill (possibly using Railveyor), including longer-term, higher-capacity underground waste storage, such as designated waste storage stopes.

7 Undertake studies to optimise the backfill material balance to address the limited quantities of tailings for pastefill and the limited volumes of waste rock for rockfill/ cemented rockfill (CRF), such as flexing the primary/secondary stope width ratio and reviewing the backfill barricade construction method (shotcreted fill fence versus shotcreted rock bumper).

8 Optimise ventilation raise diameters for CAPEX reduction and energy saving potential, including trade-off studies on the application of ventilation on demand (VOD) systems and the adoption of battery electric vehicles (BEVs).

9 Conduct a mine water balance study following hydrogeological testwork and update the mine dewatering and water management system design accordingly.

10 Investigate the technical and regulatory means of placing primary ventilation fans underground at La Romanera. The current design assumes they are on the surface

within the Natura 2000 area, which will need to be addressed during permitting. Underground installation would be preferable for reducing surface disturbance and noise; however, it may require local mine regulatory approval.

11 Expand the permit boundary slightly south of the La Infanta deposit (approximately 50 m). The current southern boundary restricts space for the decline and footwall infrastructure, compromising stand-off distances to production areas. This limited space may lead to sub-optimal mine design once a detailed geotechnical appraisal is completed.

12 Re-evaluate the material handling system for La Infanta. The current assumption of using Railveyor implies a relatively high CAPEX per tonne, with minimal LOM OPEX savings. Truck haulage may offer a more flexible option at lower CAPEX.

1.1.2.3 Mineral Processing

1 Address gaps in current metallurgical knowledge in the next stage of study through the following testwork:

a) Variability sample testwork on a suitable number of samples from all three deposits (ore hardness and metallurgical response variability, generation of recovery head grade relationships).

b) Additional locked cycle tests (LCTs) on new composite samples for each deposit representing the lower head grades as defined in the PFS Mineral Resource estimate.

c) Additional flotation testwork for pyrite concentrate production (only limited open circuit testwork has been conducted to date).

d) Thickening and filtration testwork on bulk samples of the concentrates and final tailings (only benchmark data used to date).

2 Further define the impact of the deleterious elements based on the future variability sample testwork and conduct discussions with relevant traders and smelters.

3 Explore reducing the comminution equipment costs by replacing the combination of SAG + ball mill by a combined high pressure grinding roll (HPGR) + stirred media detritor (SMD) as the ore properties may be favourable for an HPGR circuit. An HPGR supplier has indicated a substantial reduction in OPEX by reducing milling energy consumption by approximately 31% compared to the currently specified equipment. This results in a carbon emissions reduction of 44% based on energy savings and no requirement for steel grinding media. Testwork could be carried out at supplier's facilities to verify/de-risk the proposed circuit.

4 Evaluate the final mining production schedule grades against the process plant design head grades, as well as any process plant bottlenecks, especially potential bottlenecks due to higher grade ROM feed in the flotation and filtering circuits.

1.1.2.4 Infrastructure

1 Secure Grid Power Connection

a) Obtain a new grid connection via the Red Eléctrica de España network from the Puebla de Guzmán substation.

b) Finalise a power supply agreement with a regional power provider.

c) Maintain and convert the existing 30 megawatt (MW) reservation into a long-term supply arrangement sufficient for project demand.

d) Ensure power infrastructure is sized for approximately 26.8 MW installed load and annual consumption of approximately 153 GWh, including mining and processing infrastructure.

2 Advance Water Permitting

a) Progress permitting for water abstraction from the Andévalo Reservoir system with the Confederación Hidrográfica del Guadiana which, if granted, will be effective in 2028.

b) Obtain the required planning reserve, environmental approvals (AAU), mining concession, and water concession before water rights can be granted.

c) Secure the proposed water allocation of approximately 1.51 hm^3 per year for project start-up requirements.

d) Continue negotiations with the agricultural community for interim water access from the Guadiana River until the expected granting of the Industrial Water Permit allocation in January 2028.

3 Develop Site Access and Logistics Infrastructure

a) Construct the main access road network and internal 9 m wide haul and service roads linking the following surface infrastructure:

i. Process plant

ii. Mine portals

iii. Tailings dewatering area

iv. Mine waste storage facilities (*Acopio Temporal de Estériles de Mina*, ATEM)

v. Integrated Process Residue Storage Facility (*Instalación de Pasta Seca,* IPS)

vi. Administrative facilities

b) Plan for regional traffic impacts associated with concentrate transport, particularly pyrite shipments, which will account for the majority of truck movements.

4 Establish Site Operational Facilities

a) Construct administration offices, laboratory facilities, personnel buildings, and maintenance workshops early in project development

b) Provide fully equipped analytical laboratories supporting:

i. Process control

ii. Environmental monitoring

iii. Fire assay

iv. Metallurgical analysis

5 Implement Water Management Infrastructure

a) Develop the raw water, treated water, and stormwater pond systems.

b) Implement process water recycling systems to reduce long-term freshwater demand.

6 Install drainage and stormwater attenuation facilities to manage runoff from the process plant area.

7 Support High Production Logistics

8 Design transport and loading systems to accommodate annual production of:

   a) Pyrite concentrate

   b) Copper concentrate

   c) Lead concentrate

   d) Zinc concentrate

9 Ensure road and port logistics can support approximately 104 concentrate truck movements per day.

1.1.2.5 Environment, Permitting and Social

1 Reconcile the current PFS design, mine schedule, infrastructure layout, process mass balance, waste storage requirements, and backfill strategy with the exploitation permit, AAU, Restoration Plan, and supporting permit applications.

2 Maintain an integrated permit register and programme covering the AAU, exploitation permit, water concessions, discharge permit, restoration approval, road and municipal licences, containment pond classification, and land access agreements.

3 Complete an ESIA and ESMP aligned with applicable Spanish and EU requirements and relevant good international industry practice, incorporating all Project phases and updated specialist studies.

4 Complete seasonal surface water monitoring, groundwater baseline studies, hydrological and hydrogeological investigations, and an updated dynamic water balance before construction.

5 Finalise the integrated water management design, including clean and contact water separation, treatment requirements, discharge criteria, water reuse, storage capacity, and monitoring provisions.

6 Complete geochemical and geotechnical testwork for waste rock, tailings, and treatment residues, and confirm the design and capacity of the ATEM, IPS, and backfill systems.

7 Update the biodiversity assessment for the current Project footprint and complete the assessment of effects on the Andévalo Occidental Special Area of Conservation, including mitigation, restoration, monitoring, and any required compensation measures.

8 Complete design-specific air quality and noise assessments, supported by representative baseline monitoring and clearly defined sensitive receptors.

9 Establish contaminated soil, erosion, sediment, topsoil, spill-prevention, and rehabilitation management procedures before earthworks commence.

10 Complete the social baseline and impact assessment, including land tenure, livelihoods, vulnerable groups, community infrastructure, worker influx, community health and safety, human rights, traffic, employment, and procurement.

11 Prepare and implement a Stakeholder Engagement Plan, community grievance mechanism, land access strategy, local employment and procurement plan, and transparent communications programme.

12 Complete a traffic and road safety assessment for the HU-5401 and other affected roads, incorporating construction and operational traffic, community access, and emergency-response requirements.

13 Protect identified archaeological sites, provide archaeological monitoring of relevant earthworks, and implement a formal chance-find procedure and worker training programme.

14 Finalise Project-specific occupational health and safety, emergency response, security, contractor-management, and workforce training arrangements before construction.

15 Prepare a Project-wide Non-Mining Waste Management Plan addressing waste classification, segregation, storage, transport, disposal, traceability, and contractor responsibilities.

16 Update the closure and restoration plan to reflect the current PFS design, actual waste inventories, final landforms, progressive rehabilitation, post-closure monitoring, and long-term water management requirements.

17 Update closure costs and financial provisions and include adequate budgets for permitting, baseline studies, mitigation, monitoring, stakeholder engagement, rehabilitation, and post-closure obligations.

1.1.2.6 Capital and Operating Costs

1 Focus on reducing key areas of cost uncertainty prior to completion of subsequent study phases.

2 Complete further design development to improve estimate accuracy and support progression toward a Feasibility Study level estimate.

3 Continue engagement with vendors to obtain budget quotations for major equipment and construction contracts to further refine capital cost assumptions and reduce contingency requirements.

4 Use ongoing metallurgical testwork results to better define blended concentrate specifications and support more robust estimates of treatment charges, refining charges, and deleterious element penalties.

5 Advance discussions with potential smelter and concentrate purchasers to validate the treatment, refining, transportation, and penalty assumptions adopted in the PFS.

6 Refine closure and rehabilitation planning in consultation with the relevant regulatory authorities, with updates to closure cost estimates and rehabilitation schedules incorporated into future project analyses.

1.1.3 Risks

Discipline	Project Element	Risk Name	Risk Description	Consequence(s) Description	Inherent Risk		Mitigation(s)	Mitigated Risk	
					Rating	Qualitative Result		Rating	Qualitative Result
Mining and Mineral Reserves	2.B	Development advance rate	Inability to meet the development advance rates required of the PFS mine schedule	Delays in providing adequate feed to the mill leading to revenue reductions	C3	High	The mine plan is scheduled using benchmarked operational advance rates on an equivalent-meter basis (i.e., advance rates for larger profiles are reduced accordingly). Ore drive development is reduced to 25m/mo to allow provision for grade control activities. Multi-heading Jumbo assignment generally adopts an advance rate of 50m/mo (~3 rounds/week) with isolated priority headings set at 75m/mo at the start of the schedule to prioritise the establishment of early mine infrastructure. Advance rates of 100-150m/mo are applied only to single-face mode development, i.e. blasting can occur at any time during the work shift to maximise face cycle time. Such rates are considered highly sustainable with modern mining equipment under reasonable operating conditions.	D3	Medium
Mining and Mineral Reserves	2.C	Mining production rate	Inability to meet the mine production ramp-up/sustained production rates used for economic modelling	Delays in providing adequate feed to the mill leading to revenue reductions	C4	High	The mining plan includes a detailed representation of the operational stope sequencing, with stope cycle delays derived from first principles and benchmarked assumptions. Mine access and operational interactions for all stopes have been planned in detail and simulated using industry-standard mine-planning software. Mine scheduling delays are introduced for contingency, and to provide adequate time for geological definition to assist production forecasting. 1.2 Mtpa is also considered a reasonably conservative production target, given the potential of the Romanera deposit.	D3	Medium
Mining and Mineral Reserves	2.D	Decline development rate	Delays in surface decline development.	Delayed ramp-up. Reduction in project NPV.	C3	High	Conduct hydro/Geotech drilling along decline profile to confirm drifting conditions. Allocate the decline development phase to a mining contractor, with mining rates embedded into contractual obligations.	D3	Medium
Mining and Mineral Reserves	2.H	Production rate	Increase mining production rate from 1.2Mtpa	Higher mining throughputs leading to increased project revenues and potentially higher NPVs.	C3	High	Conduct a trade-off considering increased cash flows versus higher project CAPEX.	C2	Medium
Mining and Mineral Reserves	2.K	Rockfill / CRF reliance and mine productivity	Residual rockfill and CRF requirements must be integrated with the mine production schedule. The all-CRF Infanta sensitivity would require approximately 0.744 Mt CRF and results in approximately 0.72 Mt LOM deficit of fill-grade rock/aggregate.	Additional haulage and placement fleet, level congestion, competition between ore and fill transport, ventilation demand and CRF cycle times may reduce mine productivity and increase OPEX. External rock/aggregate may also be required.	C4	High	Retain paste fill at Infanta in the selected PFS basis; use CRF only where specifically required by Mining; explicitly test residual rockfill/CRF demand against haulage capacity, level access, fleet and ventilation in the integrated Mining schedule.	D3	Medium
Infrastructure and Tailings	4.	ATEM peak occupancy and waste routing	The current Mining schedule indicates that peak surface mine-waste inventory may exceed the existing 0.844 Mm3 ATEM capacity if all surface-routed waste is passed through ATEM.	Potential approximately 0.30 Mm3 temporary capacity shortfall, additional rehandling/haulage, additional temporary storage requirement and associated water-management, permitting and operating-cost impacts.	C3	High	Integrate the annual waste-routing and fill schedule; maximise direct-to-underground routing and accelerated ATEM drawdown where practicable. Retain approximately 1.20 Mm3 temporary-capacity sensitivity if schedule reconciliation demonstrates that the existing ATEM cannot maintain the required operating inventory.	C2	Medium

Discipline	Project Element	Risk Name	Risk Description	Consequence(s) Description	Inherent Risk		Mitigation(s)	Mitigated Risk	
					Rating	Qualitative Result		Rating	Qualitative Result
Environment, Social and Permitting	5.A	Natura 2000 (Andévalo Occidental Special Area of Conservation)	Construction of ventilation shafts within the Natura 2000 protected area; Discharge of water into watercourses in Natura 2000.	Delays in implementation schedule; Permit rejection or delays (const. and op.); Stakeholder / NGO objections; Costly or challenging offset commitments; Loss, degradation or fragmentation of habitat.	B4	Very High	Provision of a biodiversity offset (plus Habitats Regulation Assessment); Avoid and minimise impacts to biodiversity and water resources; Engage with relevant stakeholders (regulatory bodies) on permitting process and requirements within Natura 2000 sites; Engage with other relevant stakeholders (communities, NGOs); Restoration of habitats (habitats of community interest etc); Critical Habitat Assessment.	C3	High
Environment, Social and Permitting	5.B	Land acquisition and access	Acquisition or leasing of land required for all surface infrastructure, access and biodiversity offsets.	Unknown cost associated with purchasing or leasing land; Unrealistic expectations by landowners; Extended lease or purchase negotiations.	A3	High	Engage with landowners; Understand landowner expectations; Independent evaluation. Audit for impact on physical structures.	C2	Medium
Environment, Social and Permitting	5.C	Land acquisition and livelihood	Disruption to land-based livelihoods due to land access restrictions and land acquisition for surface infrastructure and offsets.	Loss of trust, grievances, could cause delays in permitting, could impact land purchases and lease agreements.	A3	High	Stakeholder Engagement Plan; Social baseline; Livelihood Restoration Plan if required; Grievance Mechanism.	C2	Medium
Environment, Social and Permitting	5.E	Surface water resources	Contamination of surface water from the Project (acid mine drainage, metal leaching, runoff of chemicals, sedimentation); Impacts to Andévalo Reservoir and watercourses within the Project area.	Degradation of existing surface water resources; Community or landowner grievances; Legal and reputational consequences.	B4	Very High	Undertake seasonal baseline surface water sampling; Undertake surface and groundwater impact assessment; Confirm water treatment plant, wastewater treatment plant and discharge limits (quality and quantity); Consider re-use / recycling of water within water management plan (e.g. within processing plant).	C3	High
Environment, Social and Permitting	5.F	Dust, traffic, noise and vibration	Increased dust, traffic, noise and vibration during construction and operation.	Existing land users (grazing, agriculture, other land uses); Impacts to biodiversity (flora, fauna, habitat degradation and fragmentation); Degradation of surface water resources (contamination, sedimentation); Land owner grievances.	A3	High	Air quality, noise and traffic studies (baseline and IA); Traffic management plan.	C2	Medium
Environment, Social and Permitting	5.G	Project related influx	Reduced health and wellbeing due to increased demand on services, increase in anti-social behaviour, price inflation.	Perceived expectation on EMERITA to fund any new infrastructure or expansion of existing infrastructure.	B3	High	Understanding of current capacity of existing infrastructure in the region and needs, Stakeholder engagement, local employment and management of influx.	C2	Medium
Environment, Social and Permitting	5.H	Unmet expectations	Unmet expectations of communities in terms of project benefits and jobs.	Loss in trust (increase in grievances), increase of the evaluation price of land purchases and leases, delay of permitting process.	B3	High	Stakeholder Engagement Plan; Local employment and local upskilling.	C2	Medium
Environment, Social and Permitting	5.I	Obtaining critical permits	Not obtaining all critical permits required to commence construction and operation (water supply and discharge, land access, temporary water diversion, exploitation etc).	Rejection or delays to permit approval process due to current challenging regulatory approach in Spain and national and local regulatory bodies; Permits granted with unrealistic or unreasonable expectations.	B4	Very High	Develop a permitting strategy; Benchmark permitting timeframes; Engage with stakeholders; Undertake all required specialist studies (inc. ESIA); Stakeholder Engagement Plan.	D3	Medium
Processing and Metallurgy	3.H	Concentrate Quality	Impact of penalty elements on concentrates quality.	Concentrates may be subject to further penalty deductions affecting revenues.	D4	High	Conduct variability sample testwork programme to confirm impact of penalty elements such as mercury and initiate discussions with potential smelters and traders.	D3	Medium
Infrastructure and Tailings	4.A	Performance of the backfill	Proposed backfill solution has not been tested	Backfill system may not meet the requirements of the project and may lead to increase in CAPEX and OPEX.	C4	High	Undertake the required testwork to increase confidence in the backfill solution	D3	Medium

1.2 Economic Analysis

- The economic analysis demonstrates that the IBW Project is a robust, long-life polymetallic mining operation supported by revenues from zinc, lead, copper, and pyrite concentrates, together with payable gold and silver by-products. The saleable products are intended for an international market.
- The Project is based on a 21-year mine life and a processing rate of 1.2 Mtpa. Over the LOM, approximately 23.4 Mt of ore will be processed.
- Economic modelling was undertaken on an unlevered, post-tax basis using an 8% discount rate and long-term commodity price assumptions adopted for the PFS. Pyrite concentrate represents the largest contributor to project revenue, accounting for approximately 66% of total NSR, with the balance derived from zinc, lead, copper, silver, and gold.
- Under these base case assumptions, the Project generates the following returns:
  - Gross revenue: approximately US$7.47 billion
  - NSR: approximately US$6.59 billion
  - Earnings before interest, taxes, depreciation,and amortisation (EBITDA): approximately US$4.56 billion
  - Post-tax free cash flow: approximately US$2.66 billion
  - Post-tax NPV_8: US$776 million
  - Post-tax internal rate of return (IRR) of 23.51%
  - Profitability index: 2.37
  - Pre-production period: 5 years
  - Payback from first production is approximately 1 year 11 months.
  - Payback from initial investment is 6 years 11 months.
- Sensitivity analysis indicates that Project economics are materially influenced by pyrite concentrate pricing and marketability, highlighting the importance of pyrite revenues to overall Project value. Nevertheless, the Project remains economically robust across all evaluated pricing and cost scenarios, maintaining positive NPVs and attractive rates of return. Under the conservative pyrite price case, the Project generates a post-tax $NPV_{8\%}$ of US$580 million and an IRR of 20.51%, while the high pyrite case increases these metrics to US$1,035 million and 27.03%, respectively.
- Overall, the PFS results demonstrate that the IBW Project has strong economic fundamentals, generates substantial cash flow over its operating life, and exhibits resilience to variance in key economic assumptions, supporting project advancement to the next stage of development.

1.3 Technical Summary

1.3.1 Property Description and Location

The IBW Project is located in southwest Spain within the Huelva Province of Andalusia. The Project is situated approximately 500 kilometres (km) southwest of Madrid (Spain's capital), 142 km west of Seville (capital of Andalusia), 61 km northwest of Huelva City (capital of Huelva Province), and 9 km east of the Spanish/Portuguese border. Two small towns, Puebla de Guzman and Paymogo, are within 10 km of the property and are linked by the paved provincial road HU-5401, which provides access to the Project area.

1.3.2 Land Tenure

The IBW Project exploration permit (permit number 15029) covers 51 claims, totalling 1,545.6 hectares (ha) and contains the La Romanera, La Infanta, and El Cura polymetallic sulphide deposits. Emerita holds 100% ownership via its subsidiary Emerita Resources España SLU.

The exploration permit was granted for a period of 26 months on July 12, 2021, with the option to renew for a further 3 years. On September 9, 2023, Emerita Resources España SLU applied to the *Delegación Territorial de Energia y Minas* in Huelva Province*, Junta de Andalucia* (the Junta) for an exploitation permit for the IBW Project. The exploitation permit application covers the same area as the existing IBW Project exploration permit.

On May 13, 2026, Emerita was notified that the AAU for the IBW Project exploitation permit application had advanced to the public consultation stage. The AAU approval process included public consultation from May to July 2026, followed by Junta review and resolution of stakeholder comments. An environmental ruling is expected by year-end 2026, with administrative hearings and comment resolution anticipated in Q1 2027. Final review by the relevant Huelva authorities and approval by the Junta are targeted for Q2 2027, after which the Exploitation Permit may be issued.

Exploitation permits in Spain, when granted, have a 30 year term and can be extended for two subsequent 30 year periods. During the time that the IBW Project exploitation permit application is being reviewed by the Junta, Emerita's rights under its existing exploration permit are extended, allowing ongoing exploration programmes.

1.3.3 Existing Infrastructure

The Andalusian Region is connected by a well-developed transport network, reliable energy and water supply, and high-speed communication systems. The area has a longstanding history of mining and resource development, including active production at Sandfire's MATSA Copper Operations and Atalaya Mining's Riotinto Project. Huelva City has a commercial port from which products from mining in the region can be shipped.

1.3.4 History

Historical mine workings at La Romanera, La Infanta, and El Cura date back to the pre-Roman and Roman eras. The Project contains various small-scale prospecting pits, shallow shafts, adits, and exploration drives. Limited production records are available, and no historical surface infrastructure remains on site.

The deposits have undergone several phases of small- to medium-scale exploration by various owners prior to the current phase of exploration by Emerita. Limited supporting documentation is available for historical drilling and it has been excluded from the MRE database, with drill coverage replaced by Emerita drilling.

1.3.5 Geology and Mineralisation

The La Romanera, La Infanta, and El Cura deposits are located in the northwest of the Spanish IPB, within the northern limb of the Puebla de Guzman anticline, hosted by the Paymogo Volcano-Sedimentary Alignment (PVSA), a division of the Volcano-Sedimentary Complex (VSC).

Mineralisation is classified as VMS and occurs primarily as tabular strata-bound lenses of polymetallic (Zn, Pb, Cu, Ag, Au) sulphides. All lenses strike approximately east-west and dip steeply to the north. The main minerals are pyrite, sphalerite, galena, chalcopyrite, arsenopyrite, and members of the tetrahedrite-tennantite solid solution series. Massive sulphide textures are dominant at La Romanera and El Cura, whilst lower sulphide content is typical at La Infanta. Metal association varies from distinctly Zn-Pb-Ag rich mineralisation at La Infanta, higher Cu-Au grades at El Cura, and a more mixed assemblage at La Romanera.

The Emerita geology team have completed detailed deposit-scale geological mapping, core logging, and cross-section interpretations to constrain the geological framework of each deposit, including the host lithostratigraphic sequence and the nature of key contacts. Beyond the deposit areas, Emerita has completed systematic outcrop mapping across the IBW Project permit, which has been integrated with geochemical and geophysical survey data, to develop a coherent project-scale geological map. SLR used these inputs to develop a three-dimensional geological model for the Project.

1.3.6 Exploration Status

Emerita has carried out a range of exploration activities at the IBW Project including historical data compilation, geological mapping, soil geochemical sampling, soil vapour geochemistry, airborne, surface and downhole geophysics, and exploration drill programmes.

Since 2021, and up to the MRE database cut-off date of January 16, 2026, Emerita has completed 352 surface diamond drillholes for approximately 123 km of drilling. This drilling has so far defined six major sulphide lenses across the three deposits: the Upper and Lower Lenses at La Romanera, the North, South, and South 1 Lenses at La Infanta, and the Top Lens at El Cura.

New drilling since the previous Mineral Resource estimate (effective date February 26, 2025) includes a single deep drillhole at La Infanta and an additional 52 drillholes for 17,015 m of drilling at El Cura. There is potential for further incremental extensions to the known deposits.

1.3.7 Metallurgical Testing

The metallurgical programme successfully demonstrates that the Project ROM can be processed through a single, integrated flotation plant producing copper, lead, zinc, and pyrite concentrates. Recovery levels and concentrate grades are generally commercially acceptable, and the pyrite flotation stage provides a significant additional revenue opportunity. The principal remaining technical uncertainty is the limited variability testwork, particularly for La Romanera, which represents approximately 83% of the project Resource base. Additional variability, concentrate quality, and dewatering testwork is recommended before advancing to the next study stage.

1.3.8 Mineral Resources

Modelling and estimation were completed by SLR using data provided by Emerita.

Geology, weathering and mineralisation domain wireframes were constructed using Leapfrog Geo. Estimation for Zn, Pb, Cu, Ag, Au, S, and density was completed in Leapfrog Edge and utilised hard boundaries, ordinary kriging, or inverse distance squared, an expanding three-pass search plan, and dynamic anisotropy to align search orientation to local domain orientation.

Estimates were validated globally, locally and visually against drillhole composite values and nearest neighbour estimates.

Classification was set in the block models using wireframes that define contiguous regions that meet specific drill spacing and estimation pass criteria. For Indicated Resources, nominal drill spacing is 50 m or less and blocks are mainly estimated in the first pass. For Inferred Resources, nominal drill spacing is 100 m or less.

Mineral Resource reporting is based on a conceptual operating scenario comprising underground mining via LHOS, on-site selective flotation of Cu, Pb, Zn, and pyrite concentrates, and off-site third-party treatment and refining of the flotation concentrates.

Mineral Resources are reported within underground reporting shapes based on NSR cut-off values of US$69.30/t for La Romanera, US$79.20/t for El Cura, and US$85.30/t for La Infanta. The Mineral Resource estimate was prepared in accordance with the CIM (2014) definitions.

The QP is not aware of any environmental, permitting, legal, title, taxation, socio-economic, marketing, political, or other relevant factors that could materially affect the Mineral Resource estimate.

A summary of the IBW Project Mineral Resources, effective July 17, 2026, is presented in Table 1-4.

Table 1-4: Summary of Mineral Resources – July 17, 2026

Deposit	Class	Tonnage Mt	Average Grade						NSR $/t	Contained Metal					
			Zn (%)	Pb (%)	Cu (%)	Ag (g/t)	Au (g/t)	S (%)		Zn (kt)	Pb (kt)	Cu (kt)	Ag (koz)	Au (koz)	S (kt)
La Romanera	Indicated	22.4	2.15	1.03	0.38	53	1.10	35.9	236	481	230	84	38,199	792	8,018
	Inferred	6.6	2.02	0.84	0.49	33	0.57	29.6	192	133	55	32	7,090	120	1,952
El Cura	Indicated	2.1	1.20	0.57	0.96	30	0.98	25.8	223	25	12	20	2,010	65	535
	Inferred	0.9	0.98	0.42	0.74	19	0.62	18.7	165	9	4	7	556	18	168
La Infanta	Indicated	1.7	5.25	3.00	0.73	63	0.25	6.7	228	87	50	12	3,316	13	111
	Inferred	2.4	2.87	1.67	0.45	50	0.28	5.6	147	70	41	11	3,901	22	135
IBW Project	**Indicated**	**26.1**	**2.27**	**1.12**	**0.45**	**52**	**1.04**	**33.2**	**235**	**593**	**292**	**116**	**43,525**	**871**	**8,663**
	Inferred	**9.9**	**2.13**	**1.00**	**0.50**	**36**	**0.50**	**22.7**	**178**	**212**	**100**	**50**	**11,547**	**161**	**2,256**

Notes:

1. CIM (2014) definitions were followed for Mineral Resources.
2. The reporting approach is based on underground mining via long-hole open stoping, on-site selective flotation of copper, lead, zinc, and pyrite concentrates, and off-site third-party treatment and refining of the flotation concentrates.
3. Mineral Resources are reported within underground reporting shapes generated using a mineable stope optimiser (MSO) above NSR cut-off values of US$69.30/t for La Romanera, US$79.20/t for El Cura, and US$85.30/t for La Infanta. Only primary sulphide mineralisation is included in the Mineral Resource.
4. The NSR values for each block were calculated using the following formulas:
   - La Romanera – Zn(%)*US$14.72 + Pb(%)*US$6.79 + Cu(%)*US$40.39 + Ag(g/t)*US$1.10 + Au(g/t)*US$6.77 + S(%)*US$3.28
   - El Cura – Zn(%)*US$13.11 + Cu(%)*US$93.42 + Ag(g/t)*US$0.85 + Au(g/t)*US$7.15 + S(%)*US$3.33
   - La Infanta – Zn(%)*US$17.54 + Pb(%)*US$12.56 + Cu(%)*US$25.73 + Ag(g/t)*US$1.22 + Au(g/t)*US$10.52
5. Factors in the NSR formulas are based on consensus long-term metal price forecasts, metallurgical recoveries from available testwork, and market studies, used to estimate payable factors, transport, treatment and refining charges. Inputs to the block NSR calculation are specified in notes 6 through 8.
6. Mineral Resources are estimated using long-term prices of US$3,415/t Zn, US$2,425/t Pb, US$13,775/t Cu, US$65/oz Ag, US$3,500/oz Au and US$265/t pyrite concentrate (>48% sulphur).
7. The following net metallurgical recoveries have been assumed:
   - La Romanera– 78.7% Zn, 52.2% Pb, 41.5% Cu, 93.4% Ag, 89.8% Au, and 86.6% S.
   - El Cura – 67.9% Zn, 0% Pb, 79.4% Cu, 79.8% Ag, 87.4% Au, and 82.7% S.
   - La Infanta – 78.0% Zn, 78.3% Pb, 42.4% Cu, 88.2% Ag, 50.9% Au, and 0% S.
8. The following net payabilities after deductions and penalties have been assumed:
   - La Romanera – 74.6% Zn, 83.4% Pb, 79.0% Cu, 56.9% Ag, 6.7% Au, and 95.1% S.
   - El Cura – 78.4% Zn, 0% Pb, 93.3% Cu, 49.5% Ag, 7.3% Au, and 95.8% S.
   - La Infanta – 83.1% Zn, 83.3% Pb, 52.7% Cu, 66.6% Ag, 18.4% Au, and 0% S.
9. Mineral Resources are inclusive of Mineral Reserves. Mineral Resources that are not Mineral Reserves do not have demonstrated economic viability.
10. Numbers may not add or multiply due to rounding.

1.3.9 Mineral Reserves

The Mineral Reserve estimate for the IBW Project is prepared in accordance with CIM (2014) definitions.

The disclosure of the Mineral Reserve estimate follows the NI 43-101 guidelines and therefore excludes Inferred Mineral Resources. As the Mineral Resource contains Indicated and Inferred material only, with no component in the Measured category, the Mineral Reserve comprises Probable Reserves only.

Mineral Reserves have been estimated for the La Romanera, El Cura, and La Infanta deposits using underground LHOS mining methods, with cemented paste backfill or dry rockfill. Reporting is based on NSR cut-off values of US$69.30/t for La Romanera, US$79.20/t for El Cura, and US$85.30/t for La Infanta.

The Mineral Reserves are reported and summarised in Table 1-5 and have an effective date of July 17, 2026. The reported Mineral Reserves have been used in the preparation of a mining plan, which is supported by a positive cash flow analysis.

The QP is not aware of any mining, metallurgical, infrastructure, permitting, or other relevant factors that could materially affect the Mineral Reserve estimate.

Table 1-5: Summary of Mineral Reserves –July 17, 2026

Deposit	Class	Tonnage Mt	Average Grade						NSR $/t	Contained Metal					
			Zn (%)	Pb (%)	Cu (%)	Ag (g/t)	Au (g/t)	S (%)		Zn (kt)	Pb (kt)	Cu (kt)	Ag (koz)	Au (koz)	S (kt)
La Romanera	Proven	-	-	-	-	-	-	-	-	-	-	-	-	-	-
	Probable	20.4	2.19	1.05	0.38	54	1.13	36.2	189	447	214	77	35.702	738	7,377
El Cura	Proven	-	-	-	-	-	-	-	-	-	-	-	-	-	-
	Probable	1.8	1.23	0.58	1.01	31	1.01	26.3	187	22	11	18	1,794	59	474
La Infanta	Proven	-	-	-	-	-	-	-	-	-	-	-	-	-	-
	Probable	1.2	5.57	3.15	0.77	65	0.25	6.9	195	70	39	10	2,614	10	87
IBW Project	**Proven**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**
	Probable	**23.4**	**2.30**	**1.13**	**0.45**	**53**	**1.07**	**33.85**	**189**	**539**	**264**	**105**	**40,109**	**807**	**7,938**

Notes:

1. CIM (2014) definitions were followed for Mineral Reserves.
2. The reporting approach is based on underground mining using long-hole open stoping with a minimum mining width of 3.0 m, on-site selective flotation of copper, lead, zinc, and pyrite concentrates, and off-site third-party treatment and refining of the flotation concentrates.
3. Mineral Reserves are reported based on underground stope shapes generated using Deswik Stope Optimiser (DSO) and on 3D mine development shapes, which are scheduled and supported by a positive cashflow analysis. Mineral Reserves are stated above NSR cut-off values of US$69.30/t for La Romanera, US$79.20/t for El Cura, and US$85.30/t for La Infanta.
4. Mineral Reserves are estimated using long-term prices of US$2,975/t Zn, US$2,200/t Pb, US$12,120/t Cu, US$55/oz Ag, US$3,000/oz Au and US$215/t pyrite concentrate (>48% sulphur).
5. The NSR values for each block were calculated using the following formulas, with the factors based on consensus long-term metal price forecasts, metallurgical recoveries from available testwork, and market studies used to estimate payable factors, transport, treatment and refining charges:
   - La Romanera – Zn(%)*US$11.80 + Pb(%)*US$5.70 + Cu(%)*US$33.72 + Ag(g/t)*US$0.92 + Au(g/t)*US$5.68 + S(%)*US$2.43
   - El Cura – Zn(%)*US$10.63 + Cu(%)*US$81.37 + Ag(g/t)*US$0.69 + Au(g/t)*US$6.10 + S(%)*US$2.47
   - La Infanta – Zn(%)*US$14.61 + Pb(%)*US$10.93 + Cu(%)*US$18.66 + Ag(g/t)*US$0.98 + Au(g/t)*US$7.85
6. Mineral Reserves account for the following dilution:
   - La Romanera stopes– 11.2% planned dilution, 6.7% unplanned dilution
   - El Cura stopes – 19.4% planned dilution, 16.0% unplanned dilution
   - La Infanta stopes – 20.9% planned dilution, 26.7% unplanned dilution
7. Ore development – 0% dilution
8. Mining recoveries of 95% were applied in long-hole stopes, 80% in sill pillar stopes, and 100% in ore development.
9. Numbers may not add or multiply due to rounding.

1.3.10 Mining Method

Mining at the IBW Project involves extracting ore from the La Romanera, El Cura, and La Infanta deposits via underground mining methods that maximise resource recovery while minimising environmental disturbance. There is a 1 year ramp up period. Thereafter, the mining plan supports a sustainable production rate of 1.2 Mtpa over an 18-year steady-state operating life, followed by 2 years of resource depletion. The pre-production development period lasts approximately 5 years.

Mining operations are centred on the La Romanera deposit, which accounts for approximately 87% of the total Mineral Reserve base. Due to the presence of the Natura 2000 protected area above the La Romanera deposit, access has been designed via a 6.3 km twin decline system originating outside the protected area. The twin decline also provides access to the El Cura deposit, while the La Infanta deposit is accessed via a shorter, independent single decline, as it lies outside the Natura 2000 area.

The twin decline comprises a service decline (for the movement of personnel, equipment, and supplies) and a dedicated material haulage decline to house the Railveyor infrastructure. Railveyor was selected as the primary bulk material handling system for the operation due to its low-cost characteristics over long transportation distances. The twin decline arrangement was selected over a single decline (of larger profile) for advantages in decline development rates, ventilation efficiency, operational flexibility, segregation of mobile equipment from critical Railveyor infrastructure, and emergency egress provisions.

The selected mining method for all deposits is LHOS with cemented paste backfill, or dry rockfill where fill consolidation is not required. LHOS methods were chosen due to the shape, thickness, and orientation of the deposits, as well as the geotechnical competence of the surrounding rock mass.

Two LHOS variants will be employed:

- Transverse stoping in wider mineralised zones (La Romanera only)
- Longitudinal stoping in narrower zones, generally less than 12 m wide (all deposits)

Stopes at La Romanera are designed on a 30 m sublevel interval over a total vertical extent of 660 m. Stope widths are set at 15 m (along strike) over a total east-west extent of 600 m. Transverse stopes are extracted in a primary-secondary mining sequence, with longitudinal stopes mined on retreat towards a consistent access point. Transverse primaries and longitudinal stopes are filled with pastefill, while rockfill is placed in secondaries to reduce binder costs.

La Romanera is mined consistently throughout the LOM plan and is divided into three production horizons to introduce flexibility into the mine schedule and enable the prioritisation of high-value areas of the deposit early in the mine life, thereby maximising project economics. El Cura and La Infanta are introduced into the mine plan sequentially (at limited production rates) to allow equipment and resources to be shared between the operations.

1.3.11 Mineral Processing

The plant is designed to process 1.2 Mtpa using standard comminution and flotation to produce four saleable concentrates: copper, lead, zinc and pyrite.

The ROM feed will be delivered to the ROM stockpile by Railveyors. The ore will be blended by using a FEL, which will feed the jaw crusher operated approximately 12 h/d, 365 days per annum.

The process plant, including SAG mill, ball mill, tower mill, four flotation circuits, and dewatering of concentrates and tailings, will be operated 24 hours per day, 365 days per annum for approximately 8,000 h/a.

1.3.12 Project Infrastructure

The Project is well served by existing infrastructure, benefiting from existing access roads, and grid power availability. In addition, the operational staff will live in the surrounding region, therefore no on-site accommodation is required for the operations team.

Inside the project site boundary, new roads are required for access and have been designed and estimated as 9 m wide gravel roads for two-way traffic.

The following new buildings and supporting infrastructure will be required:

- Access control gate, administration building, lunch and change rooms.
- Laboratory, core logging facility, process plant offices, showers.
- Workshops for heavy and light vehicles, equipment, and auxiliary.
- Helipad near the administration building.
- Incoming 30 kilovolt (kV) power line.
- Water ponds northwest of the process plant for fresh water, recycled water, and storm water.
- A temporary camp will be built for the construction contractors.

Initial discussions with power generation companies in Huelva Province have indicated that the projected maximum steady state power requirements for the IBW Project can be met through existing or planned operations. Puebla de Guzman has benefited from recent infrastructure expansion to support industrial development in the area and now hosts a 220 kV substation.

The Project sits 1 km to 2 km from the Andevalo Reservoir. Emerita currently has a water permit to use water from the reservoir during exploration activities. In addition, the Company has applied for an Industrial Water Permit with the Confederación Hidrográfica del Guadiana which, if granted, would enable the use of 1.51 hm^3 per year (1 hm^3 = 1 x 10^6 m^3). An agricultural water allocation from the Guadiana River of 15 hm^3 exists, of which only 2.3 hm^3 is being utilised. Emerita is actively negotiating access to the unused agricultural water allocation and re-allocation for industrial use should this additional water resource be required.

1.3.13 Market Studies

Emerita commissioned two independent market studies, Cuadri y de la Corte (2025) and Claight (2026), for the base metals' and pyrite concentrates, respectively, expected to be produced by the IBW Project. The studies reviewed market fundamentals, concentrate commercial terms, treatment charges, refining charges, potential realisation routes and concentrate marketability.

The Cuadri y de la Corte (2025) and Claight (2026) reports also assessed prevailing market conditions, long-term supply and demand fundamentals, and the potential impact of deleterious element penalties and other commercial deductions on concentrate sales.

The economic analysis presented herein is based on the Company's long-term consensus metal price forecasts. These price assumptions differ from those used for the Mineral Resource and Mineral Reserve estimates and have been adopted for the purpose of evaluating the Project's long-term economic performance. The metal price assumptions applied in the financial model are summarised in Table 1-6.

Table 1-6: Base Metal Price Assumptions Used in the PFS Financial Model (US$/t).

Price Scenario	Zn (US$/t)	Pb (US$/t)	Cu (US$/t)
Reserve Price	2,975	2,200	12,120
Resource Price	3,415	2,425	13,775
Base Case Long-Term Consensus Price	2,980	2,050	11,470
Sept. Av. Spot Price	4,020	1,871	14,483

The sulphur concentrate price assumptions adopted in the PFS financial model are summarised in Table 1-7.

Table 1-7: Pyrite Concentrate Price Assumptions Used in the PFS Financial Model

Price Scenario	Sulphur Price (US$/t)
Consensus Price	274
Oversupply (Conservative) Price	217
Extended ME Conflict Price	348
Reserves Price	215

Based on the findings of Cuadri y de la Corte (2025), the QP considers the zinc, lead, and copper concentrates expected to be produced from the IBW Project marketable through established smelting and trading networks. Although certain base metal concentrate streams contain elevated levels of deleterious elements that may attract penalties or, particularly in relation to the copper concentrate, limit the number of suitable smelter options, the study identified multiple potential offtakers within the European market. Additionally, significant gold and silver credits contained in the concentrate streams materially enhance concentrate values and support marketability.

Based on the findings of Claight (2026), the QP considers the pyrite concentrate expected to be produced from the IBW Project to be marketable through established sulphuric acid and non-ferrous smelting markets. Demand growth for sulphuric acid and the presence of recoverable precious metals provide support for a positive long-term outlook.

The assumptions applied in the independent market reports are considered reasonable and consistent with current market conditions.

1.3.14 Environmental, Permitting, and Social Considerations

An environmental, permitting, and social assessment was completed by SLR using Project information and specialist studies provided by Emerita. The assessment considered applicable Spanish and EU legislation, the AAU, exploitation and water permitting, relevant good international industry practice, baseline environmental and social conditions, management requirements, and closure obligations.

The Project has been designated as being of Strategic Interest by the Government of Andalusia. The AAU, exploitation permit, water concessions, discharge permit, restoration approval, road and municipal licences, containment pond classification, and land access agreements remain outstanding or under review. Existing permit submissions are based principally on the 2023 Project concept and require reconciliation with the PFS mine plan, infrastructure layout, process mass balance, water-management system, temporary ATEM, IPS, and underground backfill strategy.

Environmental studies identify material considerations associated with regional water stress, seasonal surface water conditions, historical ARD and metal contamination, groundwater characterisation, sulphide-bearing waste rock and tailings, and protection of the downstream Andévalo Reservoir. The Project requires an updated water balance, seasonal surface-water and groundwater baseline data, defined treatment and discharge criteria, and integrated clean-water, contact-water, seepage, and runoff controls.

The Project footprint overlaps the ZEC, although most surface infrastructure is located outside the protected area and only ventilation infrastructure is proposed within it. Updated biodiversity and Natura 2000 assessments are required to confirm avoidance, mitigation, restoration, monitoring, and any compensation measures. Air-quality modelling indicates compliance with applicable limits, and baseline noise levels are consistent with the rural setting, subject to updated design-specific assessment and monitoring.

The mining-waste strategy comprises temporary storage and subsequent underground reuse of suitable waste rock, use of filtered flotation tailings as paste backfill, and controlled surface storage of residual material. Project-specific geochemical, geotechnical, filtration, rheology, strength, and pumpability testing is required to confirm material suitability, facility capacities, backfill specifications, containment systems, and closure requirements.

Social studies indicate generally positive local support associated with employment and regional development, together with material concerns regarding water, environmental performance, permitting, land access, and the legacy of historical mining. Further assessment is required for land tenure and livelihoods, vulnerable groups, community infrastructure, worker influx, human rights, community health and safety, traffic, local employment and procurement, and cultural heritage.

Completion of the ESIA, ESMP, updated specialist studies, permit amendments, stakeholder engagement and grievance arrangements, archaeological controls, occupational and community health and safety plans, and updated closure costs and financial provisions is required before construction.

1.3.15 Capital and Operating Cost Estimates

Capital and operating cost estimates for the IBW Project have been prepared to a PFS level of accuracy and are based on detailed mine plans, process plant designs, infrastructure layouts, vendor quotations, contractor pricing, and benchmark data from comparable operations. The estimates have been developed in flat, real Q2 2026 US dollars.

The total project capital requirement is estimated at US$858.2 million, comprising US$566.7 million of initial capital, US$279.5 million of sustaining capital, and US$12.0 million of closure costs. Initial capital is primarily associated with underground mine development, mobile mining equipment, process plant construction, tailings and water management infrastructure, paste backfill facilities, and supporting site infrastructure.

LOM on-site operating costs are estimated at approximately US$2.03 billion, consisting primarily of mining and processing expenditures, as well as water treatment, waste management, paste backfill, and general and administrative costs. Additional off-site costs associated with concentrate transportation, treatment and refining charges, and concentrate penalties are estimated at approximately US$0.89 billion over the LOM.

On a unit basis, the Project is expected to operate at an average LOM cost of approximately US$86.49/t of ore processed, with mining and processing representing the largest cost components.

Overall, the capital and operating cost estimates reflect a conventional underground mining and flotation operation supported by established processing technologies and infrastructure, and provide a sound basis for the economic evaluation presented in this study.

2.0 Introduction

SLR Consulting Limited (SLR) was retained by Emerita Resources Corp (Emerita or the Company) to prepare an independent Technical Report on the Iberian Belt West (IBW) Project (the IBW Project or the Project), located in the Huelva Province of Andalusia, Spain. The purpose of this Technical Report is to present the results of a Pre-Feasibility Study (PFS) of the Project. This Technical Report conforms to NI 43-101 Standards of Disclosure for Mineral Projects.

Emerita is an exploration and development company focused on the discovery and development of high-grade polymetallic deposits in Spain. Emerita is a Canadian public company and its common shares are listed on the TSX Venture Exchange (TSX-V: EMO).

Emerita holds 100% ownership in the 1,545.6 hectare (ha) IBW Project, which is hosted in the Iberian Pyrite Belt (IPB). Three greenfield polymetallic deposits are located within the Project boundary: La Romanera, La Infanta, and El Cura. After the 1 year ramp up of production, the mining is envisaged as underground long-hole open stoping (LHOS) and supports a sustainable production rate of 1.2 million tonnes per annum (Mtpa) over an 18-year steady-state operating life, followed by 2 years of resource depletion. The pre-production development period lasts approximately 5 years. The saleable products produced at the Project are copper, lead, zinc, and pyrite concentrates, together with payable gold and silver by-products.

The effective date of the Mineral Resource and Mineral Reseve estimates in the Technical Report is July 17, 2026. Other information in this report is current as of the effective date of October 8, 2026.

2.1 Sources of Information

A site visit was carried out by SLR QPs Frank Browning (CGeol), and Christopher Penna (CEng) on January 21, 2026. During the site visit, the QPs:

- Examined drillhole core;
- Reviewed core logging, sampling, quality assurance and quality assurance / quality control (QA/QC) procedures;
- Discussed the geological setting of the deposits and the geological interpretations with the site geologist;
- Toured the IBW Project area including the proposed processing plant area and current drilling operations;
- Reviewed site access and the proposed location of key infrastructure; and
- Held discussions with key personnel at Emerita’s offies in Seville.

Frank Browning has also completed a further three site visits (March 16, 2023, May 3-5, 2023, February 10-12, 2025) and included the following inspections:

- Extent of exploration work completed to date;
- Review of drill core logging, sampling, sample preparation, analysis, and QA/QC procedures;
- Inspection of the core logging, sampling, and storage facilities;
- Inspection of drilling sites and operations;

- Inspection of selected drill core to confirm the nature of the mineralisation and the geological descriptions; and
- Inspection of geology and mineralisation at the La Romanera, La Infanta, and El Cura surface outcrops and historical workings.

During the site visit and in meetings throughout the study, discussions were held with personnel from Emerita, including:

- Joaquín Merino-Márquez, P.Geo., CEO & President, Emerita Resources
- Danniel Oosterman, P.Geo., Project Director, Emerita Resources
- Ian Hardesty, AIPG, Vice President Exploration, Emerita Resources
- Antonio Escribano Segovia, Director Infrastructure, Energy & Logistics, Emerita Resources

Table 2-1 presents a summary of the QPs responsibilities for this Technical Report.

Table 2-1: Qualified Persons and Responsibilities

QP, Designation, Title	Company	Responsible for
Frank Browning (MSc, FGS, CGeol), Principal Resource Geologist	SLR	Section 1.1.1.1, 1.1.2.1,1.3.1-6,1.3.8; Section 4-12; Section 14; Section 25.1; Section 26.1
James W.G. Turner (MCSM, MIMMM, CEng), Technical Director, Mineral Processing	SLR	Section 1.1.1.3, 1.1.2.3,1.3.7; Section 13; Section 24; Section 25.3; Section 26.3
Christopher Penna (CEng), Associate Director, Mining & Mineral Resources	SLR	Section 1.1.1.2, 1.1.2.2,1.3.9, 1.3.10; Section 15; Section 16.2-5, 16.7-9; Section 25.2; Section 26.2
Liam Alexander Johnson (RPEQ, MAusIMM CP (Geotech)), Senior Consultant – Rock Mechanics	SLR	Section 16.1
Christopher Paul Stinton (CEng IMMM), Principle Process Engineer, Zenito Limited	Zenito Limited	Section 1.1.1.4, 1.1.2.4, 1.3.12; Section 17, Section 18 (excl 18.5); Section 25.4; Section 26.4
Arturo Gutierrez del Olmo (PhD. (Mining), Eur Ing, MIMMM) Technical Director, Mine Waste Engineering	SLR	Section 16.6; Section 18.5;

QP, Designation, Title	Company	Responsible for
Alison Brianna Allen, (BSc, MSc, CEnv, FIMMM, MISEP) EU Regional Sector Lead – Environmental and Social Impact Assessments	SLR	Section 1.1.1.5, 1.1.2.5, 1.3.14; Section 20; Section 25.5; Section 26.5.
Veronika Luneva (MAusIMM, MSc, IMC (CFA UK Level 4)), Mining Finance Specialist	SLR	Section 1.1.1.6, 1.1.2.6, 1.3.15; Section 21 Section 22; Section 25.6; Section 26.6.

The documentation reviewed, and other sources of information, are listed at the end of this Technical Report in Section 27 References.

2.2 Acknowledgements

The QPs acknowledge the contributions of other team members from SLR that have assisted in the completion of this Technical Report, including Beth Payne, Principal Mining Analyst; Bryan Pullman, Technical Director Mining; Alan Clarke, Technical Director – Resource Geology; Xander Gwynn, Technical Director Mining Geotechnics; Thomas Penhall, Project Mining Engineer; Charles Peek Associate Director Hydrogeology, Beth Candy, Technical Director International Environmental & Social Impact Assessment, and Nicky Vlok Senior Project Manager.

2.3 List of Abbreviations

Units of measurement used in this Technical Report conform to the metric system. All currency in this Technical Report is US dollars (US$) unless otherwise noted.

Table 2-2: Abbreviations for Units

µ	micron	kvar	kilovolt-amperes reactive
µg	microgram	kW	kilowatt
a	annum	kWh	kilowatt-hour
A	ampere	L	litre
bbl	barrels	lb	pound
Btu	British thermal units	L/s	litres per second
°C	degree Celsius	m	metre
C$	Canadian dollars	M	mega (million); molar
cal	calorie	m^2	square metre
cfm	cubic feet per minute	m^3	cubic metre
cm	centimetre	MASL	metres above sea level
cm^2	square centimetre	m^3/h	cubic metres per hour
d	day	mi	mile
dia	diameter	min	minute
dmt	dry metric tonne	µm	micrometre
dwt	dead-weight ton	mm	millimetre
°F	degree Fahrenheit	mph	miles per hour
ft	foot	MVA	megavolt-amperes
ft^2	square foot	MW	megawatt
ft^3	cubic foot	MWh	megawatt-hour
ft/s	foot per second	oz	Troy ounce (31.1035g)
g	gram	oz/st, opt	ounce per short ton
G	giga (billion)	ppb	part per billion
Gal	Imperial gallon	ppm	part per million
g/L	gram per litre	psia	pound per square inch absolute
Gpm	Imperial gallons per minute	psig	pound per square inch gauge
g/t	gram per tonne	RL	relative elevation
gr/ft^3	grain per cubic foot	s	second
gr/m^3	grain per cubic metre	st	short ton
ha	hectare	stpa	short ton per year
hp	horsepower	stpd	short ton per day
h	hour	t	metric tonne
Hz	hertz	tpa	metric tonne per year
in.	inch	tpd	metric tonne per day
in^2	square inch	US$	United States dollar
J	joule	USg	United States gallon
k	kilo (thousand)	USgpm	US gallon per minute
kcal	kilocalorie	V	volt
kg	kilogram	W	watt
km	kilometre	wmt	wet metric tonne
km^2	square kilometre	wt%	weight percent
km/h	kilometre per hour	yd^3	cubic yard
kPa	kilopascal	yr	year

Table 2-3: Abbreviations for Acronyms

Acronym	Definition
1VD	first vertical derivative
3D	three-dimensional
AACE	Association of the Advancement of Cost Engineering
AAU	Unified Environmental Authorisation or *Autorización Ambiental Unificada*
Ag	silver
Ai	bond abrasion index testing
ANFO	ammonium nitrate fuel oil
ARD	acid rock drainage
ARO	asset retirement obligation
As	arsenic
ATEM	mine waste storage facility (*Acopio Temporal de Estériles de Mina*)
Au	gold
Ba	barium
Bi	bismuth
BIC	Bien de Interés Cultural
BOO	Build-Own-Operate
BWi	bond ball mill work index
CAPEX	Capital Expenditures
CCD	counter-current decantation
Cd	cadmium
CHSP	Community Health and Safety Plan
Cl	chlorine
CIM	Canadian Institute of Mining, Metallurgy and Petroleum
CIT	Spanish Corporate Income Tax
CPGHA	General Catalogue of Andalusian Historical Heritage
CRF	cemented rockfill
CRM	certified reference materials
CRMA	*Critical Raw Materials Act*
Cu	copper
DBR	drop board regulator
DDH	diamond drilling
DHEM	downhole electromagnetics
DSI	Declaration of Strategic Interest
DSO	Deswik Stope Optimiser
E&S	environmental and social
EBITDA	earnings before interest, taxes, depreciation,and amortisation
EBRD PR	European Bank for Reconstruction and Development Performance Requirements
EHS	Environmental, Health and Safety
EIA	environmental impact assessment
EITI	Extractive Industries Transparency Initiative
ELOS	equivalent linear overbreak sloughing
EPCM	Engineering, Procurement and Construction Management)
EPR	Emergency Preparedness and Response
ESIA	Environmental and Social Impact Assessment
ESMP	Environmental and Social Management Plan
F	fluorine
Fe	iron
FEL	front-end loader
FW	footwall (lithological domain)
G&A	general and administrative

Acronym	Definition
GHG	greenhouse gas
GIIP	Good International Industry Practice
GISTM	Global Industry Standard on Tailings Management
HARD	half absolute relative difference
HCI	Habitat of Community Interest
HDPE	high-density polyethylene
Hg	mercury
HPGR	high pressure grinding rolls
HW	hanging wall (lithological domain)
JSA	Job Safety Analysis
ICMM	International Council on Mining and Metals
ICP-AES	inductively coupled plasma atomic emission spectrometry
ICP-MS	inductively coupled plasma mass spectrometry
IDW2	Inverse distance weighting squared
IFC PS	International Finance Corporation Performance Standards
IFI	International Financial Institution
IFRS	International Financial Reporting Standards
IGME	Geophysics Branch of the Spanish Geological and Mining Survey
ILO	International Labour Organization
IP	induced polarisation
IPS	Integrated Process Residue Storage Facility (*Instalación de Pasta Seca*)
IRR	internal rate of return
ITC	Technical Instructions
IUCN	International Union for Conservation of Nature
LCT	locked cycle tests
LHD	load-haul-dump
LG	low-grade (tables and figures)
LHOS	long-hole open stoping
LOM	life-of-mine
LOTO	Lock-out/Tag-out
LRP	Livelihood Restoration Plan
MRE	Mineral Resource estimate
MS	massive sulphide (in tables and figures)
MSO	mineable stope optimiser
N’	Stability Number
NAL	Neutral Albion Leach
NN	nearest neighbour
NSR	net smelter return
NPV	net present value
OEM	original equipment manufacturer
OHS	occupational health and safety
OK	ordinary kriging
OPEX	Operational Expenditures
ORE	orebody (lithological domain)
Pb	lead
PFS	Pre-Feasibility Study
PFP	Post-Flotation Process
PI	Profitability Index
PLC	programmable logic controller
PLT	Point Load Testing
PM	particulate matter
PPE	personal protective equipment

Acronym	Definition
PRV	pressure reduction valve
pXRF	portable X-ray fluorescence
QA/QC	quality assurance and quality control
QKNA	Quantitative Kriging Neighbourhood Analysis
QP	Qualified Person
RAR	return air raise
Rb	rubidium
REE	rare earth elements
RMR	rock mass rating
ROM	run of mine
RPEEE	reasonable prospects for eventual economic extraction
RQD	rock quality designation
S	sulphur
SAG	semi-autogenous grinding
Sb	antimony
SCADA	supervisory control and data acquisition
SEP	Stakeholder Engagement Plan
SIPNA	Andalusian Natural Heritage Information System
SLO	Social Licence to Operate
SMBS	sodium metabisulphite
SMC	SAG Mill Comminution
SMP	stirred media detritor
SMS	semi-massive sulphide (in tables and figures)
Sn	tin
Sox	sulphide oxidation
SWMS	Safe Work Method Statements
TC/RC	treatment and refining charges
TDS	total dissolved solids
TEM	transient electromagnetics
TMI	total magnetic field intensity
TSO	Transmission System Operator
TSP	total suspended particles
TSS	total suspended solids
U	uranium
UCS	unconfined compressive strength
UFG	ultra-fine grinding
XRF	X-ray fluorescence
VFD	variable frequency drives
VOD	Ventilation on Demand
VSD	variable speed drive
WAD	weal acid dissociable
WBG EHS	World Bank Group
WHO	World Health Organisation
ZEC	Special Area of Conservation (ZEC in Spanish
Zn	zinc

3.0 Reliance on Other Experts

This Technical Report has been prepared by SLR for Emerita. The information, conclusions, opinions, and estimates contained herein are based on:

- Information available to SLR at the time of preparation of this Technical Report.
- Assumptions, conditions, and qualifications as set forth in this Technical Report.

For the purpose of this Technical Report, SLR has relied on ownership information provided by Emerita. This information is relied upon in Section 4.0 and related disclosure in Section 1.0. SLR has not researched property title or mineral rights for the Project and expresses no opinion as to the ownership status of the property.

SLR has relied on Emerita for guidance regarding the financial and fiscal assumptions applied in the economic evaluation, including applicable taxes, the absence of royalties and other government levies or interests. Emerita also provided guidance related to key project-specific inputs, including commodity price assumptions, concentrate payable terms, treatment and refining charges (TC/RC), transportation and handling costs, deleterious element penalties and associated costs, G&A costs, owner's costs, closure and reclamation costs, and off-site infrastructure capital requirements. These assumptions have been incorporated into the financial model and economic analysis. This information is relied upon in Section 4.0, 21.0, 22.0 and related disclosure in Section 1.0.

SLR has not independently verified marketing information and smelter terms for copper, lead, zinc and pyrite concentrates. SLR has relied upon information from market studies commissioned by Emerita through the following documents:

- Cuadri y de la Corte, 2025. Commercial Options for the Emerita IBW Polymetallic Ores, dated June 15, 2025.
- Claight (2026). Global Pyrite Concentrate Market Study, dated June 2026.

This information has been used in Section 19.0 of this report. It is also used in support of the Mineral Resource estimate in Section 14.0, Mineral Reserve estimate in Section 15.0 and economic analysis in Section 22.0.

SLR has relied on Railveyor for the assessment and cost for the mine material handling. The Railveyor design is detailed in Section 16.7.3.1.

Except for the purposes legislated under provincial securities laws, any use of this Technical Report by any third party is at that party's sole risk.

SLR has relied upon hydrogeological and hydrological information provided by FRASA Engineering Consultants (FRASA) in the preparation of Section 16.2 of this Technical Report. The information was obtained from the following reports:

- FRASA Engineering Consultants (2026). *Estudio del Estado de Base Hidrologica e Hidrogeologica RBH*. Dated March 2026.
- FRASA Engineering Consultants (2026). *Study of the Hydrological and Hydrogeological Baseline. Technical Note 01*. Dated July 2026.

SLR has not independently verified the underlying field data provided by FRASA. The information has been used to support the hydrogeological assessment presented in Section 16.2 of this Technical Report.

4.0 Property Description and Location

4.1 Location

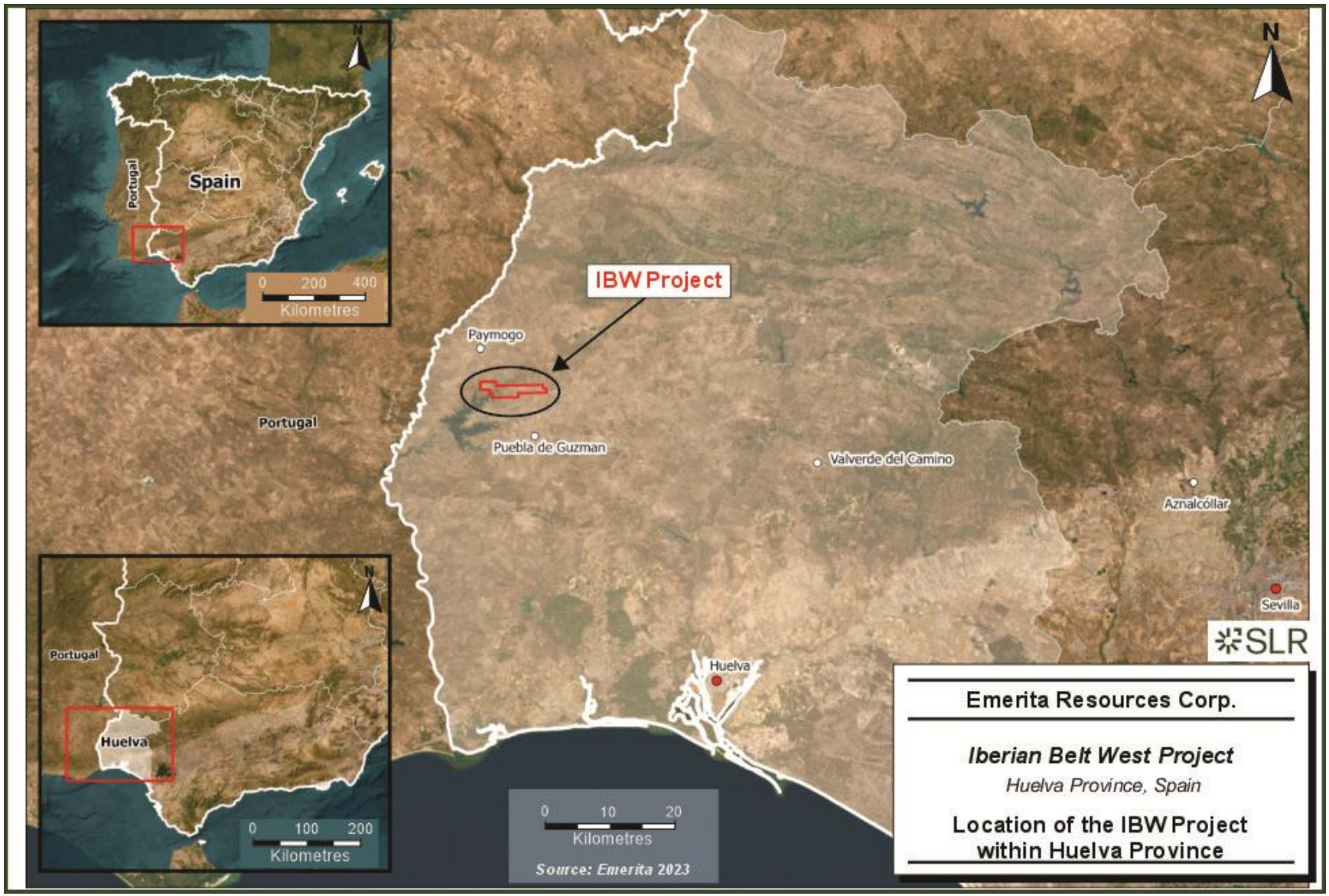
The IBW Project is located in southwest Spain within the Huelva Province of Andalusia (Figure 4-1). The Project is situated approximately 500 km southwest of Madrid (Spain's capital), 142 km west of Seville (capital of Andalusia), 61 km northwest of Huelva City (capital of Huelva Province), and 9 km east of the Spanish/Portuguese border. Huelva City is the political and administrative centre of Huelva Province.

Two small towns, Puebla de Guzman (approximately 3,500 inhabitants) and Paymogo (approximately 1,500 inhabitants), are within 10 km of the property (Figure 4-2). Approximately 80% of the property lies within the Municipality of Puebla de Guzman and the remainder within the Municipality of Paymogo.

Figure 4-1: Map of Spain Highlighting the Huelva Province of Andalusia



Figure 4-2: Location of the IBW Project Within Huelva Province



4.2 Ownership

Emerita holds 100% ownership of the IBW Project. The mineral rights and exploration permit of the IBW Project were acquired by its subsidiary, Emerita Resources España SLU, by public tender. On September 1, 2020, Emerita was officially notified through a resolution by the Provincial Secretary of the Regional Ministry of Industry in Huelva that it had won the public tender; on the same date of the public tender acquisition, Emerita applied for an exploration permit for the IBW Project.

4.3 Mineral Tenure

The IBW Project exploration permit was granted for a period of 26 months on July 12, 2021, with the option to renew for a further 3 years. On September 9, 2023, Emerita Resources España SLU applied to the *Delegación Territorial de Energia y Minas* in Huelva Province*, Junta de Andalucia* (the Junta) for an exploitation permit for the IBW Project. The exploitation permit application covers the same area as the existing IBW Project exploration permit.

On May 13, 2026, Emerita was notified that the Unified Environmental Authorisation (AAU or *Autorización Ambiental Unificada*) for the IBW Project exploitation permit application had advanced to the public consultation stage. Emerita expects the public consultation to be completed in Q1 2027, after which the Junta can rule on the exploitation permit application.

Exploitation permits in Spain, when granted, have a 30 year term and can be extended for two subsequent 30 year periods. During the time that the IBW Project exploitation permit application is being reviewed by the Junta, Emerita's rights under its existing exploration permit are extended, allowing ongoing exploration programmes.

Exploration permit details are provided in Table 4-1 and a map of the boundary is shown in Figure 4-3. In Spain, exploration permits are granted only over a defined block, made up of square grid cells or *cuadrícula minera*, as described in Law 75 of Spanish Mining Law (*Ley 22/1973, de 21 de julio, de Minas*). These must be contiguous with no gaps, and the outside boundary which encloses these cells will collectively comprise the boundary for a permit. The IBW Project exploration permit covers 51 cells, totalling 1,545.6 ha, and is bounded by the coordinates listed in Table 4-2. The permit is broadly rectangular, extends in an east-west direction for approximately 18 km, and covers the La Romanera, La Infanta, and El Cura deposits.

Table 4-1: IBW Project Exploration Permit Details

Permit Number	Tenure	Company	Application Date (DD/MM/YYYY)	Grid Cells	Area (ha)	Date Granted (DD/MM/YYYY)	Expiration Date
15029	Section C[1]	Emerita Resources España SLU	01/09/2020	51	1,545.6	12/07/2021	([2])

Source: Emerita 2023.

Notes:

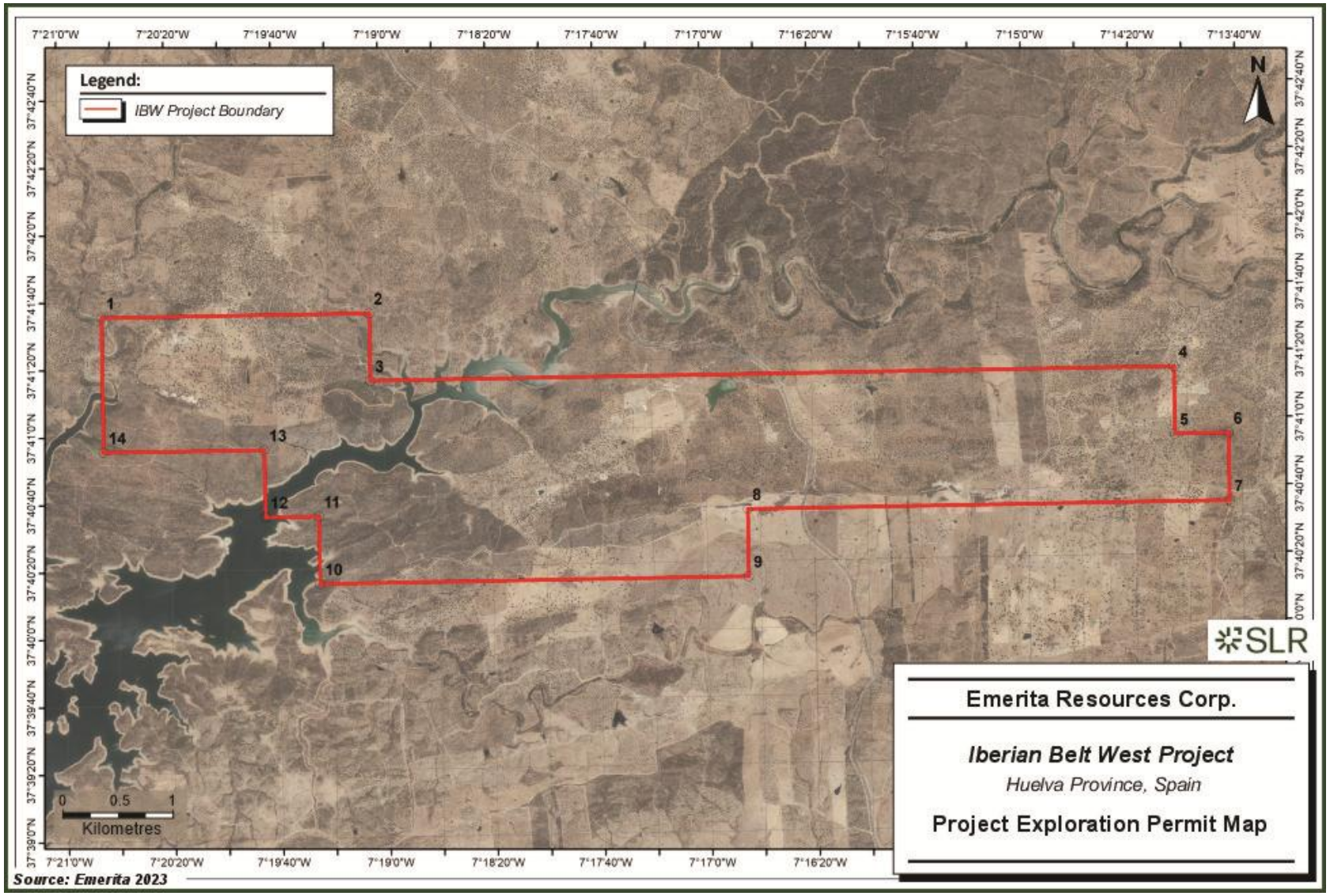
1. Section C covers non-energy mining, which comprises all mineral deposits and geological resources.
2. 2857/1978 of August 25 – General Regulations for the Mining Regime Article 88.1 states "as soon as the investigation sufficiently demonstrates the existence of a resource or resources from Section C, and always within the validity period of the exploration permit, the holder may apply for an exploitation concession over all or part of the land within the exploration perimeter. Exploration permits shall be considered extended for the duration of the processing of the concession granting procedure."

Table 4-2: IBW Project Exploration Permit Coordinates (ETRS89 Zone 29N)

ID Point	Longitude (W)	Latitude (N)	X (UTM)	Y (UTM)	UTM Zone
1	7° 20' 44.89" W	37° 41' 35.5009" N	645842.237	4173062.688	29
2	7° 19' 4.8898" W	37° 41' 35.5004" N	648291.446	4173106.282	29
3	7° 19' 4.8899" W	37° 41' 15.5001" N	648302.510	4172489.838	29
4	7° 14' 4.8883" W	37° 41' 15.499" N	655650.768	4172624.991	29
5	7° 14' 4.8884" W	37° 40' 55.4987" N	655662.377	4172008.541	29
6	7° 13' 44.8882" W	37° 40' 55.4987" N	656152.303	4172017.785	29
7	7° 13' 44.8885" W	37° 40' 35.4983" N	656163.947	4171401.335	29
8	7° 16' 44.8899" W	37° 40' 35.4989" N	651754.312	4171319.197	29
9	7° 16' 44.89" W	37° 40' 15.4986" N	651765.626	4170702.751	29
10	7° 19' 24.8904" W	37° 40' 15.4993" N	647845.705	4170631.732	29
11	7° 19' 24.8902" W	37° 40' 35.4996" N	647834.682	4171248.175	29
12	7° 19' 44.8902" W	37° 40' 35.4997" N	647344.731	4171239.428	29
13	7° 19' 44.89" W	37° 40' 55.5" N	647333.742	4171855.871	29
14	7° 20' 44.89" W	37° 40' 55.5003" N	645864.000	4171829.805	29

Source: Emerita 2023.
Note: The delimitation of the exploration permit was made in the ED50 (European Datum 1950) coordinate system.

Figure 4-3: Project Exploration Permit Map (ETRS89 Zone 29N)



Note: For coordinates of numbered ID points, refer to Table 4-2.

4.3.1 Concession Fees

Mining in Spain is regulated by the Ministry of Industry under the Spanish Mining Law and royal decree. To keep the exploration permit in good standing, Emerita must pay annual concession fees based on the size of the permit and fulfil the exploration investment requirements. The annual concession fees for the IBW Project are €1,319 per year based on the 51 IBW Project claims.

4.4 Royalties

No other mining-specific royalty or tax applies to the Spanish mining industry.

4.5 Surface Rights

Mineral rights and surface land rights are separate under the Spanish Mining Law. In case of a conflict between the owner of the surface land rights and the owner of the mineral rights, the Spanish Mining Law applies a temporary surface occupation (*expropiación temporal de territorio*), allowing the mineral rights owner to access the land to carry out exploration work.

Emerita has access agreements with local landowners covering the main exploration area. These agreements allow Emerita to conduct surface exploration and prospecting in exchange for nominal monetary compensation.

4.6 Permitting Considerations

Permits required for exploration works to be carried out by Emerita were granted by the Mining Department in Huelva. Emerita submitted a Restoration Plan on February 10, 2021. The Restoration Plan was on public display until March 26, 2021, approved on July 12, 2021, and was valid until September 12, 2023. During the time that the IBW Project exploitation permit application is being reviewed by the Junta, Emerita's rights under the current exploration licence for the Restoration Plan are extended.

In areas with environmental protection, an AAU is required as part of permit applications. The AAU requires Emerita to prepare and submit an environmental impact assessment (EIA), including an archaeological study and an urban compatibility study, issued by the municipal councils. The AAU is approved by the Environmental Department, which indicates favourability to the Mining Department.

Environmental permitting affects the three exploration deposit areas as follows (Figure 4-4):

- La Infanta: Area free of environmental protection zones, where AAU is required, it is outside of the ZEC and therefore fewer restrictions apply to La Infanta.
- El Cura: Andévalo Occidental Special Area of Conservation (*Zona de Especial Conservación*, ZEC), which requires an AAU.
- La Romanera: Andévalo Occidental Special Area of Conservation (*Zona de Especial Conservación*, ZEC) and area of cultural interest and forestry (*Dehesa Paymogo)*, which requires an AAU.

An AAU for exploration at La Romanera and El Cura (AAU/HU/075/2021) was approved on May 6, 2023, and remains valid for the duration of exploration activities while they remain permitted. Every 6 months, the administration is informed through a report demonstrating compliance with the obligations established in the AAU.

The AAU includes authorisations to develop new access routes and area designations for drilling platforms, with any changes being notified by written notice and authorised by the Huelva Mining Delegation (*Delegación de Minas de Huelva*). Waste management is also authorized under the AAU and is delegated by Huelva Environmental Prevention Department (*Departamento de Prevención Ambiental de Huelva*). Emerita has also secured water concessions from the Guadiana River Basin Authority (*Confederación Hidrográfica del Guadiana, CHGD*) for its exploration activities. In the permit-granting resolution for the Restoration Plan, the Mining Department established a restoration bond of €146,000 to ensure the proper restoration of the authorised drilling platforms. Of the amount initially deposited, €70,000 has already been recovered due to the restoration work carried out to date.

Project permitting, including the ongoing exploitation permit application and associated AAU, is described in Section 20.0.

4.7 Environmental Considerations

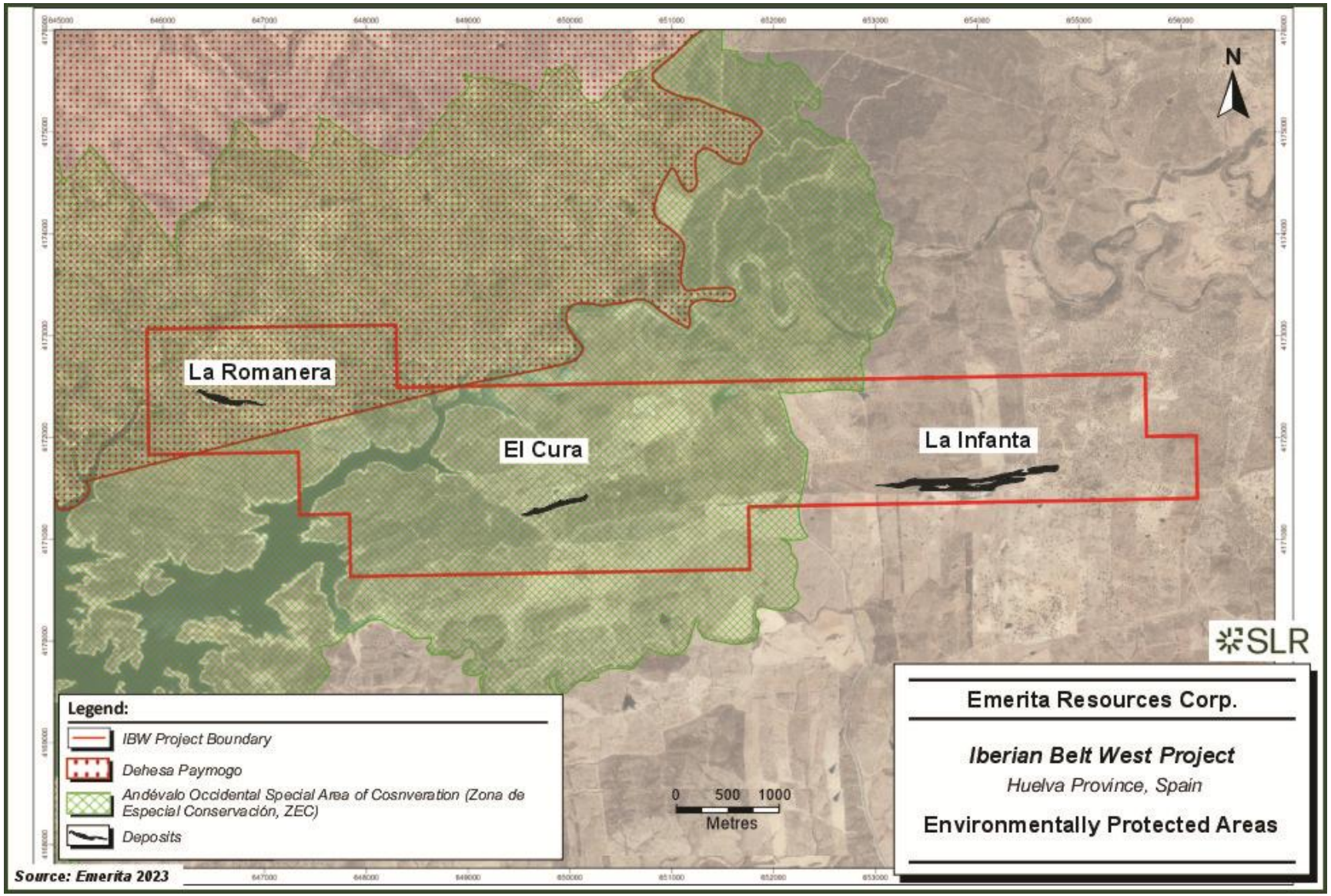
Continuous environmental control and monitoring of the disturbance and remediation of drill sites are carried out during drilling operations.

An environmental baseline study has been developed for the IBW Project comprising the following works:

- Natural environment and landscape baseline carried out by specialist ecologists;
- Soil and water analytical research (surface and groundwater) by the Spanish National Accredeitation Body (*Entidad Nacional de Acreditación,* ENAC);
- Hydrological and hydrogeological study (water balance) by specialist hydrogeologists;
- Pollutant dispersion study; and
- Environmental noise level study.

Further details of environmental studies completed to date are provided in Section 20.0.

Figure 4-4: Environmentally Protected Areas



4.8 Existing Environmental Liabilities

The three known IBW Project deposits are La Romanera, El Cura, and La Infanta. All contain remnants of historical exploration and mining, characterised by old shafts, pits, trenches, and rock dumps. The rock dumps have a reddish-orange colour due to the oxidation of pyrite and other iron sulphides (Figure 4-5). For exploration permits, including the active permit for the IBW Project, existing environmental liabilities are not considered in the Spanish Mining Law. Such obligations will only be incurred should a project progress to a mining phase when exploration permits are upgraded to exploitation permits. No other type of environmental liability has been identified at the property.

An estimation of the historical rock dumps carried out by Emerita indicates approximate volumes of 200,000 m^3 (La Romanera), 40,000 m^3 (La Infanta), and 20,000 m^3 (El Cura), totalling 260,000 m^3 of oxidised rock dumps. Emerita will consider the remediation of the historical rock dumps as part of potential environmental improvements to the area. In the event of moving to the exploitation phase, remediation measures would be considered, and the costs would be assessed.

Figure 4-5: Historical Surface Workings at La Romanera



Source: Emerita 2023.

The QP is not aware of any other environmental liabilities on the property. Emerita has all required permits to conduct the proposed work on the property. The QP is not aware of any other significant factors and risks that may affect access, title, or the right or ability to perform the proposed work program on the property.

5.0 Accessibility, Climate, Local Resources, Infrastructure and Physiography

5.1 Accessibility

The IBW Project can be accessed by road from several major cities in southwest Spain, notably from Seville via the A-49 freeway (152 km) and Huelva via the A-495 Regional Road (71 km), shown in Figure 5-1.

Seville is connected to the main cities in Spain by domestic flights and high-speed rail services, and with the rest of Europe by an international airport. Huelva has a commercial port from which products from mining in the region can be shipped.

The closest towns to the IBW Project are Puebla de Guzman and Paymogo, with access by paved provincial road HU-5401. The Project sits between these two towns (Puebla de Guzman to the south and Paymogo to the north), which are separated by 18 km. Puebla de Guzman is 142 km from Seville, with travel time of approximately two hours by car. From Puebla de Guzman to the Project is a further 8.5 km north on the HU-5401, which crosses the project site between the El Cura and Infanta deposit areas, adjacent to the proposed processing plant site (Figure 5-2). Access within the project area is via all-weather gravel roads.

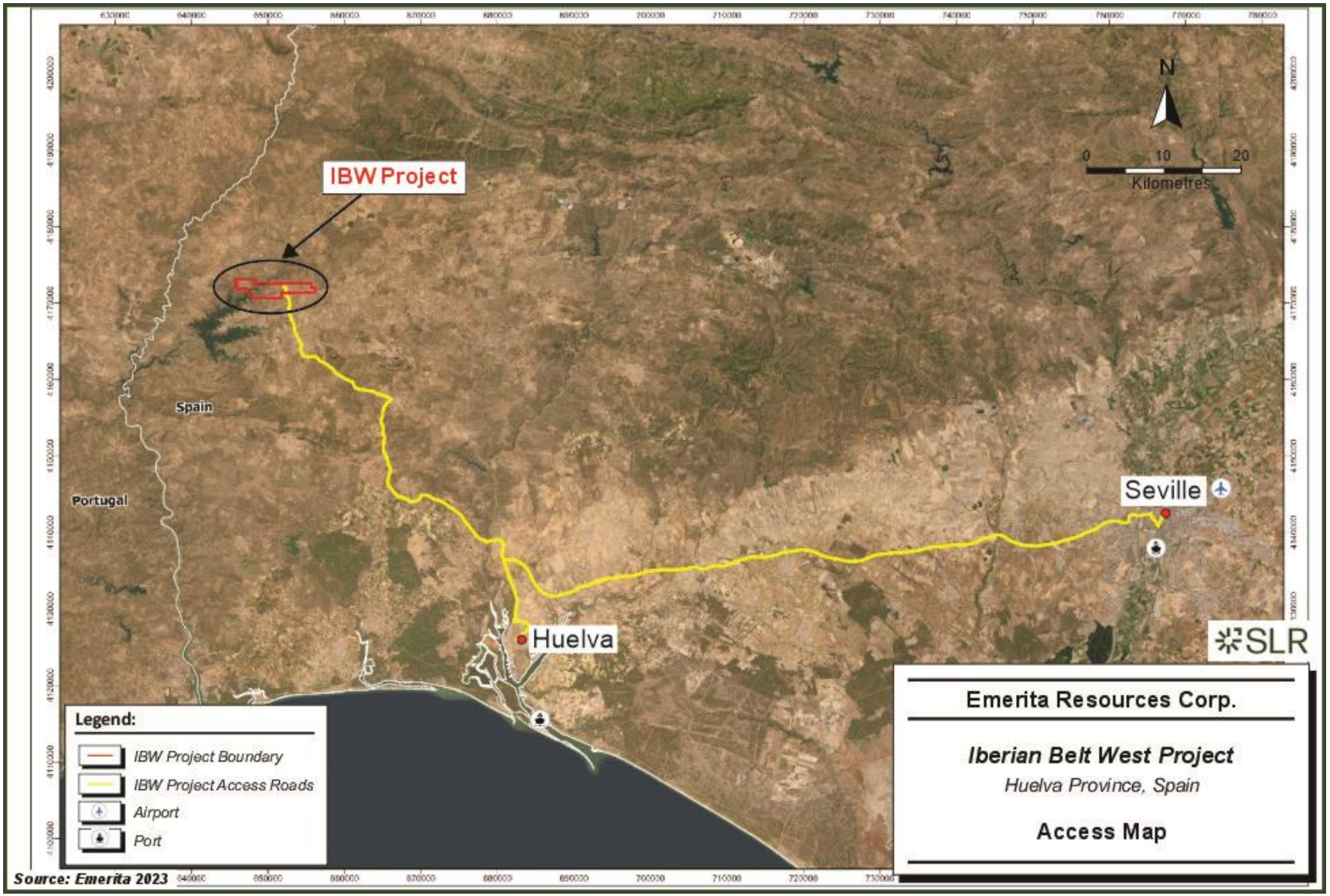
5.2 Climate

The IBW Project is located within a Mediterranean climate regime, categorised as Csa under the Köppen-Geiger system (hot summer Mediterranean climate). Temperatures vary throughout the year, with an average of 9.1°C in January and 27.1°C in July in 2022. A minimum temperature of 0.1°C was recorded in January, and a maximum of 39.9°C in July.

Annual rainfall averages between 500 mm and 600 mm, with minimal rainfall during the summer months (lowest measured rainfall in July) and peak rainfall between October and December, measuring roughly 70 mm to 90 mm per month. The region experiences periods of high evapotranspiration and summer droughts, typical of inland Andalusia.

Exploration operations can be conducted year-round and any future mining and processing operations are also expected to be conducted year-round.

Figure 5-1: IBW Project Access Map



5.3 Local Resources and Infrastructure

5.3.1 Introduction

The Andalusian Region is connected by a well-developed transport network, reliable energy and water supply, high-speed communication systems, and all the services of modern cities such as Huelva, Seville, and Cordoba. The area has a longstanding history of mining and resource development, including active production at Sandfire's MATSA Copper Operations and Atalaya Mining's Riotinto Project. This section describes existing local resources and infrastructure only. Planned IBW Project infrastructure is outlined in Section 18.0.

5.3.2 Labour and Skills

The two neighbouring towns of Paymogo and Puebla de Guzman represent potential sources of labour, accommodation, and general services. The population of Andalusia is highly educated, with access to Andalusian universities or other universities in Spain. The University of Huelva has active geology and engineering departments.

5.3.3 Power

Emerita has engaged in discussions with numerous existing power-generating companies in Huelva Province and with stakeholders involved in power projects currently in the permitting stage, all of which are situated in proximity to the Project. The Company is not permitted to disclose details surrounding these discussions; however, these suppliers have indicated that the projected maximum steady state power requirements for the IBW Project can be met through their existing or planned power generation operations.

The Transmission System Operator (TSO) for Spain's high power transmission grid (220 kV and 400 kV) is Red Eléctrica de España. Red Eléctrica de España is 20% nationally owned; the company does not generate electricity; it solely manages the distribution of power in Spain. Spain abides by the EU's unbundled energy rules where generation, transmission, and distribution are all separately managed, designed to ensure no single entity has control over the entire energy supply chain. Puebla de Guzman has benefited from recent infrastructure expansion by Red Electrica de Espana to support industrial development in the area and now hosts a 220 kV substation owned by the distributor, which is sufficient to meet the demands of mining operations in the area.

5.3.4 Water

The Project sits 1 km to 2 km from the Andevalo Reservoir. Emerita currently has a water permit to use water from the reservoir during exploration activities. In addition, the Company has applied for an Industrial Water Permit with the Confederación Hidrográfica del Guadiana which, if granted, will be effective in 2028 and subject to renewal every 5 years. Possessing this permit will grant Emerita a volume of 1.51 hm^3 per year (1 hm^3 = 1 x 10^6 m^3) under the 2028–2033 Water Management Plan to be sourced from the greater Andévalo Reservoir (water body ES040MSPF000206510).

An agricultural water allocation from the Guadiana River of 15 hm^3 exists of which only 2.3 hm^3 is being utilised. Unused allocation by the agricultural community (*comunidad de regantes*) within this allocation can be used for industrial purposes, but a company must receive permission from the agricultural community in order to do so. Emerita is actively negotiating access with the agricultural community to secure a portion of the agricultural water allocation to

ensure industrial water supply during the interim between the present and the expected granting of the Industrial Water Permit allocation in January 2028. These negotiations are ongoing at the time of this report. Emerita has all the necessary water permits to complete its ongoing exploration activities, as they fall under the permissions granted by the AAU for these activities.

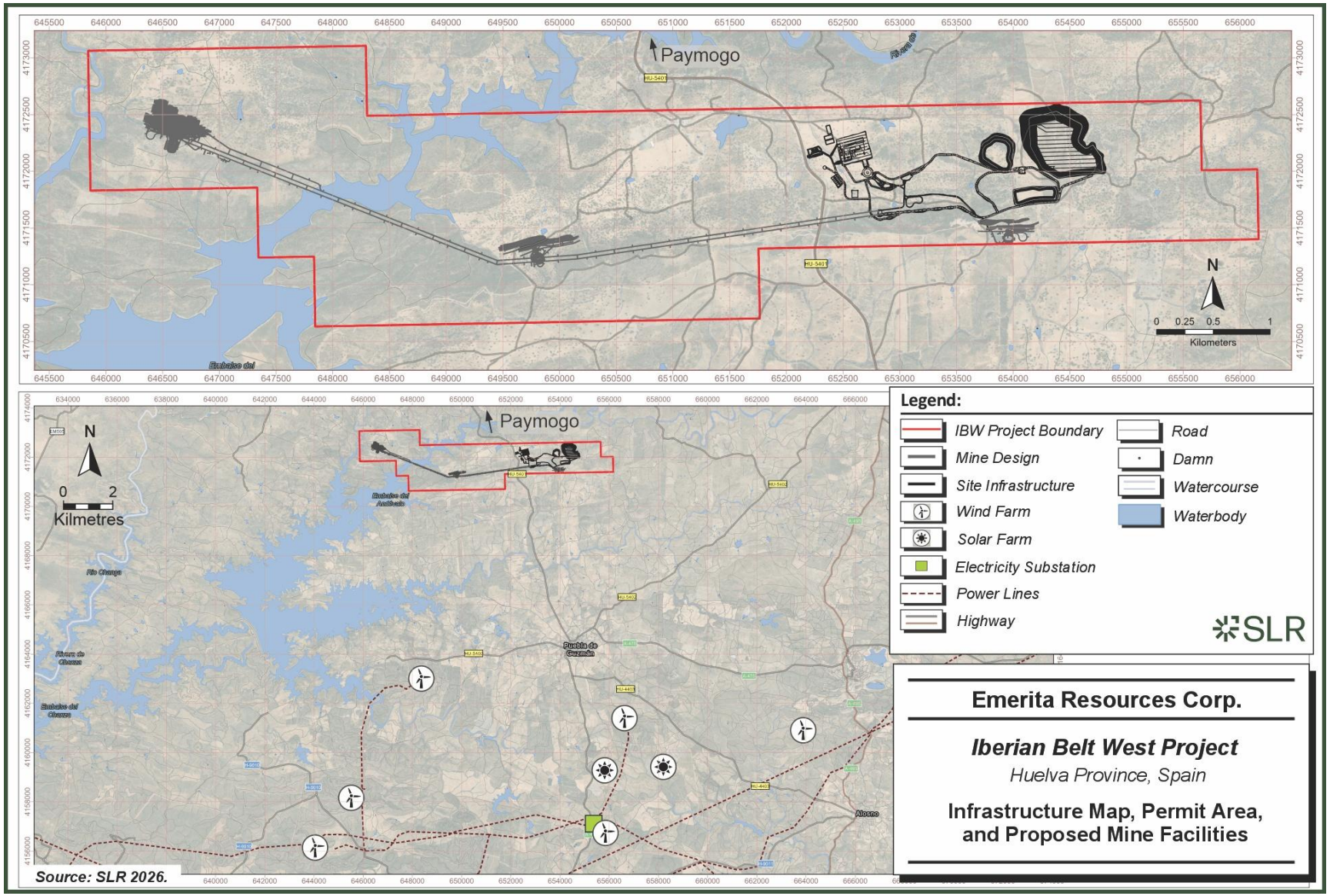
5.3.5 Infrastructure Areas

The potential exploitation permit area, if approved, is sufficient for the development of infrastructure to sustain a mining operation. Potential sites for tailings storage, waste rock disposal, and processing facilities are available in the La Infanta area, which is outside of the environmental protection zones outlined in Section 4.6.

5.4 Physiography

The project area is characterised by undulating topography with elevations ranging between 115 masl and 215 masl. Elevation at the proposed plant location ranges between 160 masl and 170 masl. The natural environment (topography, vegetation, soil) has been greatly modified by human activity over millennia. The dominant vegetation is quercine meadows with holm oaks. In the western half of the property, grazing lands have been developed for livestock. These were derived by the transformation of the primaeval forest through the removal of trees and understory shrubs.

Figure 5-2: IBW Project Infrastructure Map, Permit Area, and Proposed Mine Facilities



6.0 History

6.1 Prior Ownership

Historical workings at La Romanera, La Infanta, and El Cura date back to the pre-Roman and Roman eras. The deposits have since undergone several phases of small- to medium-scale exploration by various owners prior to the current phase of exploration conducted by Emerita (Table 6-1, Table 6-2, and Table 6-3). Historical records regarding ownership of El Cura are incomplete and Table 6-3 lists an approximate timeline based on the data available.

Table 6-1: Ownership History of the La Romanera Deposit

Time Period	Ownership
-	Roman and pre-Roman workings
1866	Sociedad Huelvana
1907	Unidentified owner
1926-1927	Unidentified owner
1960-1980	Asturiana de Zinc, SA
1982-1985	Phelps Dodge Española
1987-1995	Rio Tinto Minera, SA
2021-Present	Emerita Resources Corporation

Table 6-2: Ownership History of the La Infanta Deposit

Time Period	Ownership
-	Roman and pre-Roman workings
1890-1895	Unidentified owner
1965-1971	Productos Químicos de Huelva
1971-1975	Rio Tinto Minera, SA
1975	Asturiana de Zinc, SA
1980-1984	Phelps Dodge Española
1987-1995	Rio Tinto Minera, SA
2021-Present	Emerita Resources Corporation

Table 6-3: Ownership History of the El Cura Deposit

Time Period	Ownership
-	Roman and pre-Roman workings
1882	Unidentified owner
1938-1943	Austrian Geological Institute
Mid 1950s	Unidentified owner
Early 1980s	Phelps Dodge Española
Late 1980s to 1990s	Rio Tinto Minera, SA
2021-Present	Emerita Resources Corporation

6.2 Exploration History

The most significant prior exploration in the IBW Project area was carried out by three companies: Asturiana de Zinc, SA (Asturiana de Zinc), Phelps Dodge Española (Phelps Dodge), and Rio Tinto Minera, SA (Rio Tinto). The exploration consisted of geochemical sampling, geological mapping at different scales, geophysical surveys, and diamond drilling.

Part of the historical technical information and data has been preserved and made available to the public by the University of Cantabria. The National Geological Service is another source of technical information pertaining to the area. Emerita geologists have completed the digital compilation of historical hard copy data for the La Romanera, La Infanta, and El Cura deposits as part of the initial project assessment. The resulting digitised database contains collar locations, drillhole surveys, lithological coding, and core sample assay results. A summary of the historical drillhole databases compiled for each deposit is provided in Table 6-4, whilst the holes for which there is location information available are shown graphically in Figure 6-1, Figure 6-2 and Figure 6-3. All historical drilling presented is from within the IBW Project exploration permit area.

Table 6-4: Historical Drillhole Databases

Deposit	Company	Holes Drilled	Metres Drilled
La Romanera	Rio Tinto Minera, SA	29	5,282
	Asturiana de Zinc, SA	18	4,758.21
La Infanta	Asturiana de Zinc, SA	40	3,390.82
	Phelps Dodge Española	9	1,253.1
El Cura	Rio Tinto Minera, SA	2	1,000
	Phelps Dodge Española	17	5,078

Figure 6-1: La Romanera Historical Drilling

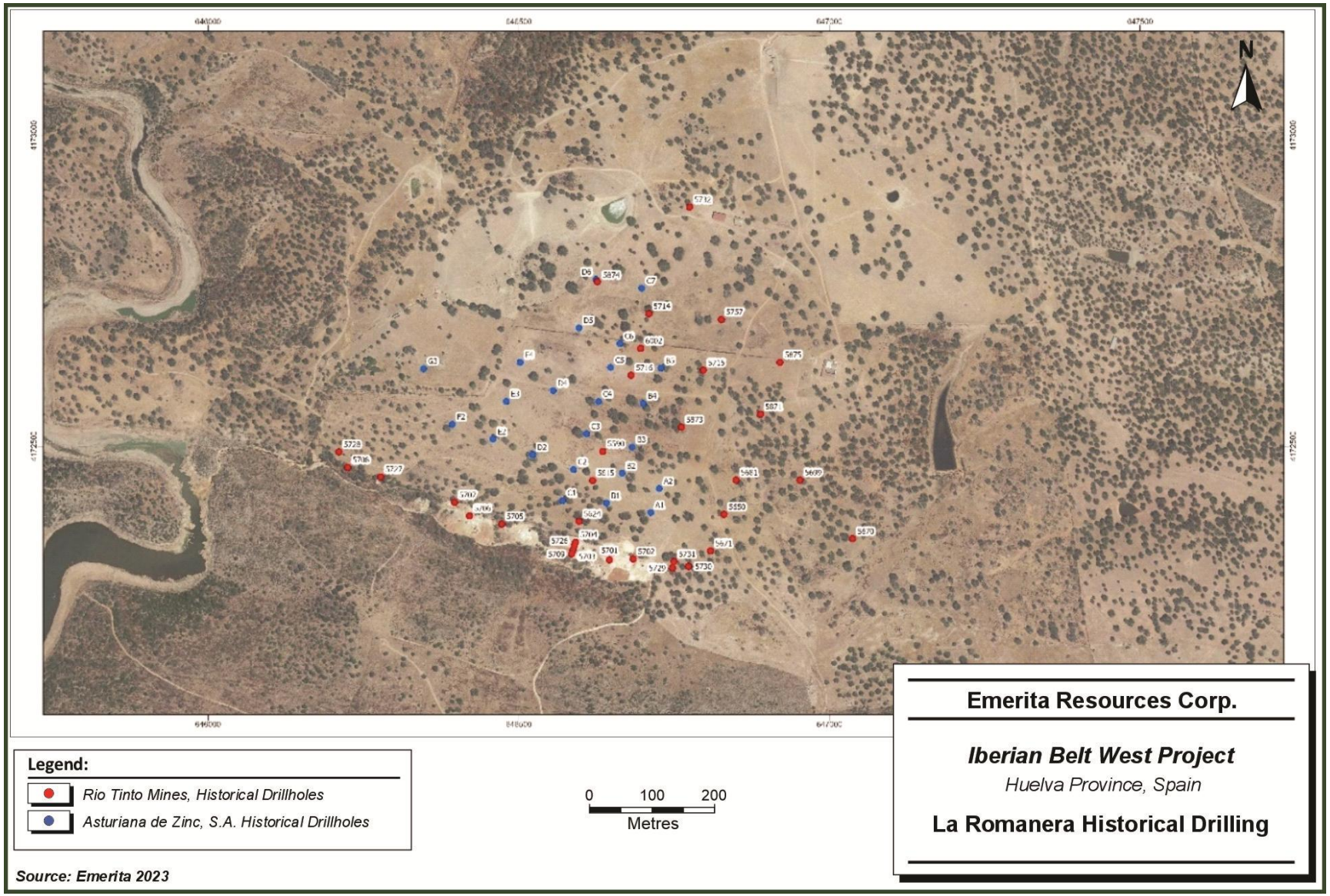


Figure 6-2: La Infanta Historical Drilling

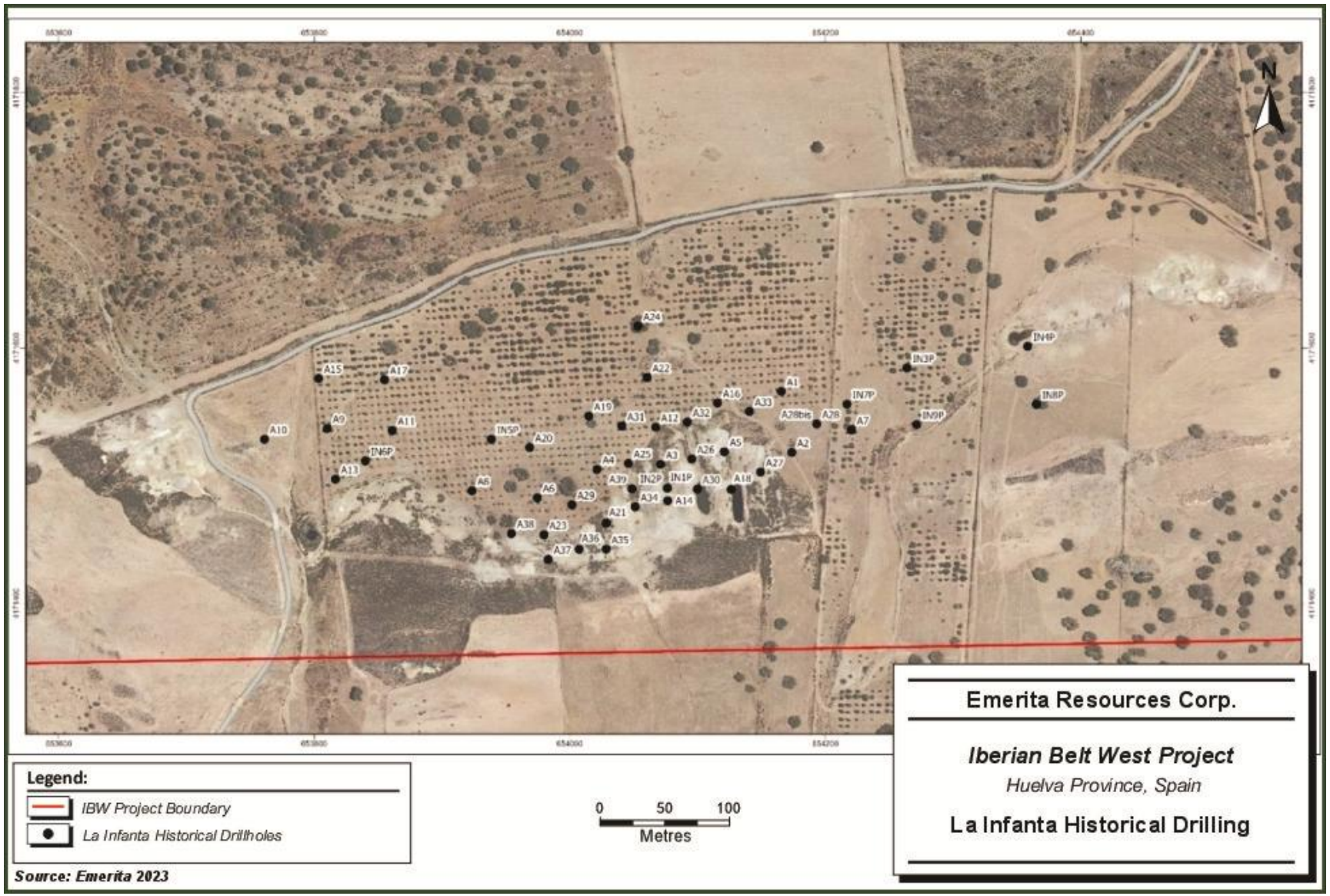
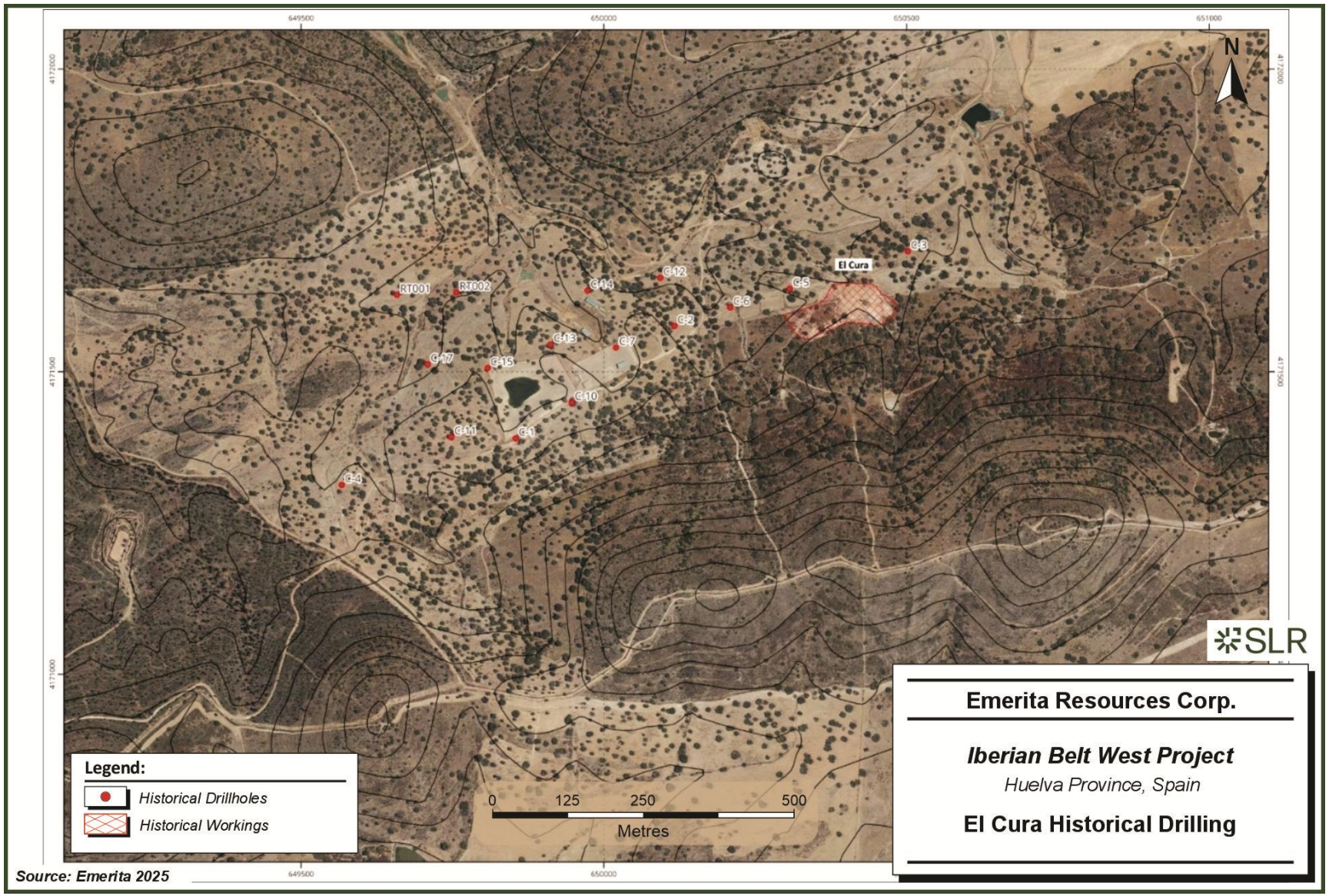


Figure 6-3: El Cura Historical Drilling



6.3 Historical Resource Estimates

Some historical Mineral Resource estimates (MREs) prepared by past owners have been found in documents compiled from the University of Cantabria and Rio Tinto Foundation holdings. The historical estimates are listed in Table 6-5.

Table 6-5: Historical Mineral Resource Estimates

Deposit	Owner	Year	Tonnage (Mt)	Average Grade				
				Cu (%)	Pb (%)	Zn (%)	Ag (%)	Au (%)
La Romanera (Global)	Rio Tinto Minera	1990s	34	0.42	2.20	2.30	44.4	0.8
La Romanera (High Grade)	Rio Tinto Minera	1990s	11.2	0.40	2.47	5.50	64.0	1.0
La Infanta	Rio Tinto Minera	Unknown	1	1.54	5	1	500	-
El Cura	Phelps Dodge	1979	2.98	1.48	0.52	1.89	17.6	-

A QP, as defined by NI43-101, has not done sufficient work on behalf of Emerita to classify the historical estimates as Mineral Resources. The historical estimates should not be relied upon and are superseded by the MREs presented in Section 14.0.

6.4 Production History

The IBW Project contains various historical mine workings, including small-scale prospecting pits, shallow shafts, adits, and exploration drives. Limited production records are available, and no historical infrastructure, mine buildings, or processing plant remain on site.

6.4.1 La Romanera

The La Romanera deposit has produced minerals since Roman times, primarily from surface gossan material.

Prior to modern exploration, small-scale mining was carried out at La Romanera. In 1866, Sociedad Huelvana mined 46 t of copper ore from trenches along the mineralised lenses. In 1907, an additional 100 t of copper ore was mined by an unknown owner. In 1926, exploratory underground development was carried out and identified three massive sulphide lenses, with thicknesses from 2 m to 6 m over a 400 m strike extent.

Information available to constrain the location and extent of the historical exploration drives is limited to an Asturiana de Zinc long section, which includes a vertical projection of multiple shafts and two development levels, with a maximum depth of approximately 50 m from surface (+110 mRL). Historical La Romanera resource and reserve reporting was restricted to below the +100 mRL.

6.4.2 La Infanta

A cluster of pre-Roman and Roman shafts has been mapped above the Infanta South and South 1 lenses, over a 110 m strike extent. Ancient mining is unlikely to have developed below groundwater level and a maximum depth of 5 m is interpreted based on the elevation of the associated drainage adit. This restricts any mining to oxide mineralisation, which is not part of the La Infanta Mineral Resource or Mineral Reserve.

The La Infanta deposit produced 400 t of ore between 1890 and 1895, from a 40 m deep shaft connected to two parallel mining levels 15 m apart and 10 m to 15 m long. Between 1965 and 1971, Productos Químicos de Huelva S.A. conducted small-scale exploratory development from the Levente and Poniente shafts.

Available cross-sections and level plans have been georeferenced and used to reconstruct development associated with the Levante and Poniente shafts. The Levante shaft is 40 m deep, with three levels containing approximately 110 m of combined ore development, located in the eastern extension of the Inferred Resource. The Poniente shaft is 60 m deep, with approximately 200 m of ore development mainly restricted to a single level, located in the western extension of the Inferred Resource. Like La Romanera, historical underground mining at La Infanta was exploratory in nature and there is no record of stoping.

6.4.3 El Cura

The El Cura deposit was referenced in an 1888 report by Gonzalo and Tarin that noted the existence of six ancient shafts to depths of between 18 m and 24 m, presumably of Roman origin. A mining group established in London in 1882 reportedly mined 500 t of ore from El Cura. Later, between 1938 and 1943, the Austrian Geological Institute conducted research and exploration work, including electrical surveying followed by underground exploration, comprising a 100 m shaft and three north-south drifts at 30 m, 60 m, and 90 m from the surface. Between the early 1940s and the mid-1950s, two shallow exploration drives were made to test the potential of manganiferous jaspers in the area.

All historical shafts and development at El Cura are located more than 250 m east along strike beyond the current Mineral Resource and Mineral Reserve area.

7.0 Geological Setting and Mineralisation

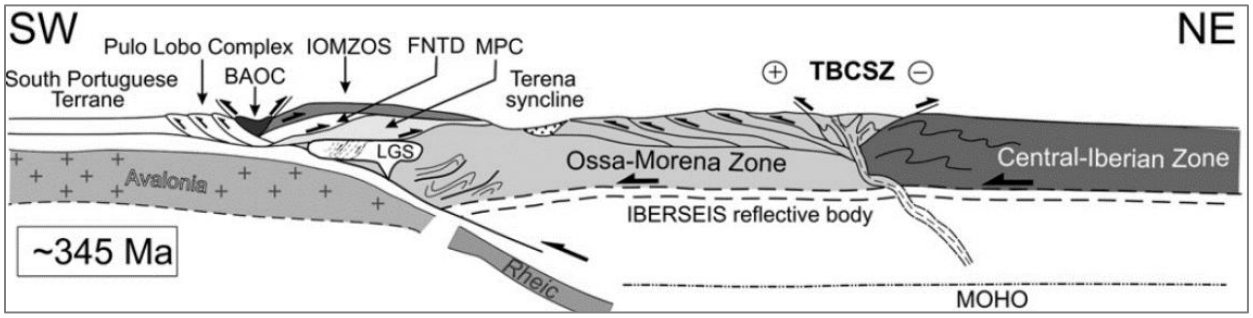
7.1 Regional Geology

The IBW Project is located in the Iberian Pyrite Belt (IPB), one of the largest mining districts in the world and a key area of base metal production in Europe. It hosts more than 1,600 Mt of massive sulphides, approximately 250 Mt of stockwork-associated mineralisation, and more than 90 volcanogenic massive sulphide (VMS) deposits, comprising 22% of the known VMS deposits globally (Tornos 2006). The map in Figure 7-2 shows the location of the Project in context with the regional geology.

The IPB is the southernmost domain of the South Portuguese Terrane (SPT). North of the SPT is the Ossa Morena Zone (OMZ), separated by the Variscan suture, which formed during the closure and northward oblique subduction and later obduction of the Rheic Ocean (Silva et al., 1990), evidenced by the Beja-Acebuches ophiolite (BAOC) and the Pulo do Lobo accretionary prism (Silva 1989; Quesada 1991; Quesada et al., 1994; Ribeiro et al., 1990) (Figure 7-1).

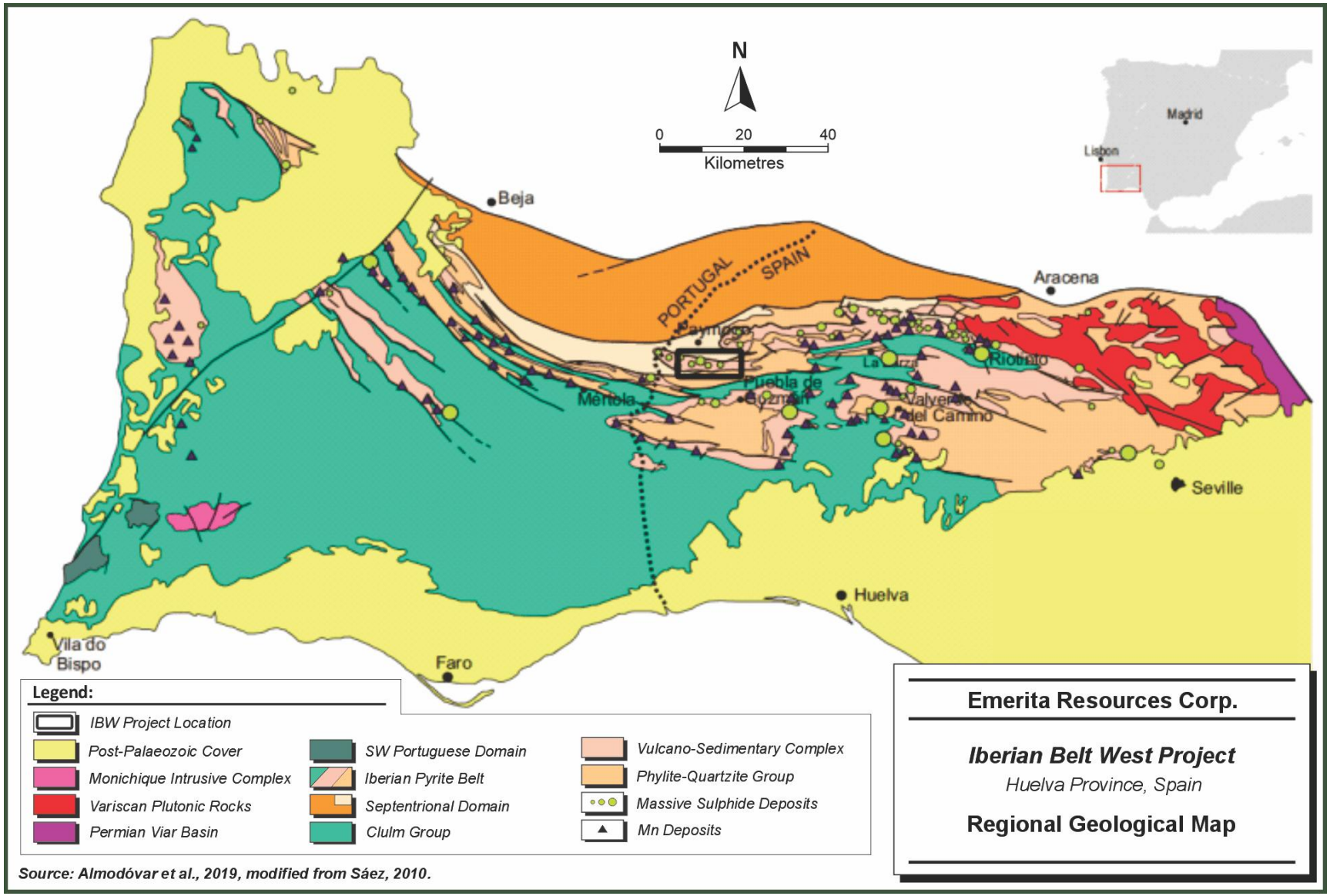
The oblique nature of the collision under a sinistral transpressional regime (Ribeiro et al., 1990; Quesada et al. 1994) promoted magmatic activity (Silva et al. 1990; Quesada 1998; Tornos et al., 2002; Jesus et al., 2007). This generated the VMS deposits of the IPB, formed within an intracontinental forearc basin from the Upper Devonian to the Lower Carboniferous (Quesada et al. 1998; Tornos 2006).

Figure 7-1: Schematic Section of the Suture Zone Between the SPT and OMZ



Source: Ribeiro et al. 2010.

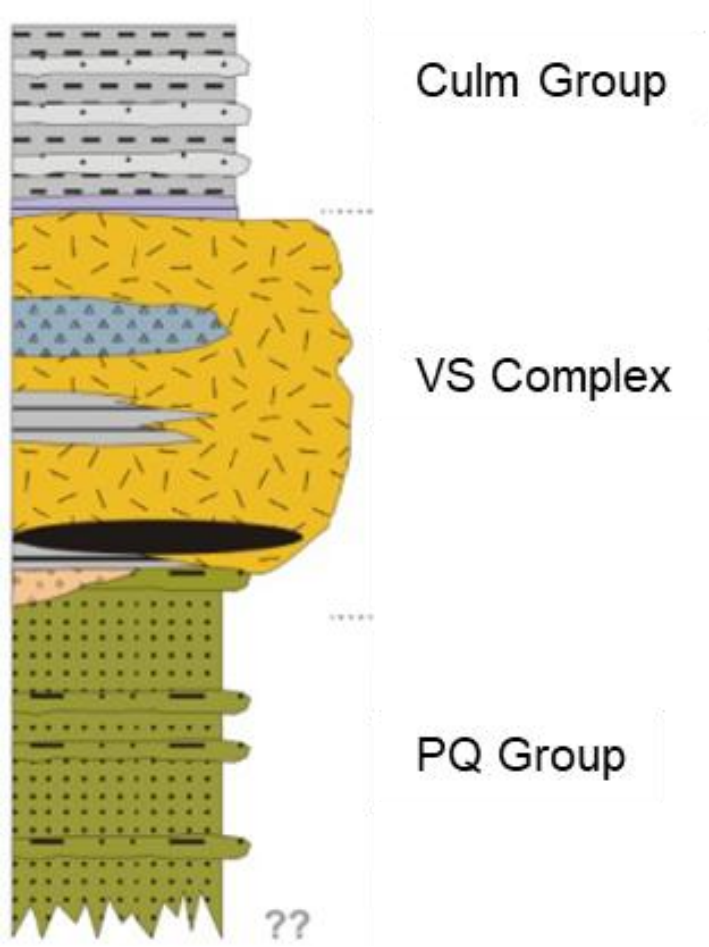
Figure 7-2: Regional Geological Map



The IPB stratigraphic sequence can be divided into three main groups despite lateral facies variations and tectonic deformation that complicate the stratigraphy (Leistel et al., 1998) (Figure 7-3):

- **PQ Group** (Frasnian to Late Famennian): Over 2 km thick (Tornos 2006) and composed of a detrital-siliciclastic sequence with alternating mudstone, limestones, and sandstones with typical characteristics of a stable epicontinental platform (Moreno et al., 1996).
- **VS Complex (VSC)** (Late Famennian to Early Visean): Comprises a 1.3 km thick bimodal volcanic sequence, dominated by felsic rocks of rhyolitic-dacitic composition, with minor proportions of mafic volcanic rocks and intercalations of mudstone, limestone, and chemical sediments (Tornos 2006). The VSC represents deposition during the collision of the SPT (Avalonia), with the Iberian Massif (Gondwana), in an intracontinental basin (Tornos 2009).
- **Culm Group** (Late Visean to Late Pensilvanian): Also known as the Baixo Alentejo Flysch Group in Portugal. This flysch includes more than 3 km of shales, sandstones, and scarce conglomerate intercalations, with turbiditic characteristics. The Culm Group represents the Variscan syn-orogenic foreland flysch related to the collision and its tectonic inversion (Moreno 1993).

Figure 7-3: General Stratigraphic Column of the Iberian Pyrite Belt



Source: Modified from Schermerhorn 1971 and Conde 2016.

The IPB has been interpreted to comprise three distinct litho-structural domains (Quesada 1996):

- **The Northern Domain** has the highest number of mineral deposits in the IPB along a 26 km strike length, including La Romanera, La Infanta, El Cura, Aguas Teñidas, Lomero-Poyatos, Cueva de la Mora, Concepción, San Platón, Monte Romero and San Miguel (Tornos et al., 2009). This domain is characterised by massive sulphides hosted by felsic volcanoclastic rocks, replacing pumice or volcanic glass metastable layers, such as dome hyaloclastites, and developing stratiform layers to irregular orebodies (Tornos 2006). The VSC here consists mainly of fine grained sediments with massive sub-marine lavas and felsic volcanoclastics. Leistel et al. (1998) interpretated it to be an isolated basin from continental source.
- **The Intermediate Domain** contains the least massive sulphide deposits. The only two significant deposits are La Zarza and Rio Tinto. Rio Tinto massive sulphide shares common characteristics between the northern and southern domains of the IPB (Tornos et al., 2009).
- **The Southern Domain** includes the most important VMS deposits in the IPB, associated with sedimentary rocks in a continental supplied basin with minor volcanic activity (Leistel et al., 1998). These deposits include Aznalcollar-Los Frailes, Sotiel-Migollas, Masa Valverde, Tharsis, and Las Cruces. Most of these deposits are exhalative type, associated with more saline and lower temperature fluids, embedded in black shales deposited on an anoxic seafloor during the Upper Devonian and formed by bio-induced precipitation (Tornos et al., 2018).

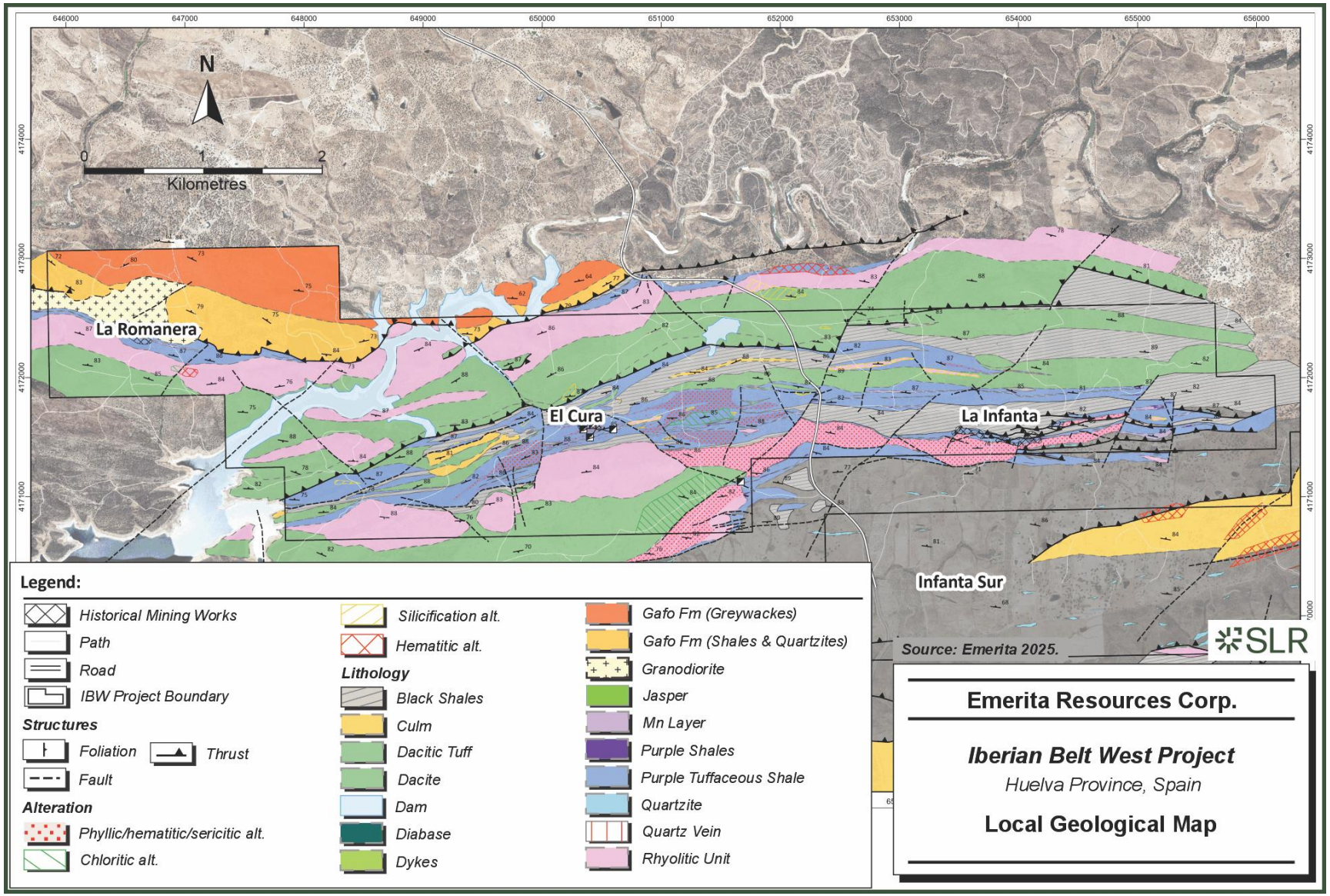
7.2 Local Geology

The La Romanera, La Infanta, and El Cura deposits are located in the northwest of the Spanish section of the IPB, within the normal northern limb of the Puebla de Guzman anticline, hosted by the Paymogo Volcano-Sedimentary Alignment (PVSA), a division of the VSC. The Puebla de Guzman anticline is isoclinal and verges to the south. The southern volcanic axis of Paymogo is the most northwestern outcrop of the IPB in Huelva Province (Donaire et al., 1998).

Felsic tuffs and black shales within VSC host the VMS mineralisation in different stratigraphic levels, with La Infanta and El Cura located at the footwall and La Romanera at the hanging wall of the sequence (Figure 7-4). The VMS mineralisation has been dated at 350 Ma (Oliveira et al., 2004). There are several levels of dacitic rocks of variable composition and texture. In the hanging wall of the dacitic sequences appear rhyolitic breccias and grayish strongly silicified massive rhyolites. The dacitic sequence is older (348.9 ± 0.4 Ma) than the rhyolitic sequence (347.3 ± 0.8 Ma) (Donaire et al., 2020). The Gafo Formation (base of Culm Group) is located north of the mineralised horizons in La Romanera, by structural contact with the VSC. U-Pb zircon geochronology determined a depositional age of 369.1± 2.5 Ma for the Gafo Formation.

IBW Project rocks record a penetrative regional axial planar foliation (S1) that strikes approximately 100°E and dips approximately 75° to the north. The layering (S0) is oriented subparallel to S1, but shows greater oscillations. There is a large sector with gently dipping or subhorizontal bedding due to the presence of a kilometre-scale fold hinge. The minor fold axes and intersection lineation between S0 and S1 have a dominant gentle plunge to the east, and the general vergence of the foliation is to the south (Azor 2023). The VSC, which hosts the mineralisation, dips to the north-northwest.

Figure 7-4: Local Geological Map

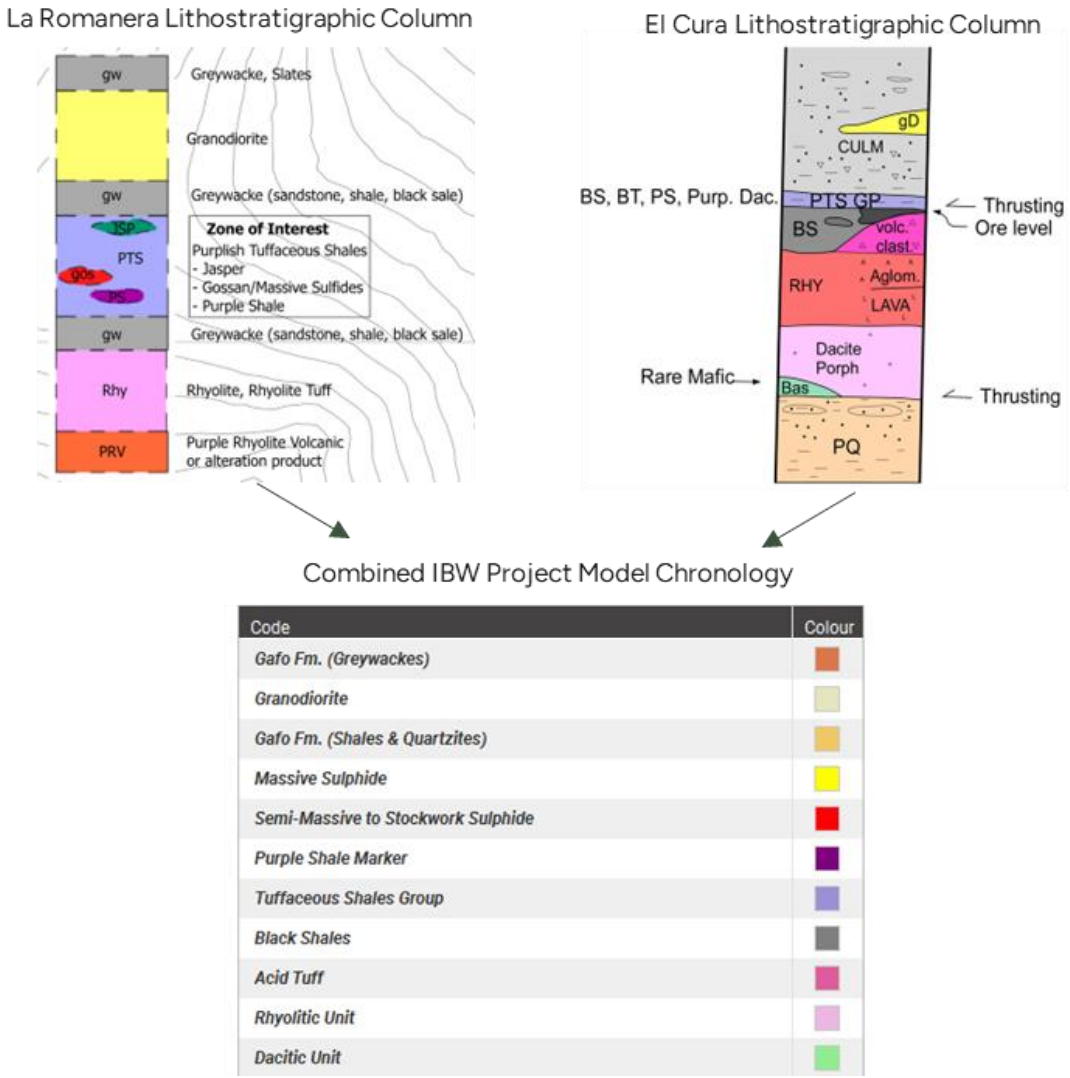


7.2.1 IBW Project Geological Model

The Emerita geology team have completed detailed deposit-scale geological mapping, core logging, and cross-section interpretations to constrain the geological framework of each deposit, including the host lithostratigraphic sequence and the nature of key contacts (Figure 7-5). Beyond the deposit areas, Emerita has completed systematic outcrop mapping across the IBW permit area, which has been integrated with the geochemical and geophysical survey data described in Section 9.0, to develop a coherent project-scale geological map (Figure 7-4).

SLR has used these inputs to develop a three-dimensional (3D) geological model for the IBW Project (Figure 7-6 and Figure 7-7) using Leapfrog Geo. The model is detailed across the three deposit areas, primarily based on the drillhole logging data and deposit-scale map and cross-section interpretations. Beyond the deposit areas, the model is more generalised and relies on the project-scale geological map to merge local inputs into a combined model.

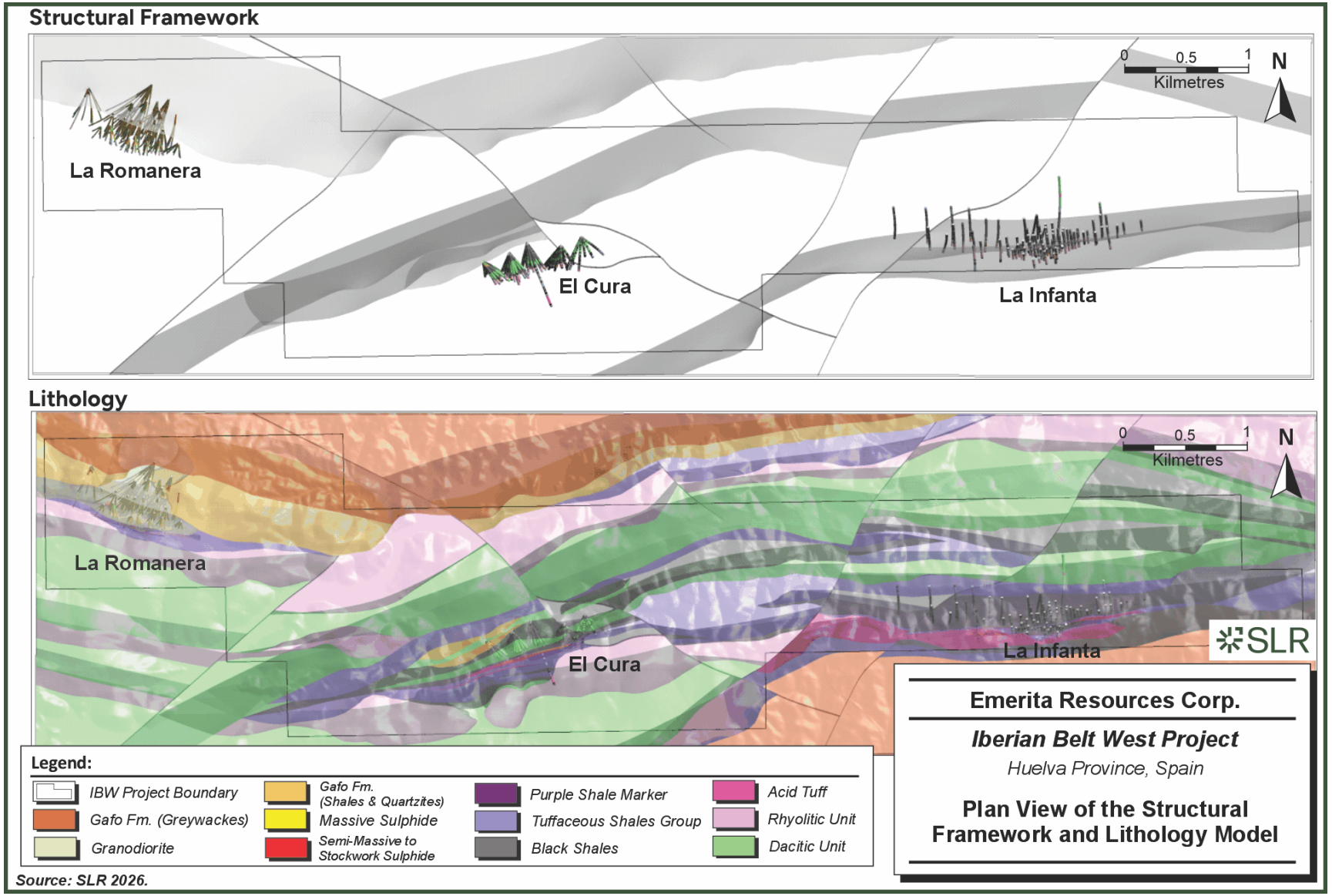
Figure 7-5: Relationship between Deposit Scale Lithostratigraphic Columns and IBW Project Geological Model Chronology



Code	Colour
Gafo Fm. (Greywackes)	
Granodiorite	
Gafo Fm. (Shales & Quartzites)	
Massive Sulphide	
Semi-Massive to Stockwork Sulphide	
Purple Shale Marker	
Tuffaceous Shales Group	
Black Shales	
Acid Tuff	
Rhyolitic Unit	
Dacitic Unit	

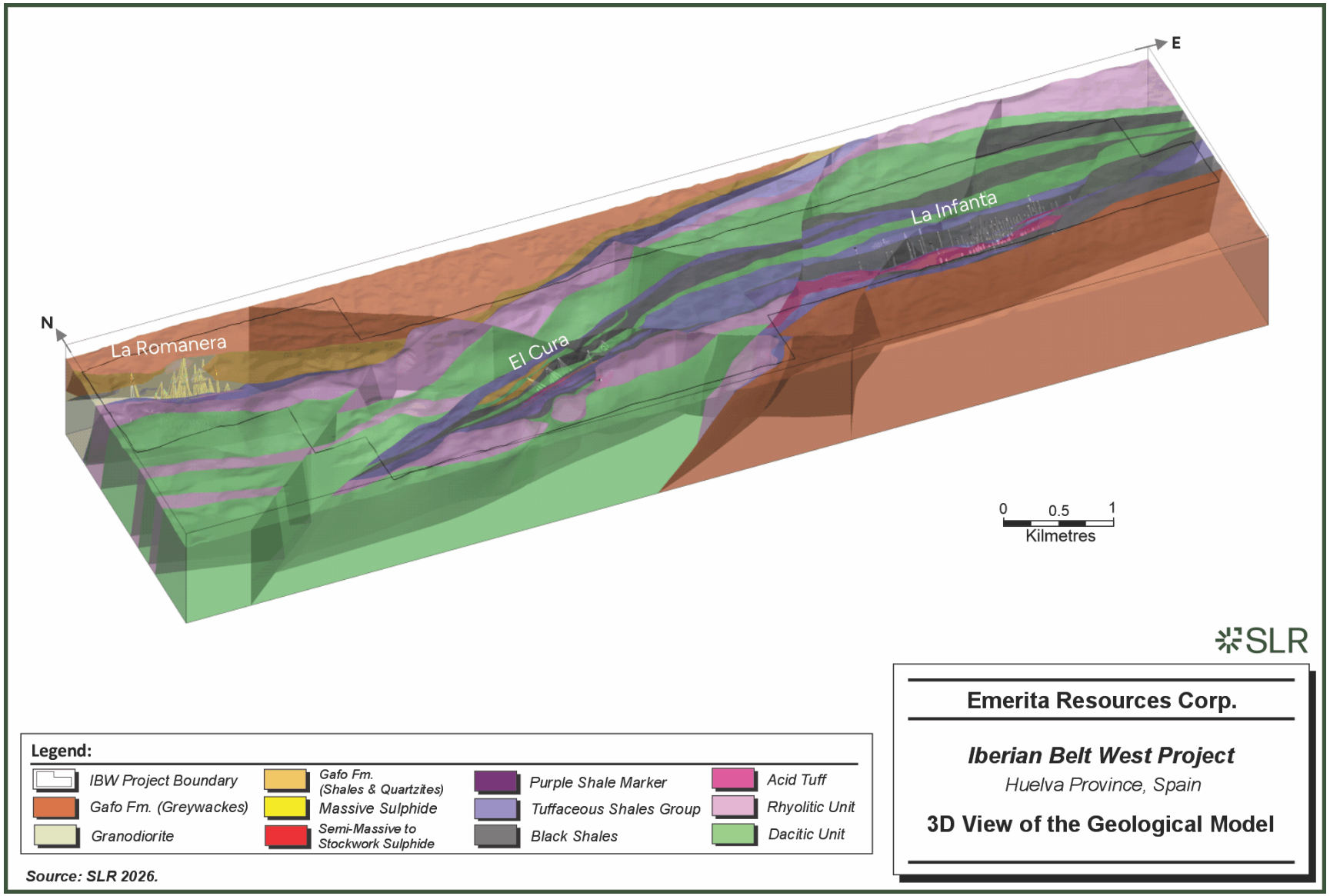
Source: SLR 2026.

Figure 7-6: Plan View of the Structural Framework and Lithology Model



Source: SLR 2026.

Figure 7-7: 3D View of the Geological Model



7.3 Property Geology

7.3.1 Introduction

The La Romanera, La Infanta, and El Cura deposits are classified as VMS deposits and mineralised domains occur primarily as tabular strata-bound lenses of polymetallic (Zn, Pb, Cu, Ag, Au) massive sulphides. Metal association varies between deposits from distinctly Zn-Pb-Ag rich mineralisation at La Infanta, higher Cu-Au grades at El Cura, and a more mixed assemblage at La Romanera.

7.3.2 La Romanera

The deposit-scale geological model for La Romanera is outlined in Figure 7-8 and Figure 7-9. Mineralisation is hosted by a purple tuffaceous shale unit (PTS), underlain conformably by a footwall rhyolite. A sinistral thrust bounds the hanging wall contact of the mineralised sequence with overlying Gafo Formation shales and quartzites. Locally, the base of the Gafo Formation is intruded by granodiorite, which is the dominant hanging wall unit in the deposit. The granodiorite is itself intruded by a series of minor andesite dykes.

Type examples and descriptions of the main lithostratigraphic units at La Romanera are provided in Table 7-1.

7.3.3 La Infanta

The deposit-scale geological model for La Infanta is illustrated in Figure 7-10 and Figure 7-11. The La Infanta deposit is located at the contact between a footwall unit of highly silicified acid tuffs and a hanging wall volcanoclastic unit of the PTS group. Tectonically, the mineralisation is located on the northern flank of an extensive anticline, which is consistently faulted. These faults create a repetition of the mineralised horizon, which divide the mineralisation into the North, South, and South 1 lenses or fault blocks. Only the fault between the North and South lenses is delineated and actively applied in the current geological model.

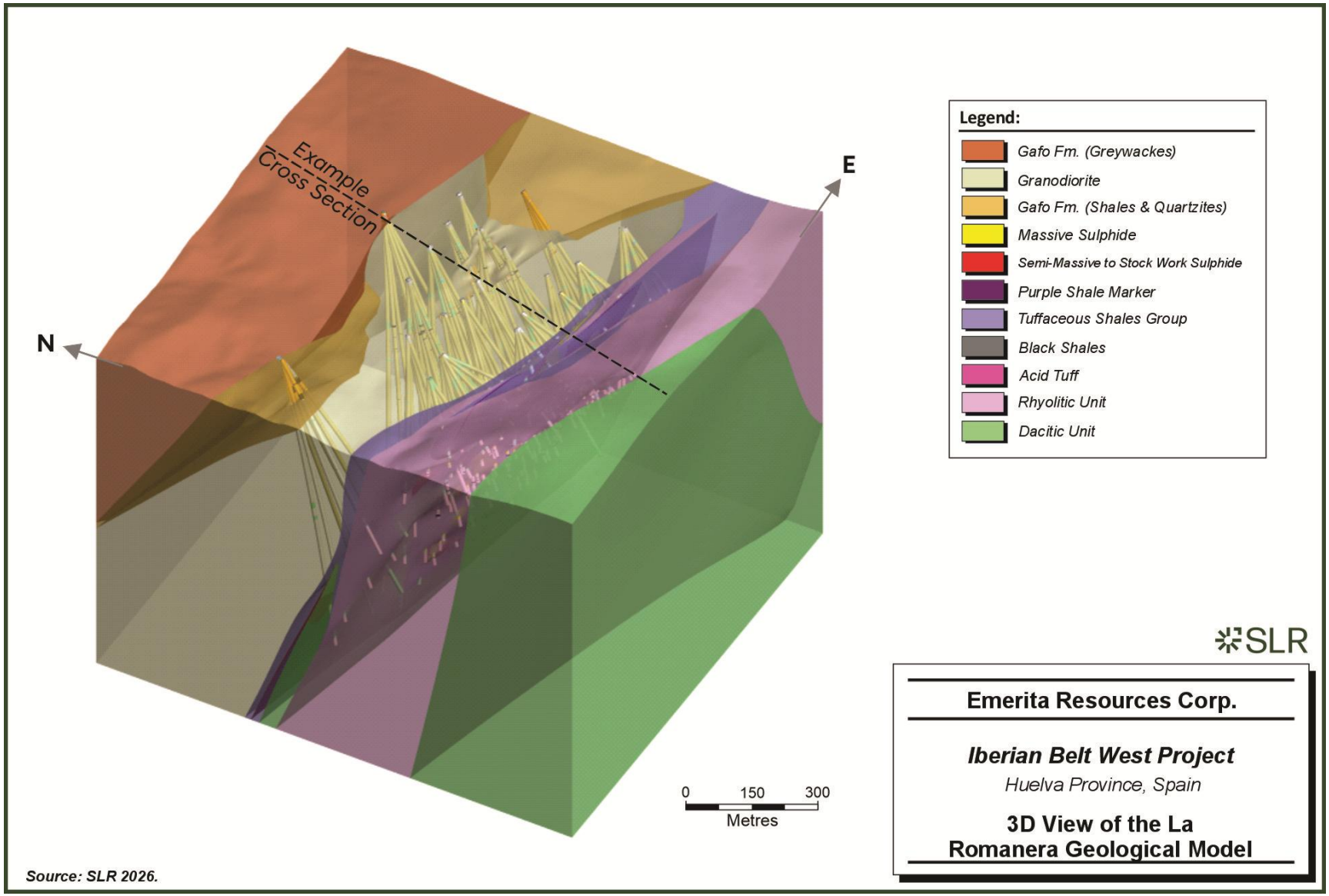
Type examples and descriptions of the main lithostratigraphic units at La Infanta are provided in Table 7-2.

7.3.4 El Cura

The deposit-scale geological model for El Cura is illustrated in Figure 7-12 and Figure 7-13. El Cura is situated in a valley between two prominent ridges of volcanic dacite and rhyolite. The host rocks are shales and volcaniclastics of the PTS Group, stratigraphically overlying the volcanics and variably altered by chlorite, sericite, and silica. The only surface evidence of the deposit is rare and scattered gossanous cobbles within a zone of phyllic alteration.

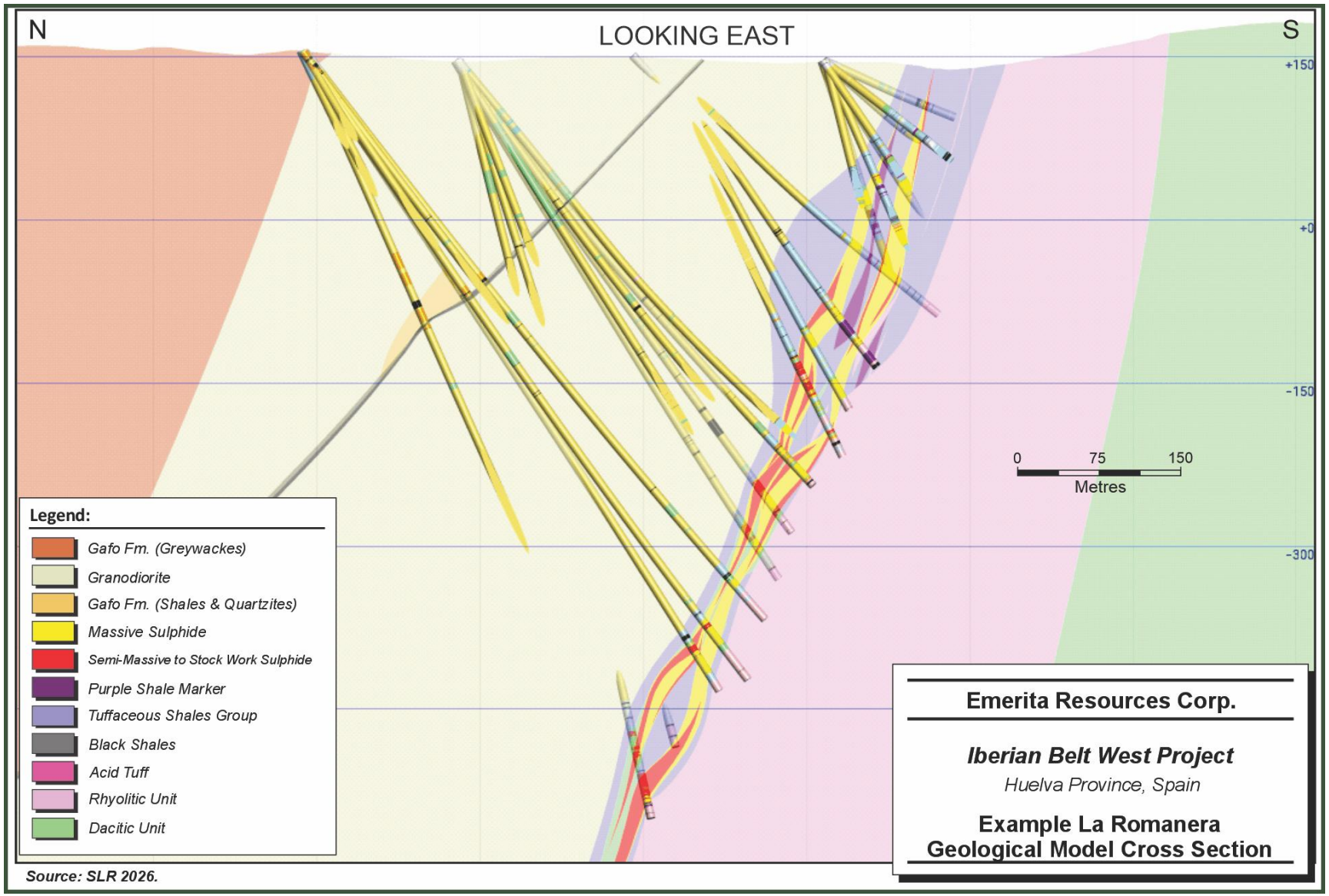
Type examples and descriptions of the main lithostratigraphic units at El Cura are provided in Table 7-3.

Figure 7-8: 3D View of the La Romanera Geological Model



Source: SLR 2026.

Figure 7-9: Example La Romanera Geological Model Cross-section



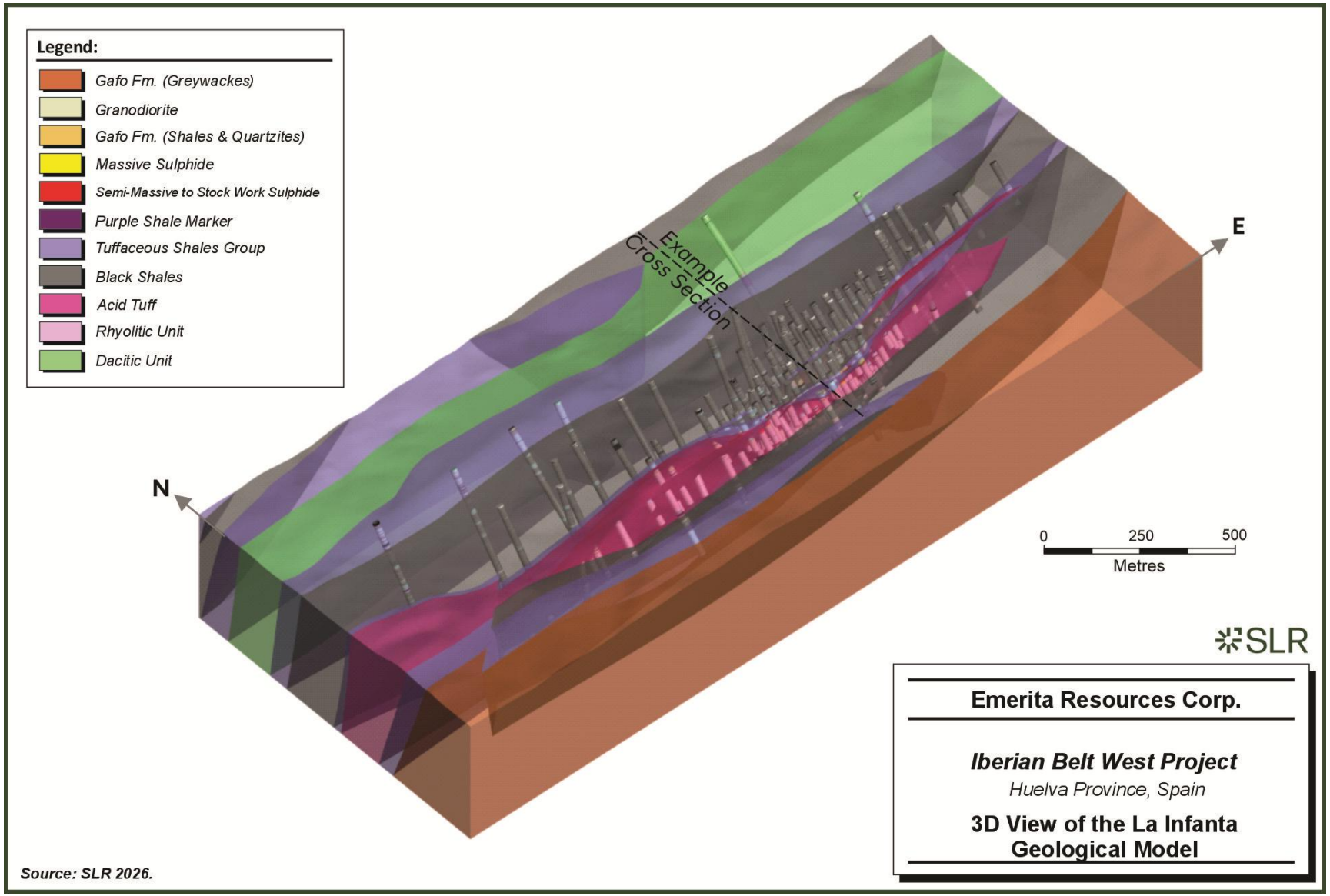
Source: SLR 2026.

Table 7-1: La Romanera – Major Lithostratigraphic Units

Name	Type Example	Description
Gafo Formation Shales and Quartzites		Characterised by flysch facies turbiditic sedimentary rocks including greywackes and interbedded shales-quartzites with minor tuffite intercalations.
Granodiorite		Granodiorite texture, grain size, and alteration varies spatially. Shown here is a melanocratic granodiorite with a coarse-grained phaneritic texture.
Purple Tuffaceous Shale Group		Reddish to purple fine-grained sediment. Colour related to pervasive hematite alteration. Used as a mapping guide at Project to regional scale.
Rhyolitic Unit		Combination of massive rhyolites, rhyolitic breccia, and agglomerates. Strong silicification is common.
Dacitic Unit		Combination of porphyritic massive dacite and dacitic tuffs. Porphyritic dacite is plagioclase-phyric with frequent microgranular enclaves and strong chlorite alteration.

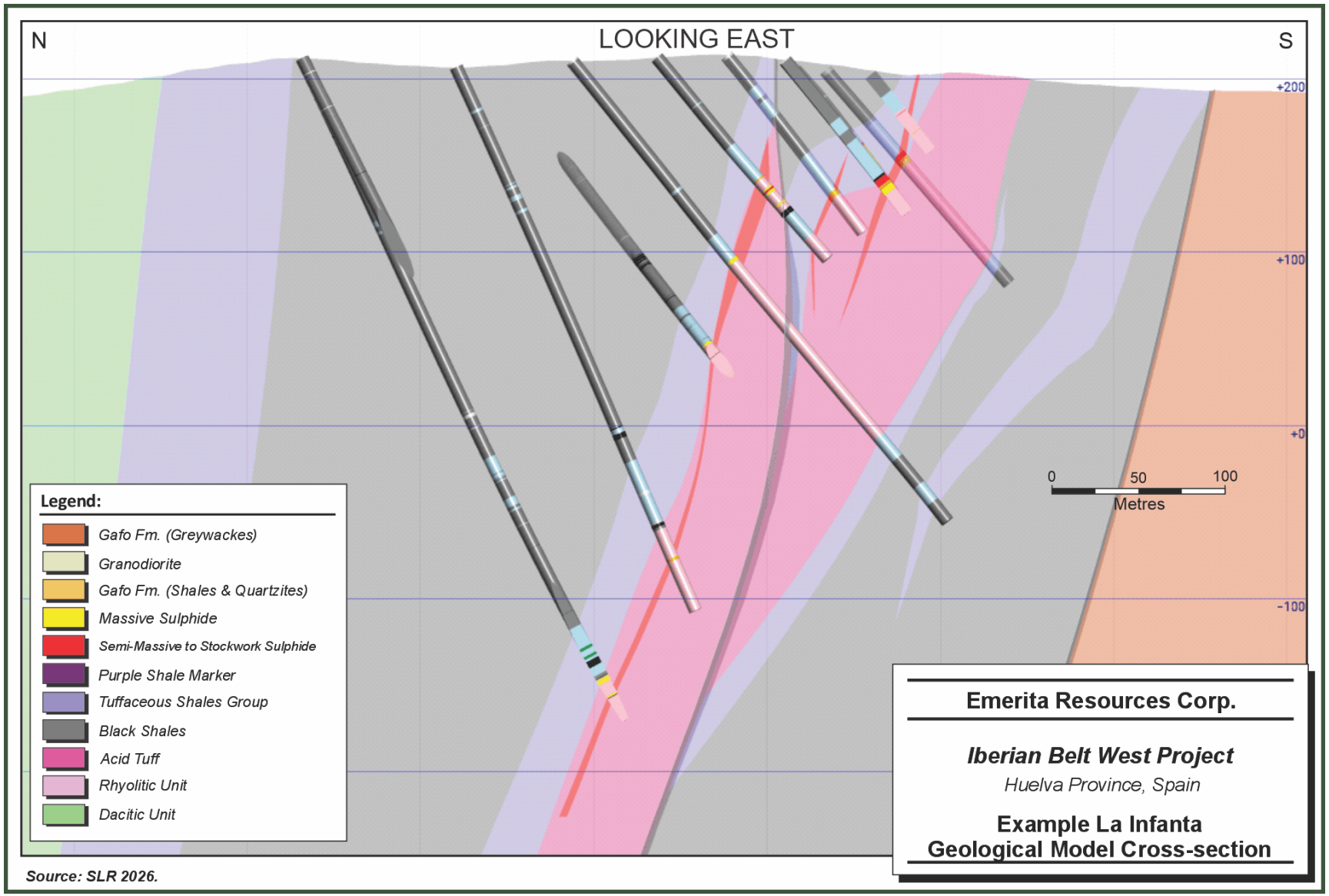
Source: Emerita 2023.

Figure 7-10: 3D View of the La Infanta Geological Model



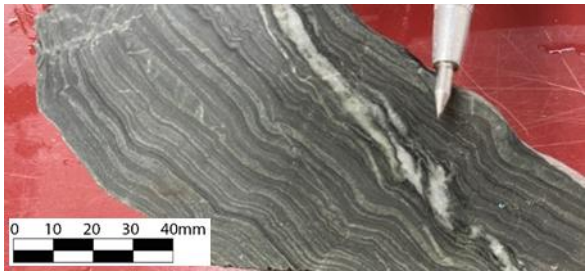
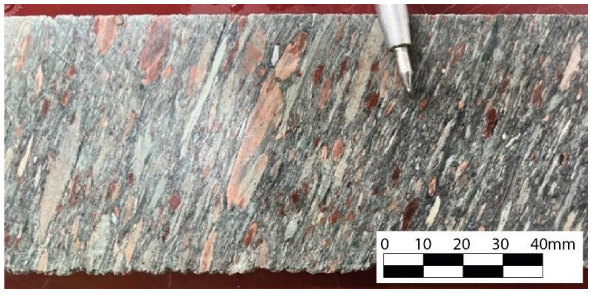
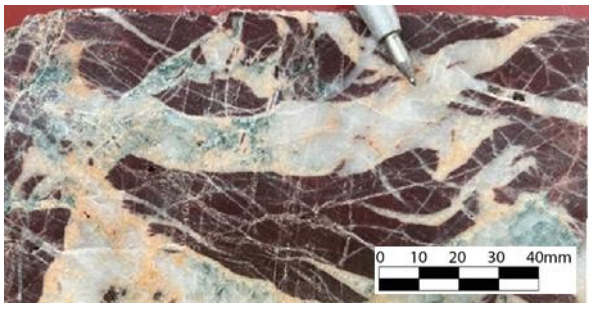
Source: SLR 2026.

Figure 7-11: Example La Infanta Geological Model Cross-section



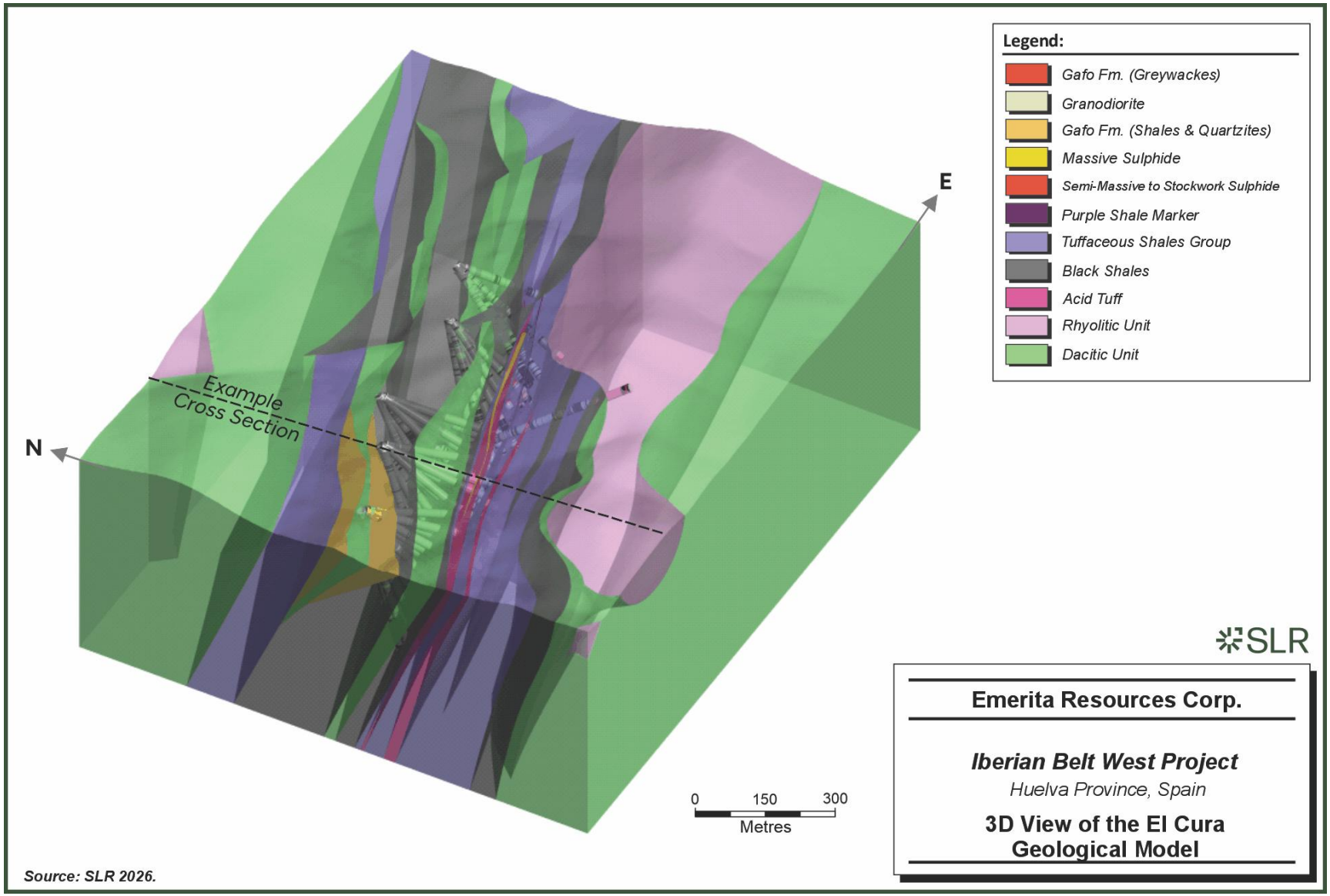
Source: SLR 2026.

Table 7-2: La Infanta – Major Lithostratigraphic Units

Name	Type Example	Description
Shale Unit		Grey to black colour due to organic content. Laminated to massive textures. Quartz veins parallel to a strong penetrative foliation.
Volcanoclastic Unit		Unit is differentiated into volcanoclastic tuffs, sandstones, and conglomerate according to grain size and texture.
Marker Horizon		Mixture of jasper and purple shales. Jasper more abundant than in La Romanera, forming marker horizon outcrops due to associated silicification.
Acid Tuff		Combination of volcanoclastic lapilli tuffs and bedded tuffs. Fin-e to medium-grain size, grayish to greenish colours and silicification alteration. Some minor base metal mineralisation characterised by veins and patches of sphalerite and galena.

Source: Emerita 2023.

Figure 7-12: 3D View of the El Cura Geological Model



Source: SLR 2026.

Figure 7-13: Example El Cura Geological Model Cross-section

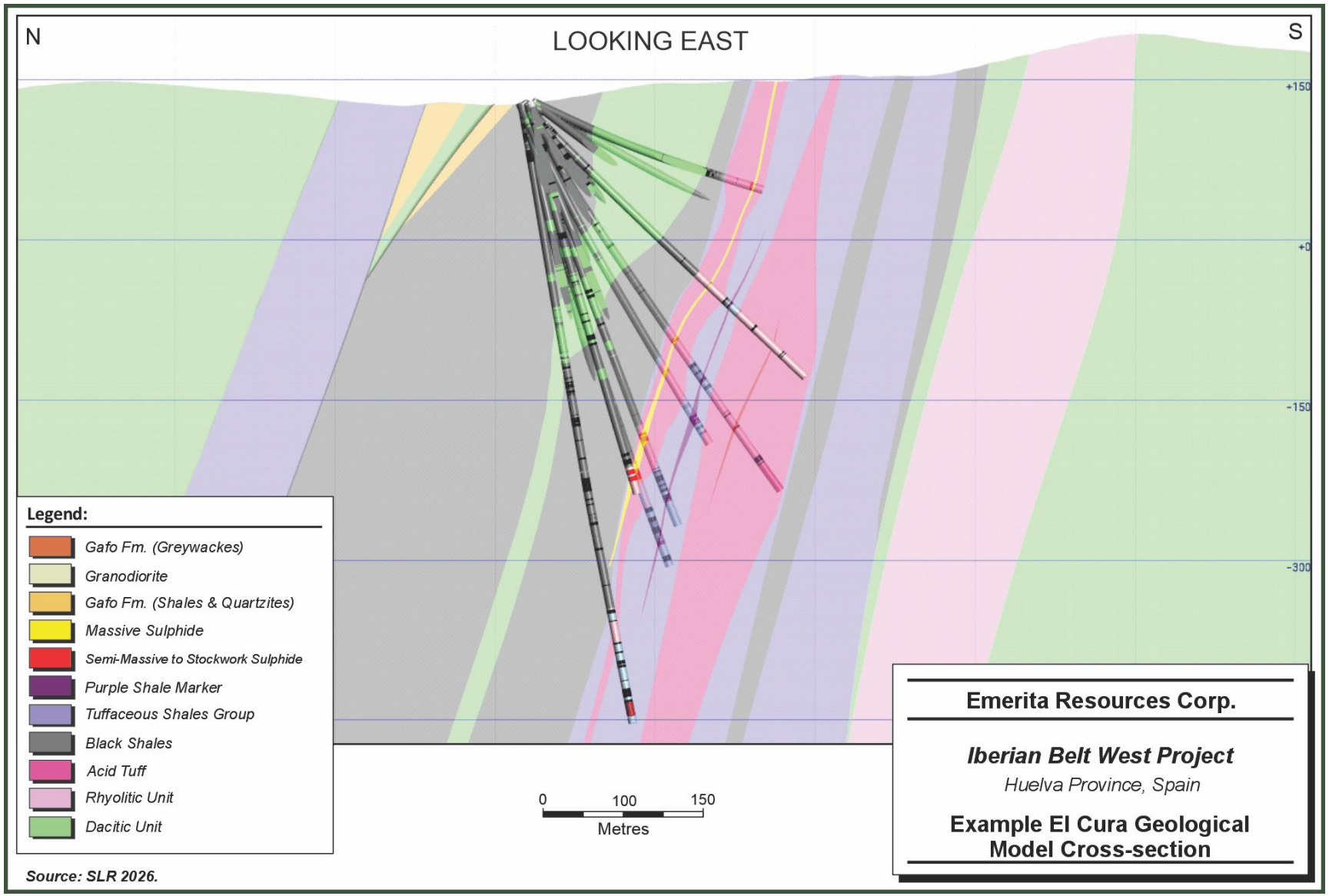
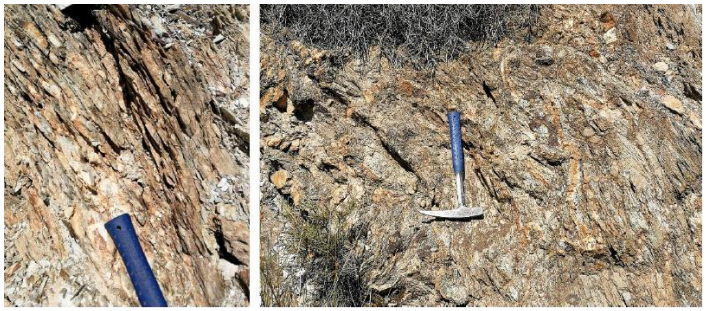
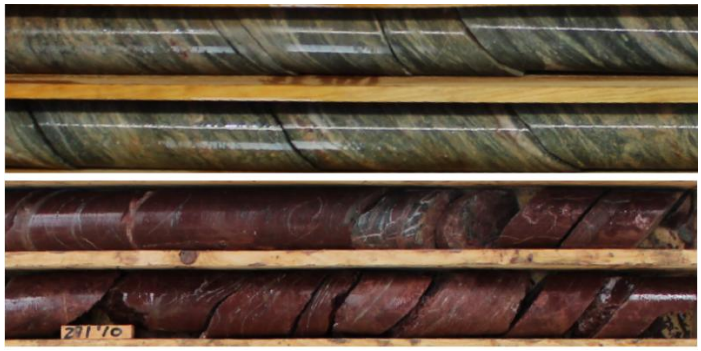


Table 7-3: El Cura – Major Lithostratigraphic Units

Name	Type Example	Description
Culm Shales		Impure shales and siltstones.
PTS Group		Black shales; volcaniclastics; cherts, and jaspers; thin rhyodacites; purple shales, and green tuffs.
Rhyolite Lava and Agglomerate		Dark purple to grey cryptocrystalline lava with fine felsic phenocryts; agglomeratic rinds of such eruptives.
Dacite		Equigranular to porphyritic felsite +/- quartz (rare).
PQ Sediments		Sandstones and shales. Local metre-scale quartzite beds.

Source: Emerita 2025.

7.4 Mineralisation

7.4.1 La Romanera

Two major sulphide lenses have so far been defined at La Romanera. The Upper Lens consists of massive to semi-massive sulphide mineralisation. The Lower Lens underlies the Upper Lens and also consists of massive to semi-massive sulphide mineralisation. Four minor parallel lenses have been defined that have limited continuity and extent. No significant stockwork-style mineralised zone is recognised in the deposit.

The main mineralogy of the deposit is pyrite, sphalerite, galena, chalcopyrite, arsenopyrite, and members of the tetrahedrite-tennantite solid solution series. Examples of La Romanera massive sulphide mineralisation are shown in Figure 7-14.

Figure 7-14: Examples of La Romanera Upper and Lower Lens Massive Sulphide Mineralisation (LR003)



Source: Emerita 2023.

The Upper Lens is a continuous mineralised horizon which varies from approximately 2 m to 32 m in true thickness and averages 10 m overall, with a strike length of 650 m.

The Lower Lens is a continuous mineralised horizon which varies from approximately 2 m to 30 m in true thickness and averages 13 m overall, with a strike length of 800 m.

The Upper Lens and the underlying Lower Lens are locally both separated and in contact with one another throughout the deposit. The Upper Lens occurs approximately 2 m to 30 m in the hanging wall above the Lower Lens. The lenses get closer together and merge at depth.

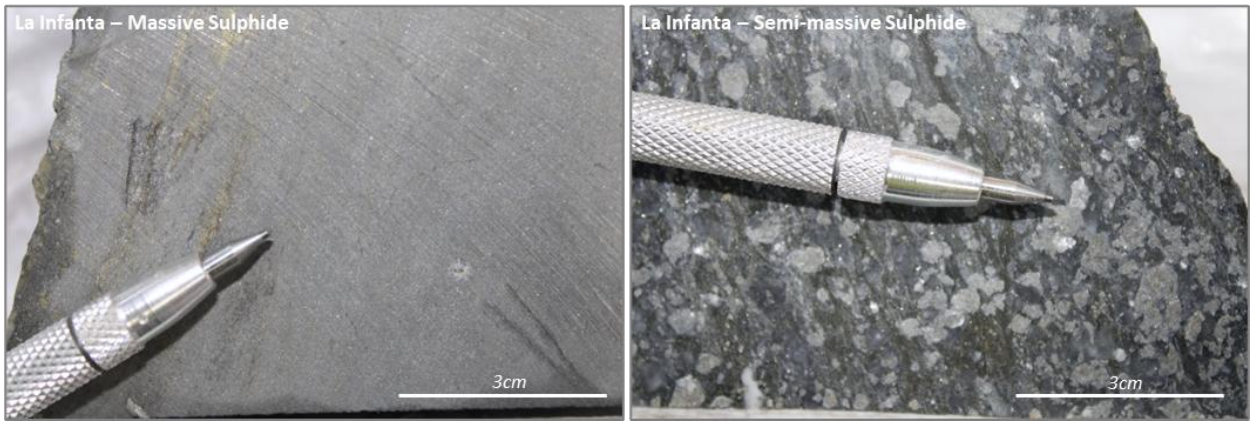
The deposit dips at approximately 70° to the north from surface. The lenses have been drill tested over a down-dip length of approximately 720 m (Upper Lens) and 800 m (Lower Lens).

7.4.2 La Infanta

Three major sulphide lenses (North, South, and South 1)) have so far been defined at La Infanta, thought to be faulted repetitions of a single mineralised horizon. Mineralisation style is broadly typical of VMS deposits but exhibits greater variability in sulphide abundance from disseminated to massive sulphide. The North Lens is underlain by the South Lens, which itself is underlain by the South 1 Lens. No significant stockwork-style mineralised zone is recognised in the deposit.

The main mineralogy of the deposit is sphalerite, pyrite, galena, chalcopyrite, and members of tetrahedrite-tennantite solid solution series. The proportion of pyrite is exceptionally low (typically <10%) and pyrite is absent over large areas. Examples of La Infanta mineralisation are shown in Figure 7-15.

Figure 7-15: Examples of La Infanta Sulphide Mineralisation



Source: Emerita, 2023.

The North Lens is a continuous mineralised horizon which varies from approximately 1 m to 10 m in true thickness and averages 3 m overall, with a strike length of 1900 m.

The South Lens is a continuous mineralised horizon which varies from approximately 1 m to 9 m in true thickness and averages 3 m overall, with a strike length of 1,090 m.

The South 1 Lens is a continuous mineralised horizon which varies from approximately 1 m to 7 m in true thickness and averages 2.6 m overall, with a strike length of 325 m.

The North Lens and the underlying South Lens are generally separated throughout the deposit by approximately 30 m. The South Lens and the underlying South Lens 1 are generally separated throughout the deposit by approximately 15 m.

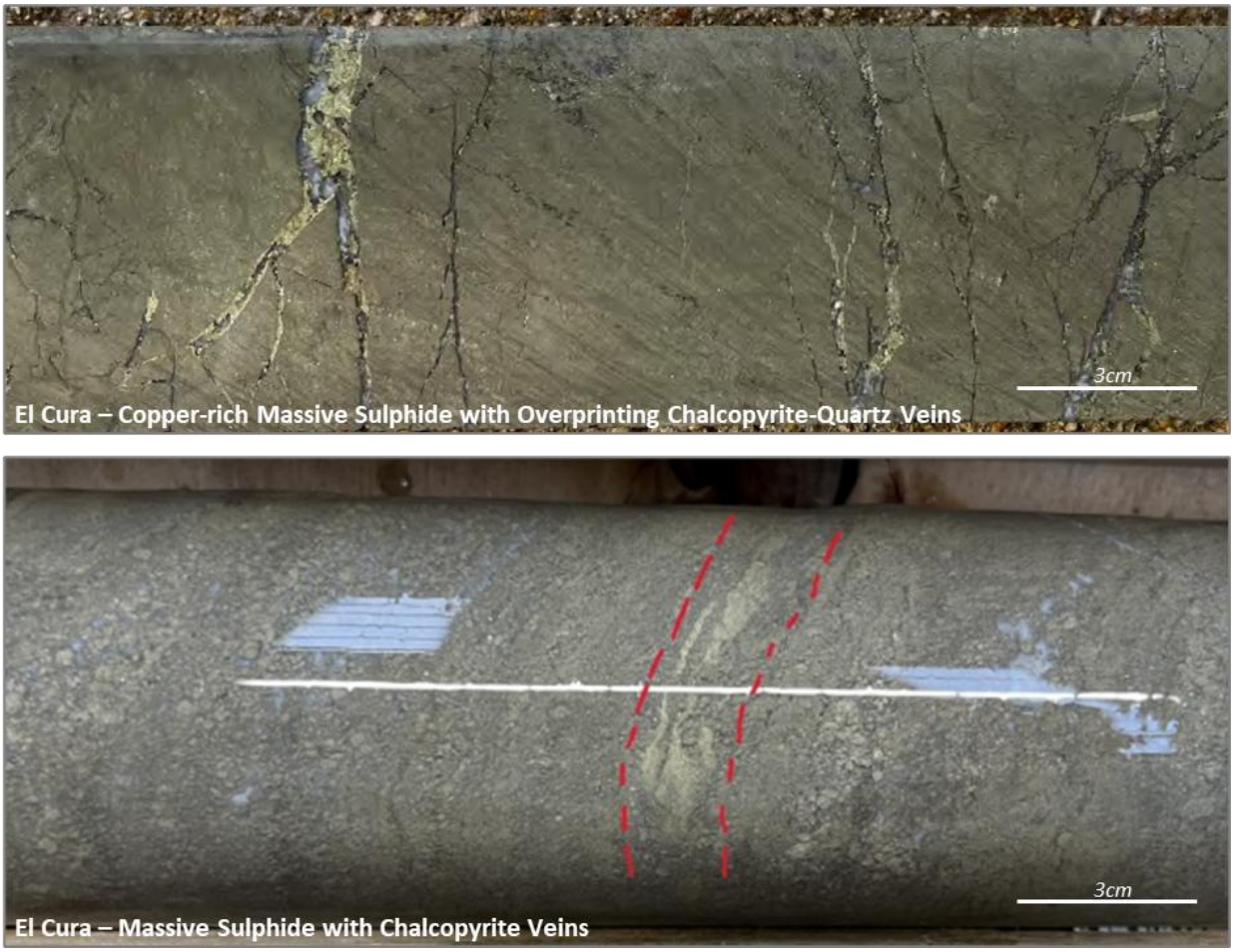
The deposit dips at approximately 70° to the north from surface. The lenses have been drill tested over a down-dip length of approximately 425 m (North Lens), 190 m (South Lens), and 150 m (South 1 Lens).

7.4.3 El Cura

Two sulphide lenses have so far been defined at El Cura. The Top Lens is dominated by massive sulphide, with lesser amounts of semi-massive typically with shale and chlorite interstitial material. Local overprinting by copper-rich veining can significantly enrich grades. Nine drillholes have been extended deeper into the footwall of the Top Lens, with four intersecting a potential Bottom Lens, so far characterised by disseminated to banded sulphides and lower grade zinc-dominant mineralisation. The Bottom Lens is not well defined by the current drill grid and is not included in the El Cura MRE. No significant stockwork-style mineralised zone is recognised in the deposit.

The main mineralogy of the deposit is pyrite, chalcopyrite, sphalerite, galena, and members of tetrahedrite-tennantite solid solution series. Examples of El Cura mineralisation are shown in Figure 7-16.

Figure 7-16: Examples of La Infanta Sulphide Mineralisation (EC014 and EC022)



Source: Emerita, 2025.

The Top Lens is a continuous mineralised horizon which varies approximately from 1 m to 8.5 m in true thickness and averages 2.5 m overall, with a strike length of 800 m. The Bottom Lens true thickness varies approximately from 1 m to 7.4 m and averages 3.6 m overall, with a strike length of 400 m. The Top Lens and Bottom Lens are generally separated throughout the deposit by approximately 60 m.

The deposit dips at approximately 70° to the north from surface. The lenses have been drill tested over a down-dip length of approximately 450m (Top Lens). The current spatial distribution of significant intersections indicates a westerly plunge to mineralisation.

8.0 Deposit Types

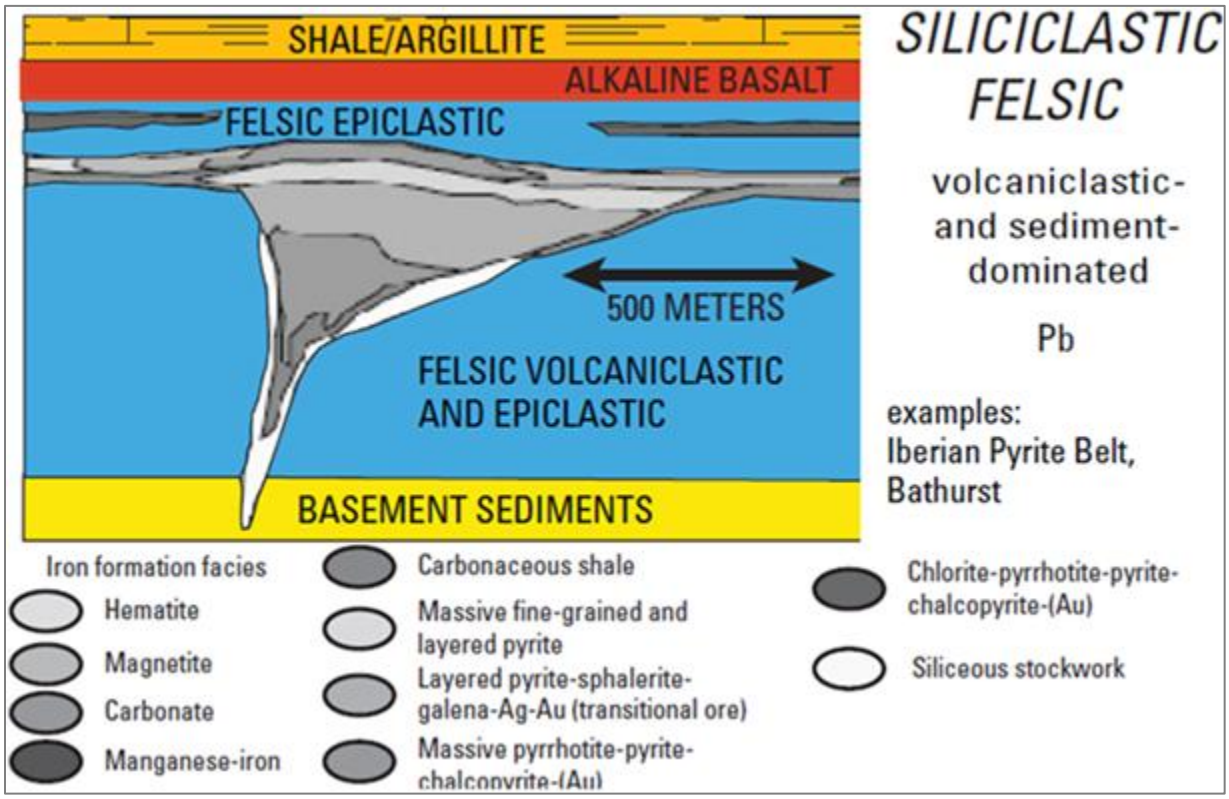
The polymetallic deposits of the IBW Project are classified as VMS deposits. VMS deposits are strata-bound concentrations of sulphide minerals precipitated from hydrothermal fluids in extensional seafloor environments. They are also known as volcanic-hosted massive sulphide (VHMS) deposits. The term volcanogenic implies a genetic link between mineralisation and volcanic activity, but siliciclastic rocks dominate the stratigraphic assemblage in some settings (including the IPB).

The principal tectonic settings for VMS deposits include mid-oceanic ridges, volcanic arcs (intraoceanic and continental margin), back arc basins, rifted continental margins, and pull-apart basins. The composition of volcanic rocks hosting individual sulphide deposits ranges from felsic to mafic, but bimodal mixtures are not uncommon. The volcanic strata consist of massive and pillow lavas, sheet flows, hyaloclastites, volcanic breccias, pyroclastic deposits, and volcaniclastic sediment. Deposits range in age from Early Archean (3.55 Ga) to Holocene; deposits are currently forming at numerous localities in modern oceanic settings (Shanks et al., 2010).

VMS deposits have two morphological and genetic components (Figure 8-1):

- A mound-shaped to tabular strata-bound body composed mainly of massive sulphides; and
- An underlying zone with development of a stockwork system of irregular veins filled by quartz and disseminated sulphides.

Figure 8-1: Schematic Diagram of a Siliciclastic Felsic VMS Deposit

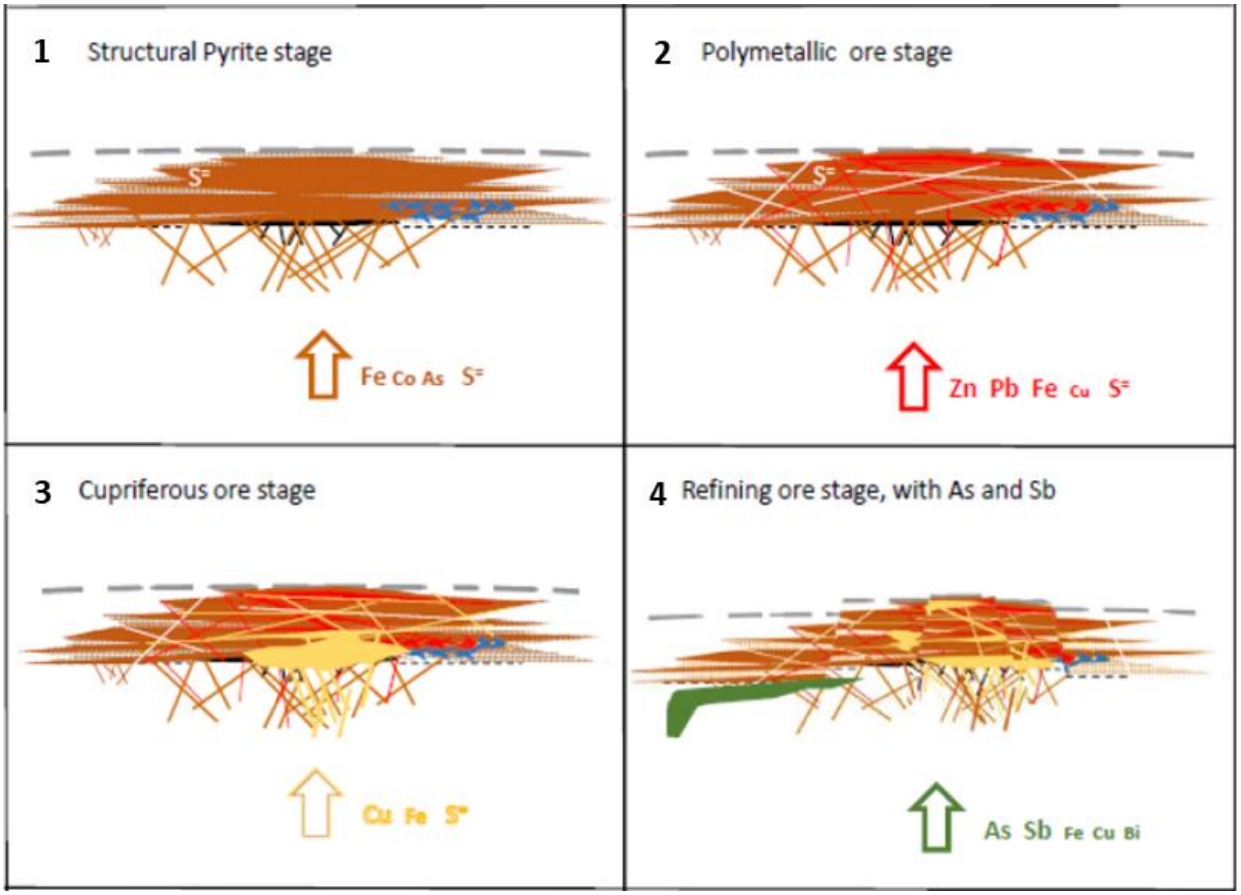


Source: Modified from Barrie and Hannington,1999, by Franklin et al., 2005.

The mineral composition of massive sulphide deposits from the IPB mostly comprises pyrite, subordinate sphalerite, galena, chalcopyrite, arsenopyrite, tetrahedrite–tennantite, cobaltite, Sb–As–Bi sulphosalts, gold, and electrum. Common oxide phases include magnetite, hematite, cassiterite, and barite.

The mineralogical and textural evolution of massive sulphides leads to a common general model for IPB deposits including four main stages (Figure 8-2): (1) An early oxic system dominated by Fe-oxides and barite precipitation; (2) Bacterial sulphate reduction (BSR) disoxic dominated conditions; (3) A high temperature hydrothermal system responsible for the main base metal mineralisation. Later in this stage, the refining processes takes place, driven by the emplacement of mafic magmas at depth leading the Sb- and As-rich mineralisation; and (4) Formation of ore shoots by selective remobilisation during the Variscan deformation.

Figure 8-2: Stages of IPB VMS Mineralisation



Source: Modified from Almodóvar et al., 2019.

9.0 Exploration

9.1 Introduction

Historical exploration surveys by Asturiana de Zinc, Phelps Dodge, and Rio Tinto have been superseded by Emerita's exploration programmes and do not inform the IBW Project MREs.

Since 2012, Emerita has completed multiple phases of exploration at the IBW Project. Until 2020, the main activity was reviewing existing information through desktop research (publications and other companies reports) and visual inspection in the field. After formal granting of the IBW permits in 2021, Emerita has carried out a range of exploration, including:

- Geological mapping.
- Soil geochemical sampling.
- Soil vapour geochemistry.
- Airborne, surface, and downhole geophysics.
- Exploration drill programmes.

Further information on drilling programmes is available in Section 10.0. A description of all other exploration work is given in the following subsections.

9.2 Geological Mapping

Detailed geological mapping has been completed by Emerita over the La Romanera, La Infanta, and El Cura deposits, as presented in Figure 7-4. Mapping began once Emerita acquired the Project and geological interpretations continue to be refined over time. Mapping helped constrain the surface distribution of lithology, alteration, structure, and mineralisation.

9.3 Soil Chemistry

Emerita completed a geochemical soil sampling campaign from 2023 to 2024, comprising 2,975 samples, analysed for 38 elements via portable X-ray fluorescence (XRF). The campaign was laid out along 52 lines with a 200 mE x 25 mN sample spacing. The primary purpose of the programme was to find additional drill targets by detecting potential geochemical indicators/pathfinders, including As, Ba, Cu, Hg, Pb, Sb, Sn, and Zn. A secondary purpose was to locate changes in soil geochemistry that mark lithological contacts and inform geological mapping. The distribution of samples and sampling lines, along with selected results are shown in Figure 9-1.

Review of the soils campaign shows that anomalous values in indicator and pathfinder elements occur within the PTS Group, which hosts VMS mineralisation at the IBW Project. Anomalous geochemistry is concentrated largely over the known deposits and secondarily over on-trend extensions of these areas. As noted in the exploration literature for the area, it is difficult to distinguish in situ geochemical anomalies from contamination resulting from centuries of open-air ore processing.

Rubidium has been identified as a useful lithogeochemical marker. Figure 9-2 presents the geology based on outcrop mapping, overlain by soil sample points coloured by rubidium concentration. Contrasting rubidium in soil values mark lithological contacts, with granodiorite and dacite having distinctly lower rubidium values than surrounding lithologies.

Figure 9-1: Soil Geochemical Sample Data for Select Elements

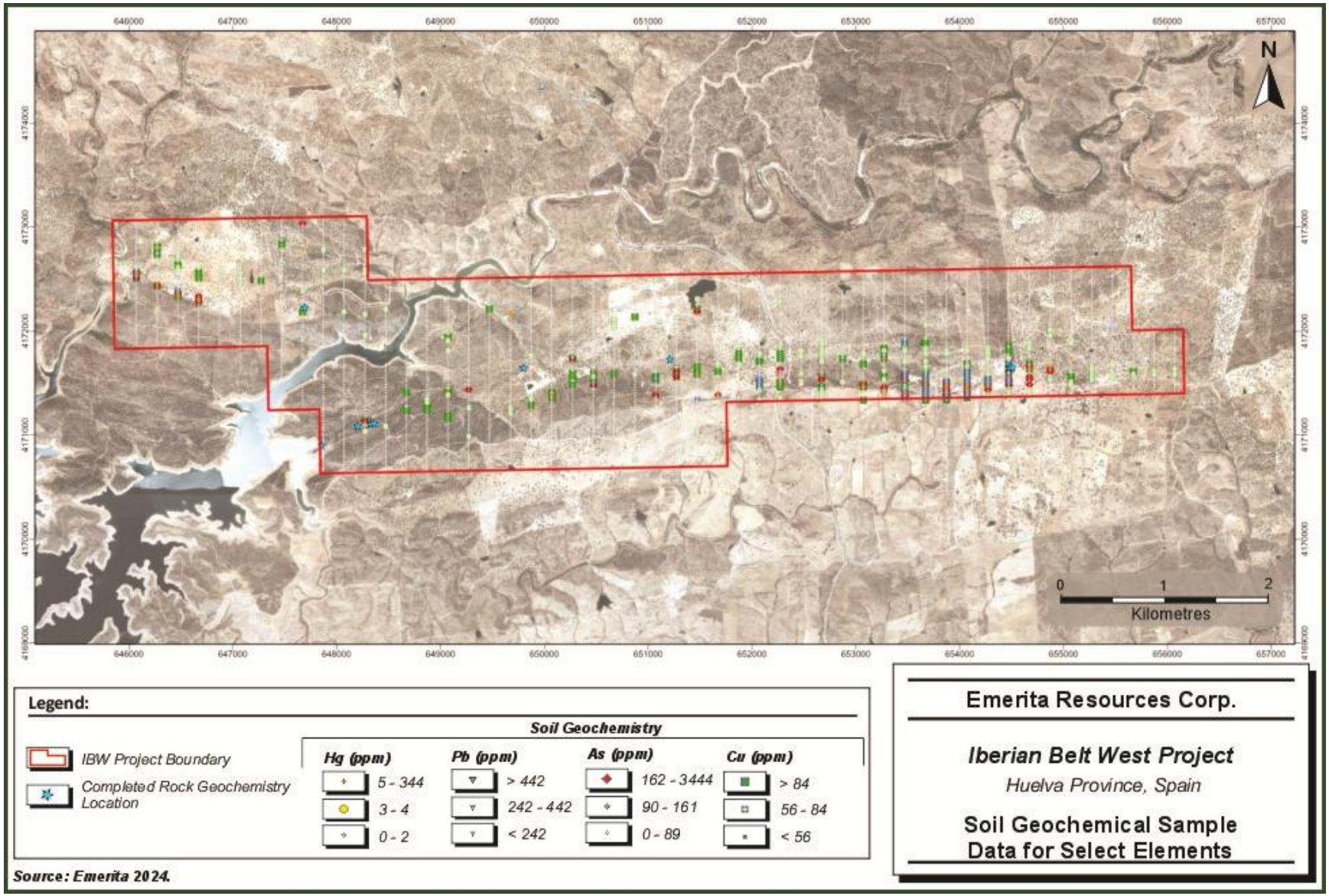
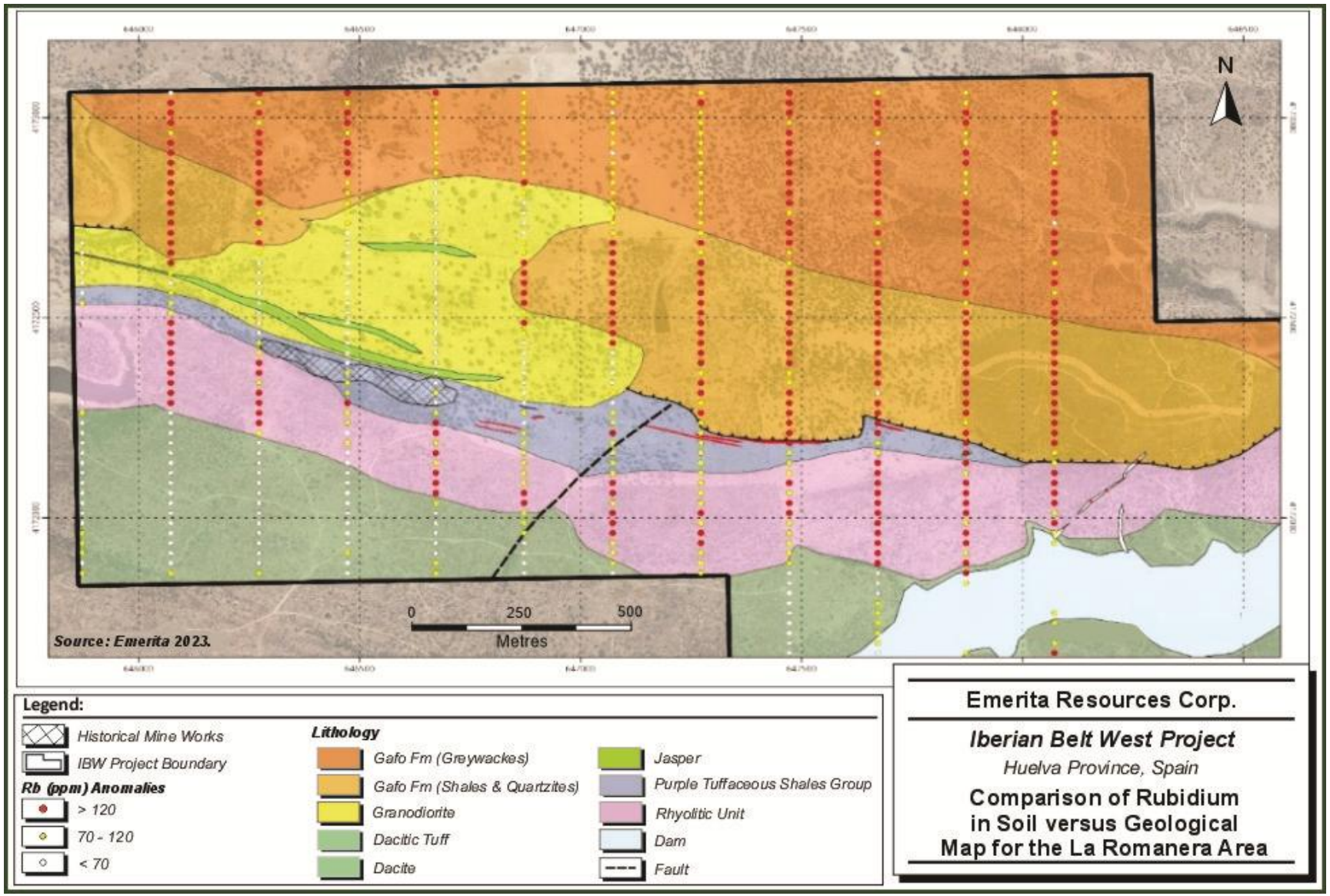


Figure 9-2: Comparison of Rubidium in Soil versus Geological Map for the La Romanera Area



9.4 Soil Vapour Geochemistry

A preliminary soil vapour survey was completed at the IBW Project by Emerita in 2025 to evaluate the potential use of mercury vapour anomalies as an exploration vector associated with VMS mineralisation.

The survey was designed based on the recognition that mercury may occur in association with sulphide mineral systems, including sphalerite and sulphosalt mineralisation, and that gaseous mercury can migrate through permeable soils and fractured rock due to natural variations in atmospheric pressure and temperature.

9.4.1 Methodology

The soil vapour survey was conducted using a NIC EMP-3 portable mercury gas spectrometer, which measures mercury concentrations in the vapour phase by atomic absorption spectroscopy. Sampling was undertaken using inert probes and tubing installed in shallow drillholes to collect representative subsurface gas samples.

Prior to measurement, the sampling system was purged to remove dead-volume air and minimise atmospheric contamination. Leak testing and controlled pumping procedures were implemented to improve sampling consistency and data quality.

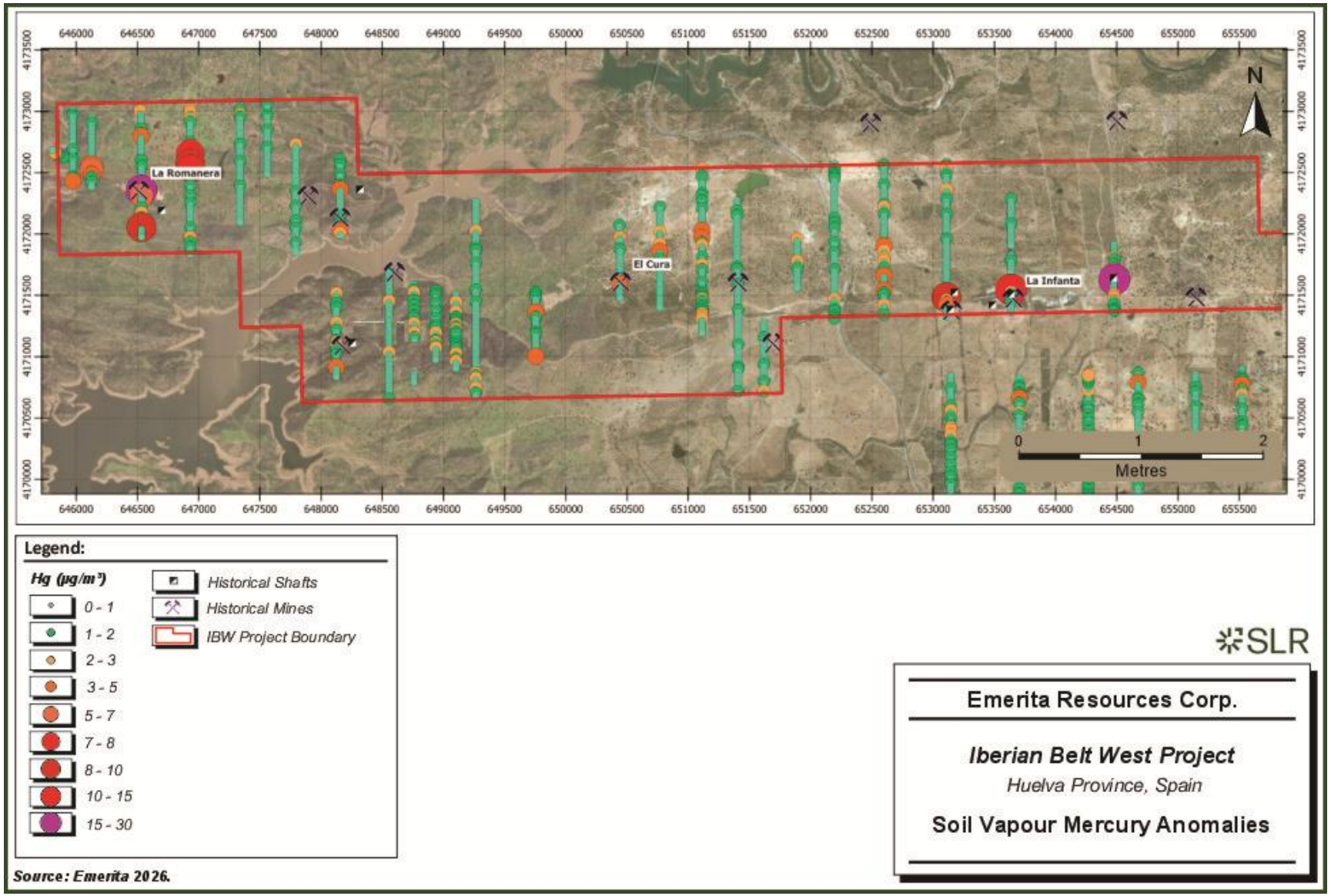
Environmental and operational parameters, including atmospheric pressure, temperature, humidity, rainfall conditions, soil conditions, and the presence of groundwater, were monitored during the survey, as these factors may influence gas migration and vapour concentrations in the subsurface.

9.4.2 Results

The preliminary mercury survey results at the Project confirm a good correlation between mercury vapour anomalies and known VMS mineralisation (Figure 9-3), which validates the reliability of the NIC EMP-3 spectrometer and the applicability of the method in the area.

Positive mercury anomalies are associated with known deposits, major structures, lithological contacts, and alteration zones, supporting the use of mercury vapour surveys as an effective exploration tool for detecting buried mineralisation trends. Overall, the survey demonstrates that mercury vapour geochemistry is a rapid and cost-effective method for regional exploration and target definition within the IBW Project area.

Figure 9-3: Soil Vapour Mercury Anomalies



9.5 Geophysics

Emerita has compiled and analysed historical gravimetric and magnetic data and has completed its own geophysical surveys, including surface gravimetrics, surface transient electromagnetics (TEM), helicopter-based magnetics and TEM, surface induced polarisation (IP)-resistivity, and downhole electromagnetics (DHEM).

9.5.1 Historical Surveys

9.5.1.1 Surface Gravity

Historical gravimetric data was provided by the Geophysics Branch of the Spanish Geological and Mining Survey (IGME). Using a common bouguer gravity value of 2.67 g/cm^3, a residual gravity grid was calculated and is shown in Figure 9-4. These data covered most of the Project area and were collected by different companies in different programmes. Evidence of historical mining was verified and subsequently compared to the compiled gravimetric data.

9.5.1.2 Airborne Magnetics

Historical magnetic data were generated by a regional airborne magnetometer survey conducted by Sander Geophysics from November 1996 to March 1997. This survey utilised a Geometrics G-822A Cesium Magnetometer Sensor system to measure total magnetic field intensity (TMI), configured on a fixed-wing (Cessna 208B Grand Caravan) aircraft. North-south lines spaced every 250 m were completed from an average 80 m height above ground, sampling every 0.1 seconds. A TMI plot over the IBW Project was generated from the results of this survey (Figure 9-5). The trend of the volcanics is clearly indicated as a magnetic high, as is the diversity of deposit settings in relation thereto.

Figure 9-4: Bouguer Anomaly Map from Historical Survey Data

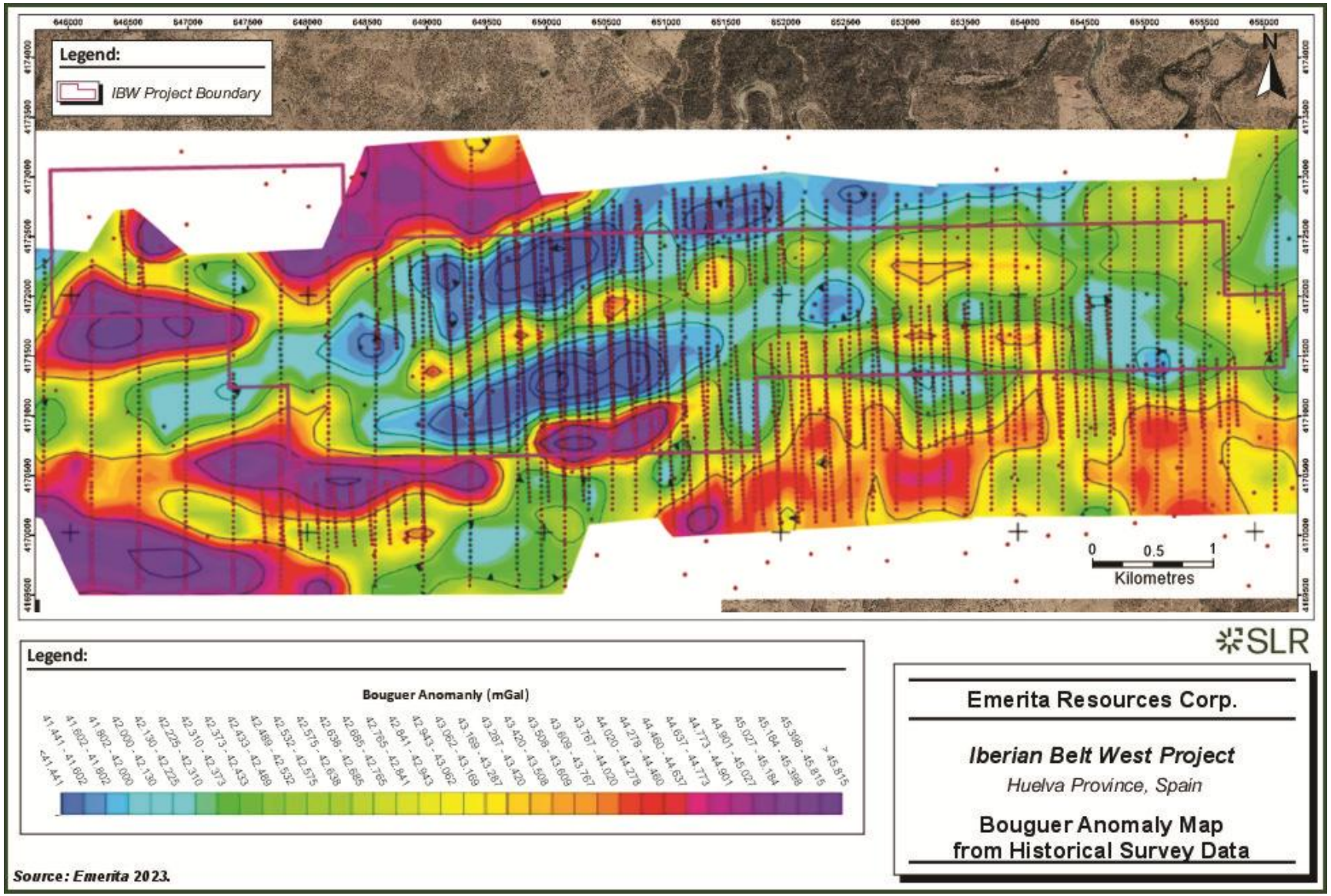
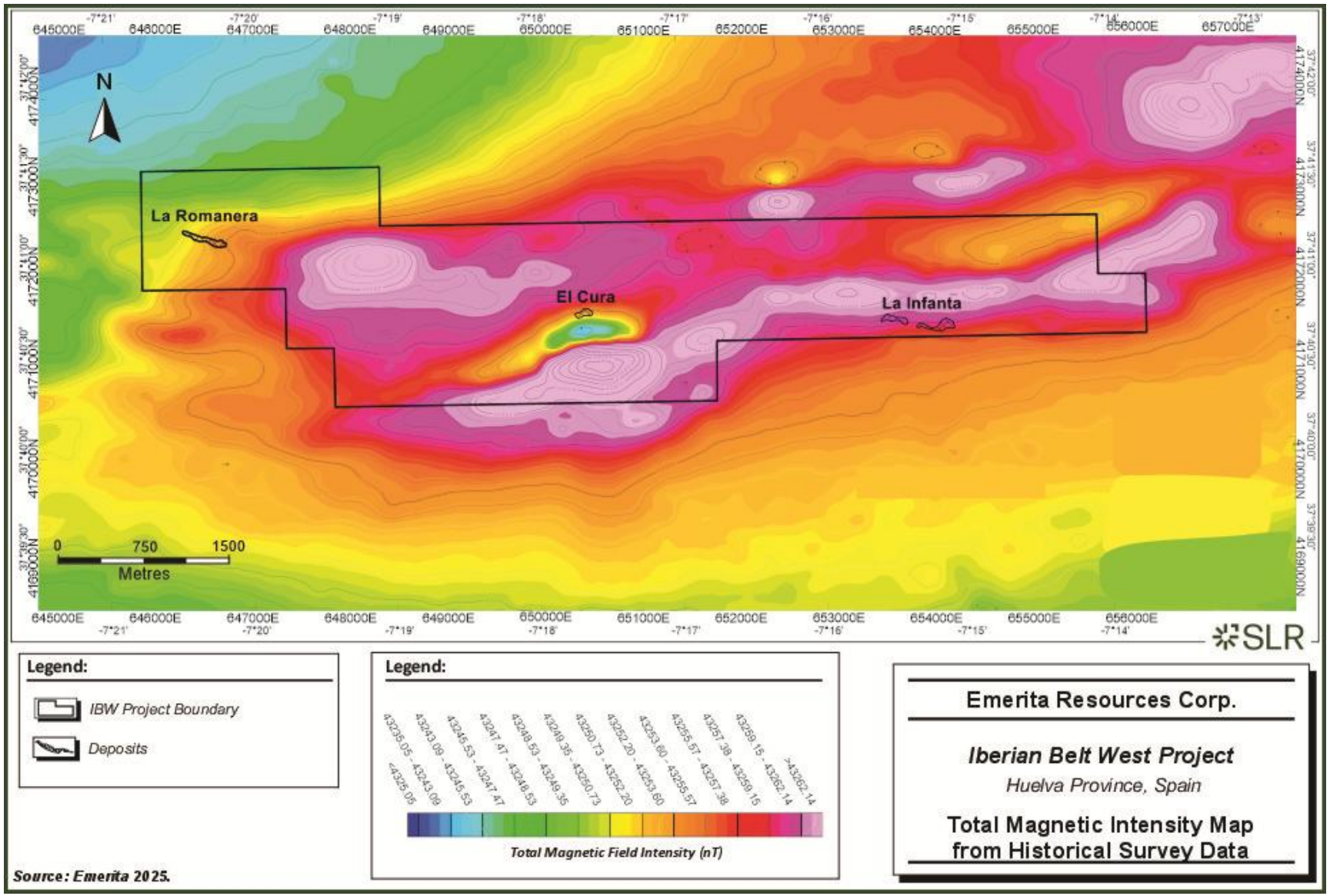


Figure 9-5: Total Magnetic Intensity Map from Historical Survey Data



9.5.2 Emerita Surveys

9.5.2.1 Surface Gravity

Emerita completed additional gravity testing over La Romanera, La Infanta, and El Cura between late 2023 and early 2024, utilizing Scintrex CG-5 and CG-6, as well as Romberg Models D and G instrumentation. Stationing was at 50 m intervals along north-south lines spaced every 200 m over the central and eastern parts of the property and along 100 m spaced lines at La Romanera. An enhanced residual Bouguer gravity map is shown in Figure 9-6, exhibiting good correlation between La Romanera and the gravity high, whereas El Cura and La Infanta are located along the edges of gravity anomalies.

9.5.2.2 Surface TEM

Emerita completed a surface TEM programme across the Project area in 2023, comprising 28 km of fixed loop (Turam) and 19 km of mobile loop (Slingram). Frequencies included 2.5 Hz, 6.25 Hz, and 25 Hz. Separation between loops ranged from 250 m to 350 m. The geophysical survey detected a series of high conductivity TEM anomalies, interpreted to trend east-west like the known VMS mineralisation (Figure 9-7).

Figure 9-6: Enhanced Residual Bouguer Gravity Map from Emerita Survey Data

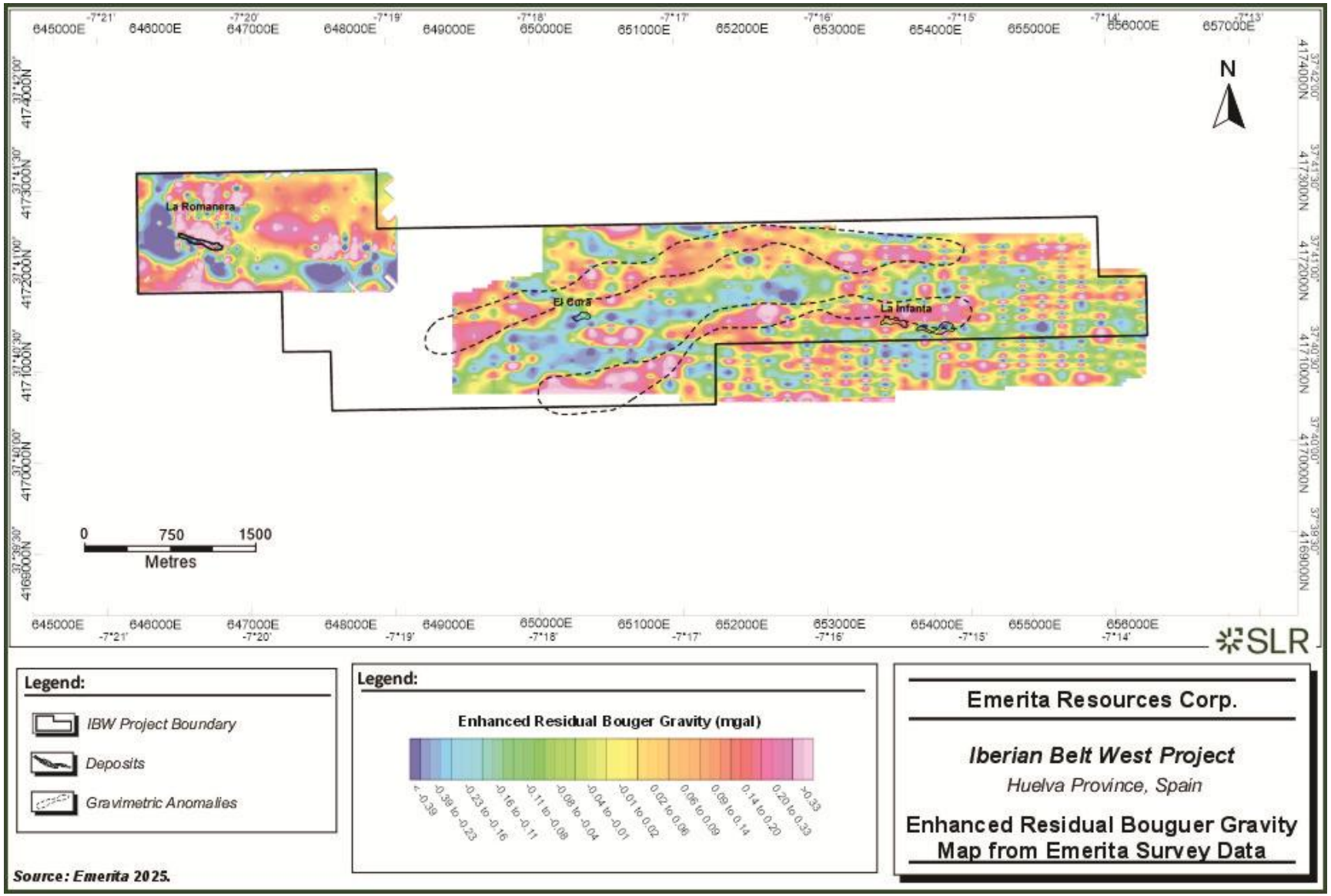
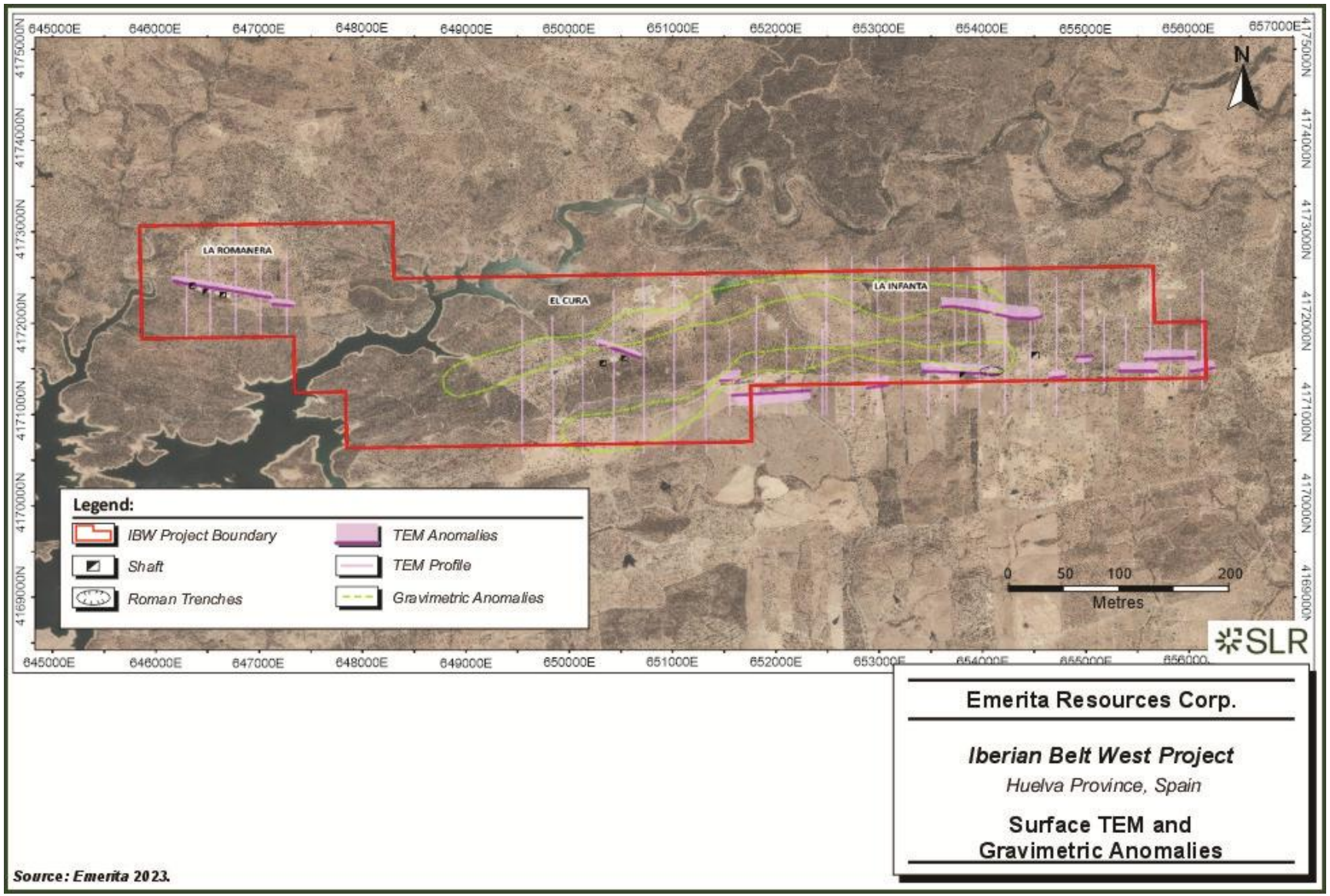


Figure 9-7: Surface TEM and Gravimetric Anomalies



9.5.2.3 Helicopter TEM and Magnetics

Emerita completed a helicopter-based geophysical survey across the entire IBW Project area in early 2026, using Xcalibur's HELITEM time domain electromagnetic system, which integrates both electromagnetic and high resolution magnetic measurements. The system consists of a 35 m diameter horizontal transmitter loop towed beneath a helicopter, with the three-component electromagnetic receiver positioned at the centre of the loop. A Scintrex CS 3 caesium vapour magnetometer was mounted between the receiver and the loop edge, allowing simultaneous acquisition of magnetic data.

To maximize depth penetration in areas with conductive sedimentary cover, the survey employed the low base frequency of 6.25 Hz, which enhances sensitivity to deeper conductors. The helicopter maintained an average terrain clearance of approximately 64 m, with variations dictated by topography and infrastructure. Flight lines were oriented north-south at 100 m spacing, with tie lines every 1,000 m.

The TEM data were recorded across multiple time windows to capture responses from near surface to deeper sources. Early-time channels highlight shallow conductivity contrasts, while mid- and late-time channels provide sensitivity to deeper conductors beneath the sedimentary cover. The system's Z component proved particularly diagnostic, as demonstrated by the La Romanera deposit, which produced a classic double peak response indicative of a steeply dipping conductor (Figure 9-8). These results confirm that the system performed as expected in detecting VMS mineralisation.

Magnetic data were acquired continuously during the TEM survey, providing complementary information on lithological variations and structural features. The caesium vapour magnetometer delivered high resolution TMI data, later processed to generate first vertical derivative (1VD) products. These results clearly delineate the volcanic units of the VSC, which exhibit higher magnetic susceptibility and appear as distinct bipolar gradients (Figure 9-9). Areas of thick sedimentary cover show very low magnetic gradients, consistent with expectations.

Figure 9-8: Helicopter Transient Electromagetics Early Channel Conductivity

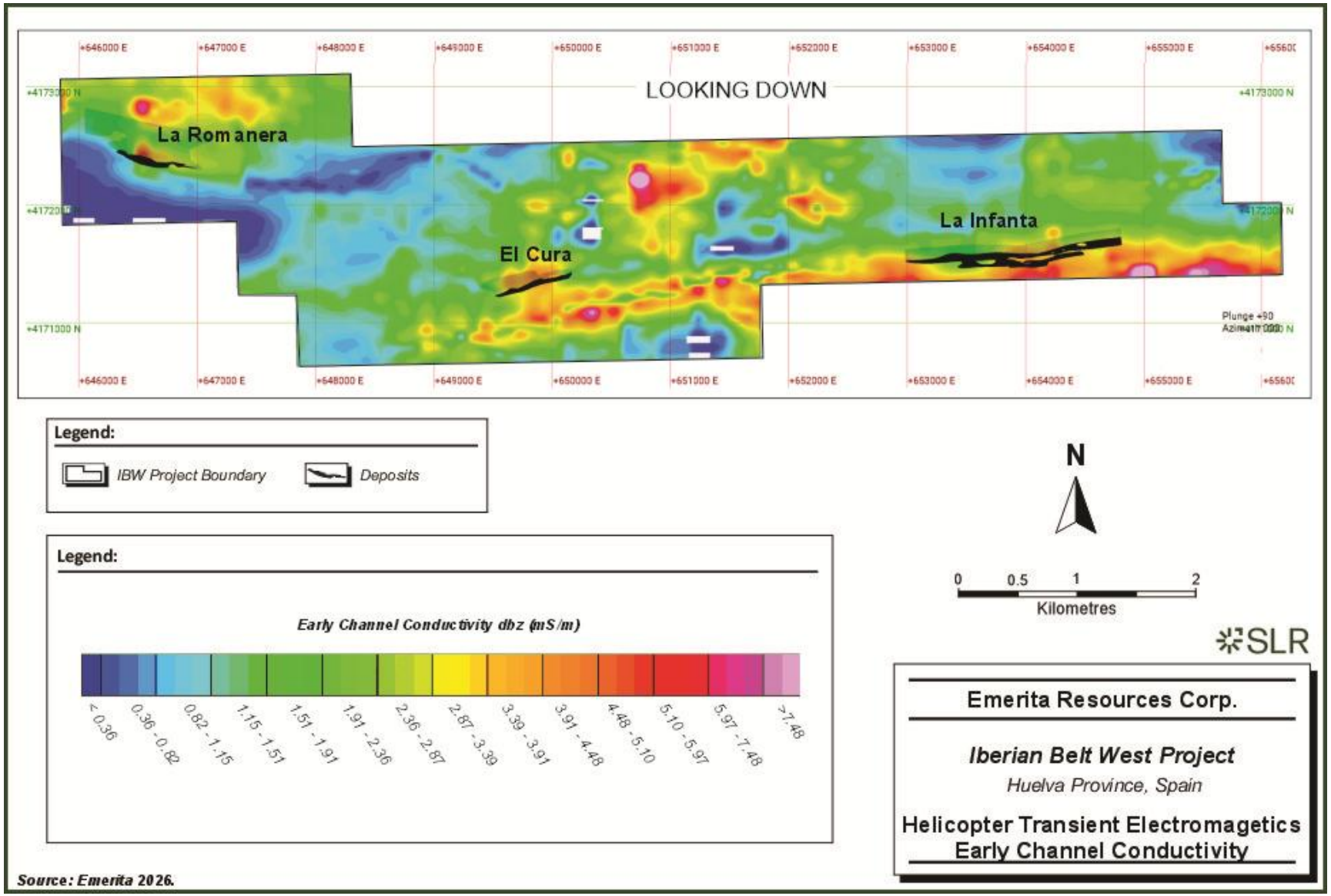
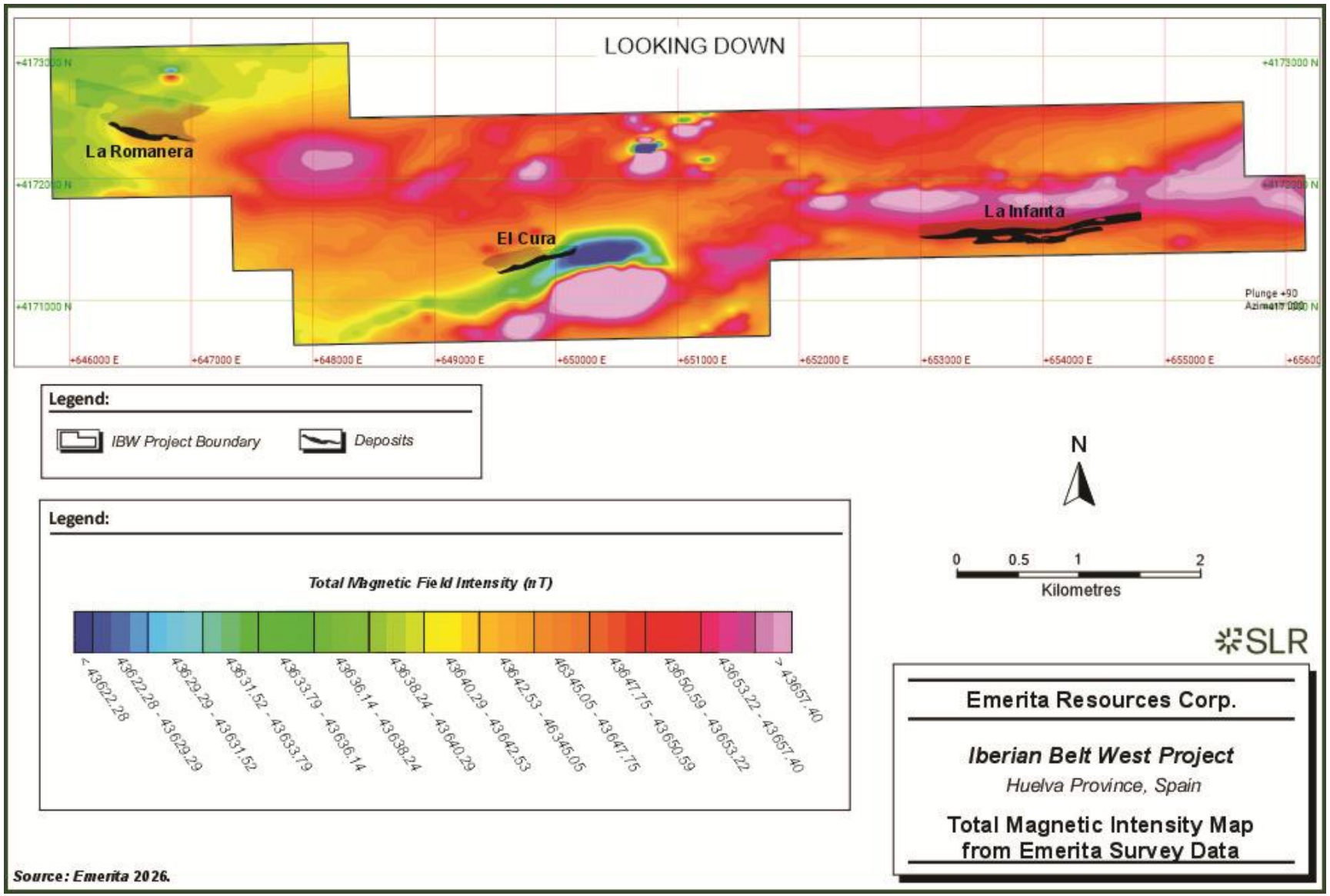


Figure 9-9: Total Magnetic Intensity Map from Emerita Survey Data



9.5.2.4 Surface Induced Polarisation-Resistivity

In September 2023, Emerita completed three lines of dipole-dipole IP-resistivity over the La Infanta deposit, coincident with previously surveyed lines of fixed-loop TEM. A resistivity low and chargeability high were recognised, coincident with the known La Infanta deposit. In 2025, a second phase of dipole-dipole IP-resistivity surveys was completed in the La Romanera and La Infanta areas. Compilations of chargeability pseudosections for each deposit are provided in Figure 9-10 and Figure 9-11, alongside interpreted chargeability trends.

9.5.2.5 Downhole Electromagnetics

To date, 15 drillholes have been surveyed with downhole-electromagnetics across the IBW Project deposits. Of these, one was completed at El Cura, one was completed at La Infanta, and the remainder were completed at La Romanera. Drillholes located on the edges of the mineralised zones were surveyed to investigate potential extensions. Measurements are collected at 10 m intervals. Results included:

- IN068: Weak anomaly between 220 m to 230 m;
- LR065: Significant conductivity mass subvertical at 560 m;
- LR087: Positive polarity indicates that the edge of ore is far from the drillhole;
- LR101: Polarity change in the mineralised zone indicating the drillhole is on an edge;
- LR117: Results indicate that the ore has continuity laterally; and
- LR142: Measured the first 100 m only and no anomaly detected.

TEM and DHEM demonstrated a good response on relatively thick massive sulphide lenses like the La Romanera deposit. For La Infanta and El Cura, the responses are more subtle.

Figure 9-10: La Romanera Chargeability Pseudosections and Interpreted Trends

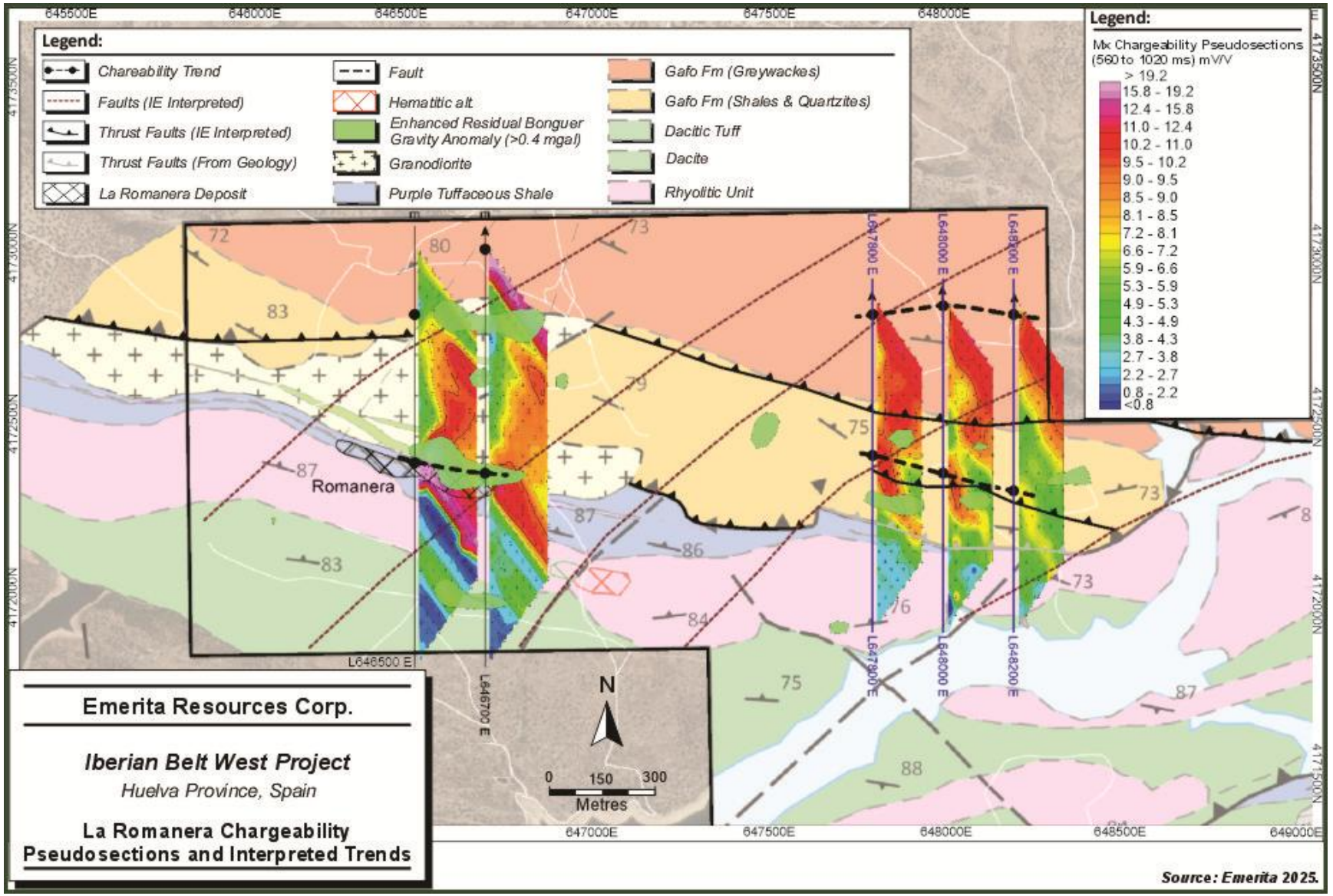
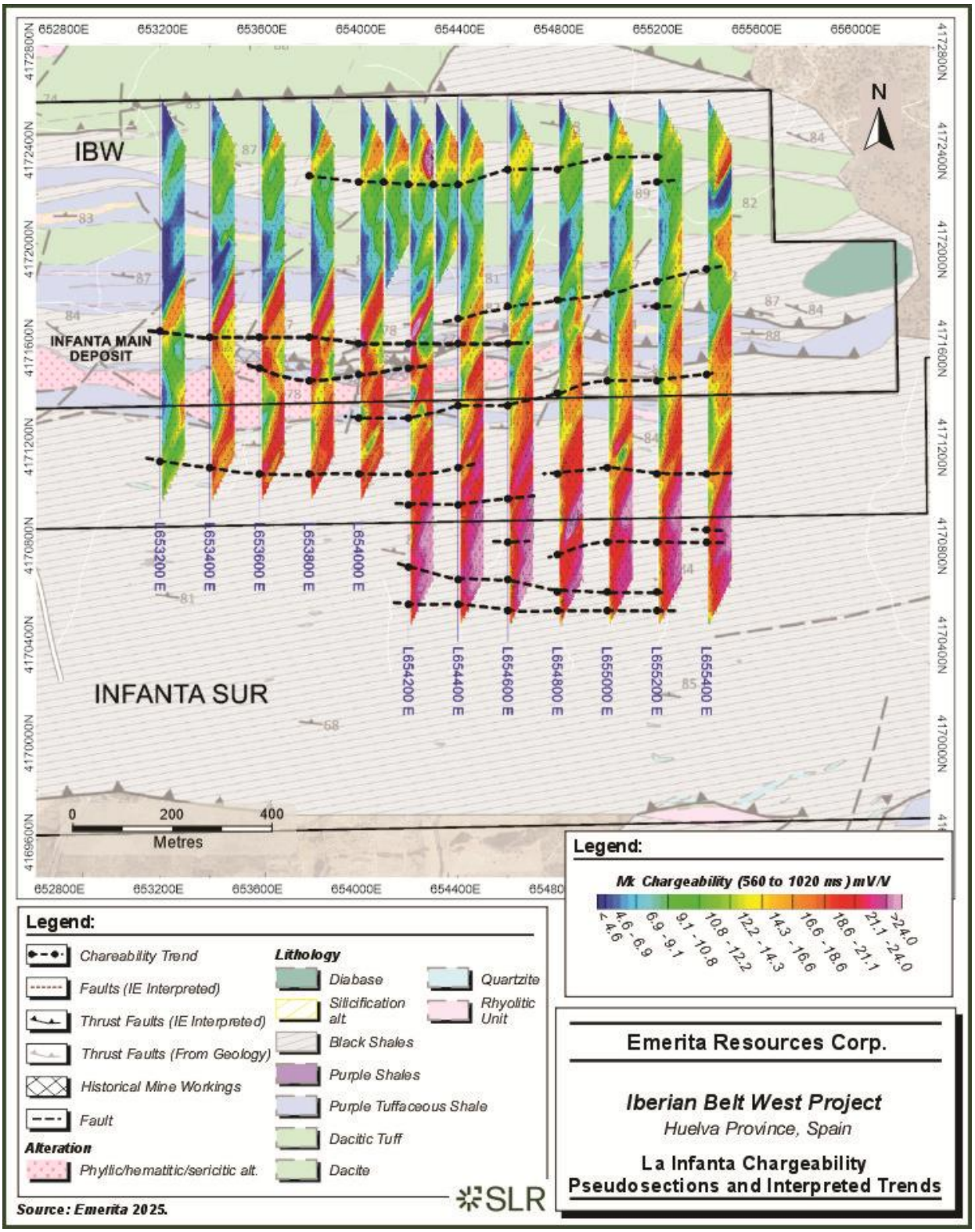


Figure 9-11: La Infanta Chargeability Pseudosections and Interpreted Trends



10.0 Drilling

10.1 Historical Drilling (Prior to 2021)

Historical drilling is described in Section 6.2. Limited supporting documentation is available for historical drilling and it has been excluded from the MRE database, with drill coverage replaced by Emerita drilling. Only Emerita drilling is described in the remainder of this section.

10.2 Emerita Drilling (2021 to Present)

Emerita's exploration strategy has focused on diamond drilling (DDH) from surface. Over 120 km (Table 10-1 and Figure 10-1) of diamond drilling has been carried out since 2021 in three broad phases:

1 From July 2021 to June 2022 most drilling was carried out in the La Infanta area.

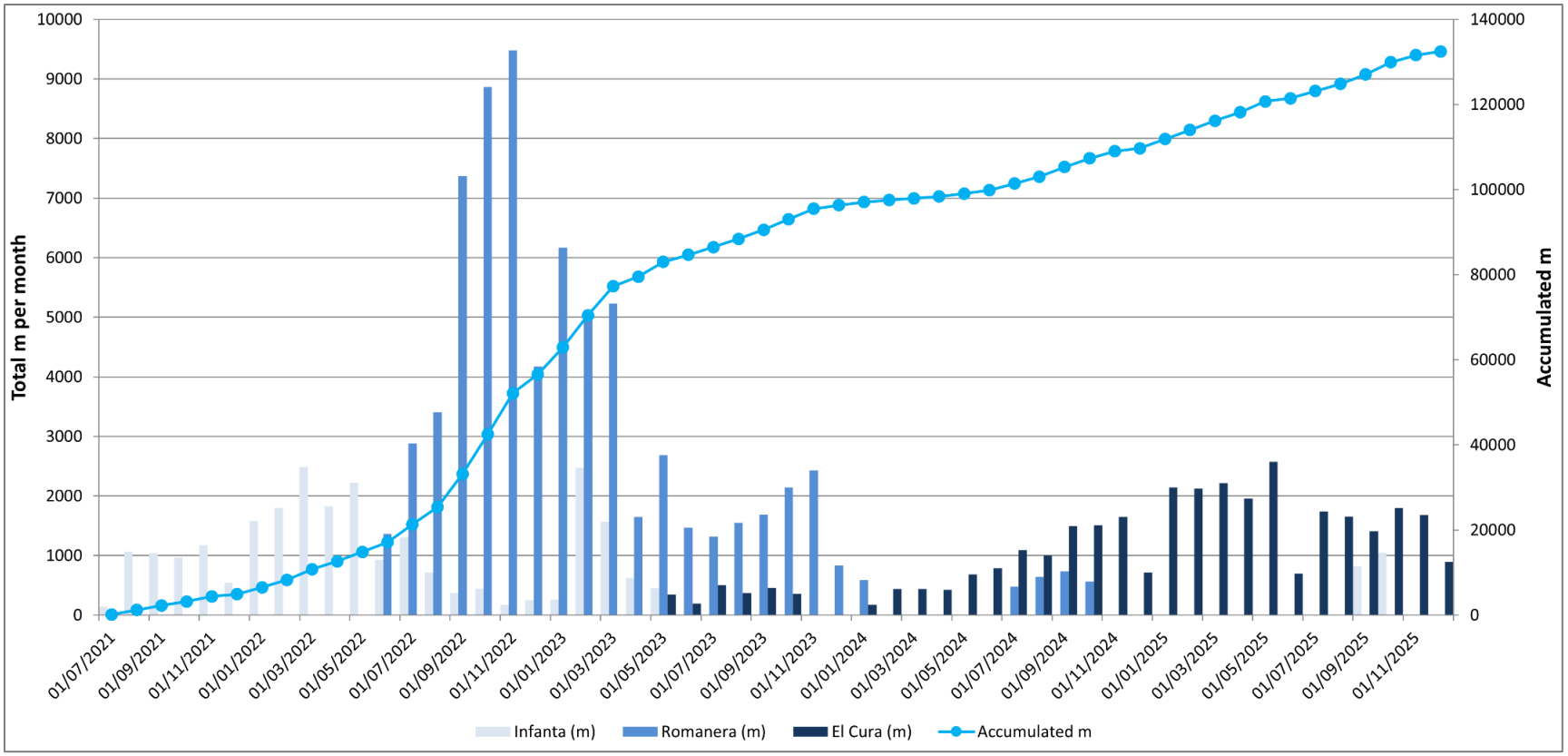
2 From June 2022 to January 2024 diamond drilling increased substantially when drilling began in the La Romanera area.

3 From January 2024 to present the drilling focus shifted to El Cura.

Table 10-1: Emerita Diamond Drilling by Year and in Total at Each Deposit (MRE Databases)

Area	Metric	2021	2022	2023	2024	2025	Total
La Infanta	Number of Drillholes	31	38	22		1	92
	Metres Drilled	4,511.3	10,796.9	5,666.8		672.2	21,647.1
La Romanera	Number of Drillholes		92	71	6		169
	Metres Drilled		34,779.1	31,863.1	3,702.1		70,344.3
El Cura	Number of Drillholes			6	26	59	91
	Metres Drilled			2,118.8	9,896.2	19,235.0	31,250.0
Total	Number of Drillholes	31	130	99	32	60	352
	Metres Drilled	4,511.3	45,576.0	39,648.7	13,598.3	19,907.2	123,241.3

Figure 10-1: Monthly Drilling Statistics (2021-2025)



Source: Emerita 2026.

10.2.1 La Romanera

No new drilling has been completed at La Romanera since the previous MRE (effective date February 26, 2025).

Figure 10-2 shows the location and azimuth of Emerita diamond drilling at La Romanera. Multiple holes are drilled from a single collar to minimise rig moves, drill site preparation, and environmental disturbance. Azimuth (180° to 220° typical) and dip (50° to 70° typical) are varied to cover a coherent panel of the deposit in long section.

The cross-section in Figure 10-3 shows the typical sample coverage and range of dip orientations. This drillhole configuration means downhole widths typically vary from 60% to 100% of true width. Nominal drill spacing is 50 m x 50 m in the core of the deposit, increasing to 100 m x 100 m on the periphery.

10.2.2 La Infanta

A single deep exploration hole (INN08) has been drilled at La Infanta since the previous MRE (effective date February 26, 2025) and prior to the MRE database cut-off date (January 16, 2026).

Figure 10-4 shows the location and azimuth of Emerita diamond drilling at La Infanta. Holes have been drilled on a broadly consistent azimuth around 175°.

The cross-section in Figure 10-5 shows the typical sample coverage and dip orientation around 50°. This drillhole configuration means downhole widths typically vary from 80% to 90% of true width. Nominal drill spacing is locally 50 m x 50 m in the upper 150 m of the deposit, increasing to greater than 100 m x 100 m in the down-dip and strike extensions.

10.2.3 El Cura

An additional 52 drillholes for 17,015 m of drilling has been completed at El Cura since the previous MRE (effective date February 26, 2025) and prior to the MRE database cut-off date (January 16, 2026).

Figure 10-6 shows the location and azimuth of Emerita diamond drilling at El Cura. Similar to Romanera, multiple holes are drilled from a single collar. Azimuth (140-200° typical) and dip (40-80° typical) are varied to cover a coherent panel of the deposit in long section.

The cross-section in Figure 10-7 shows the typical sample coverage and range of dip orientations. This drillhole configuration means downhole widths typically vary from 70% to 90% of true width. Nominal drill spacing is locally 50 m x 50 m in the core of the deposit, increasing to >100 m x 100 m in the dip and strike extensions.

Figure 10-2: La Romanera Drill Plan

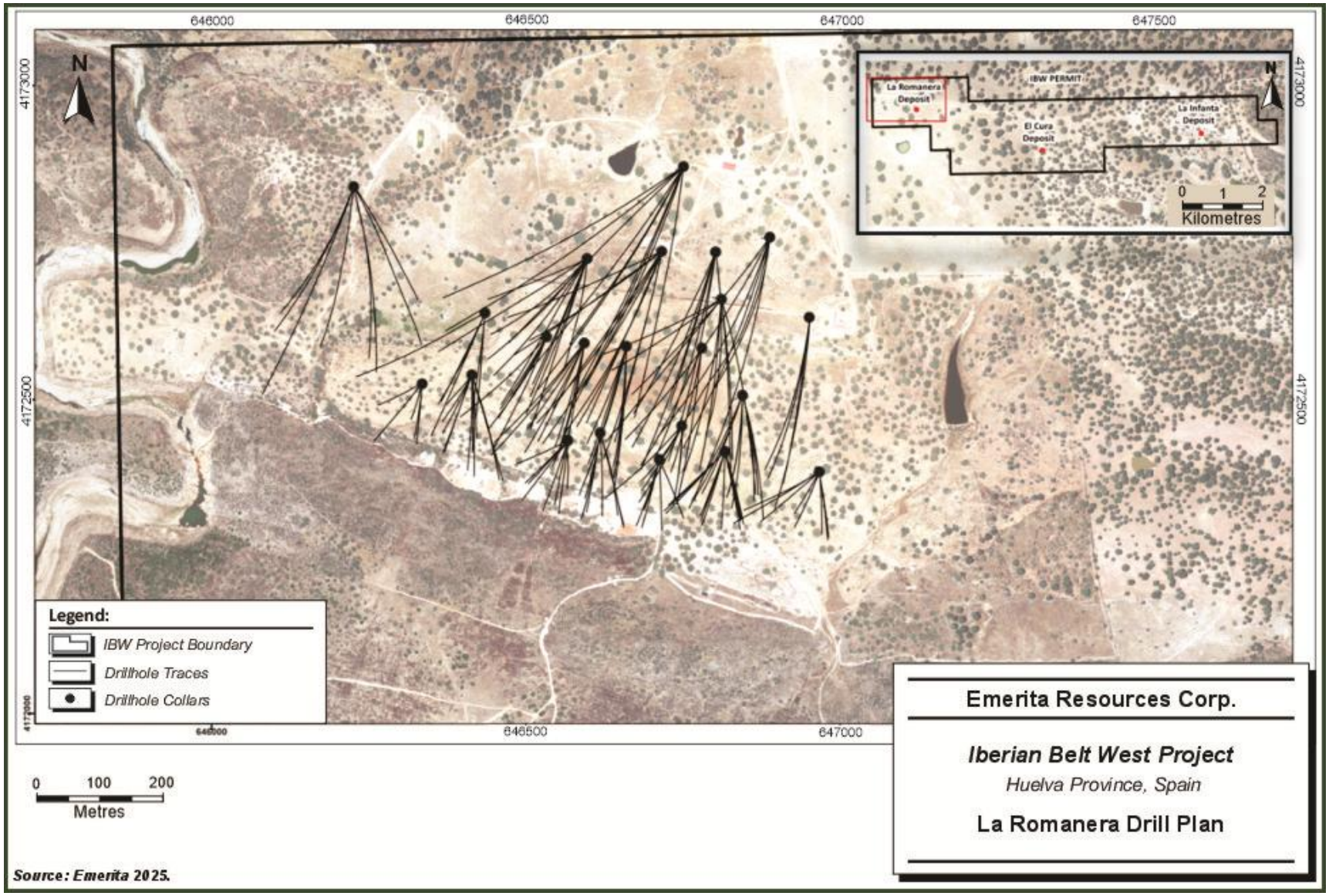


Figure 10-3: Representative La Romanera Drill Section

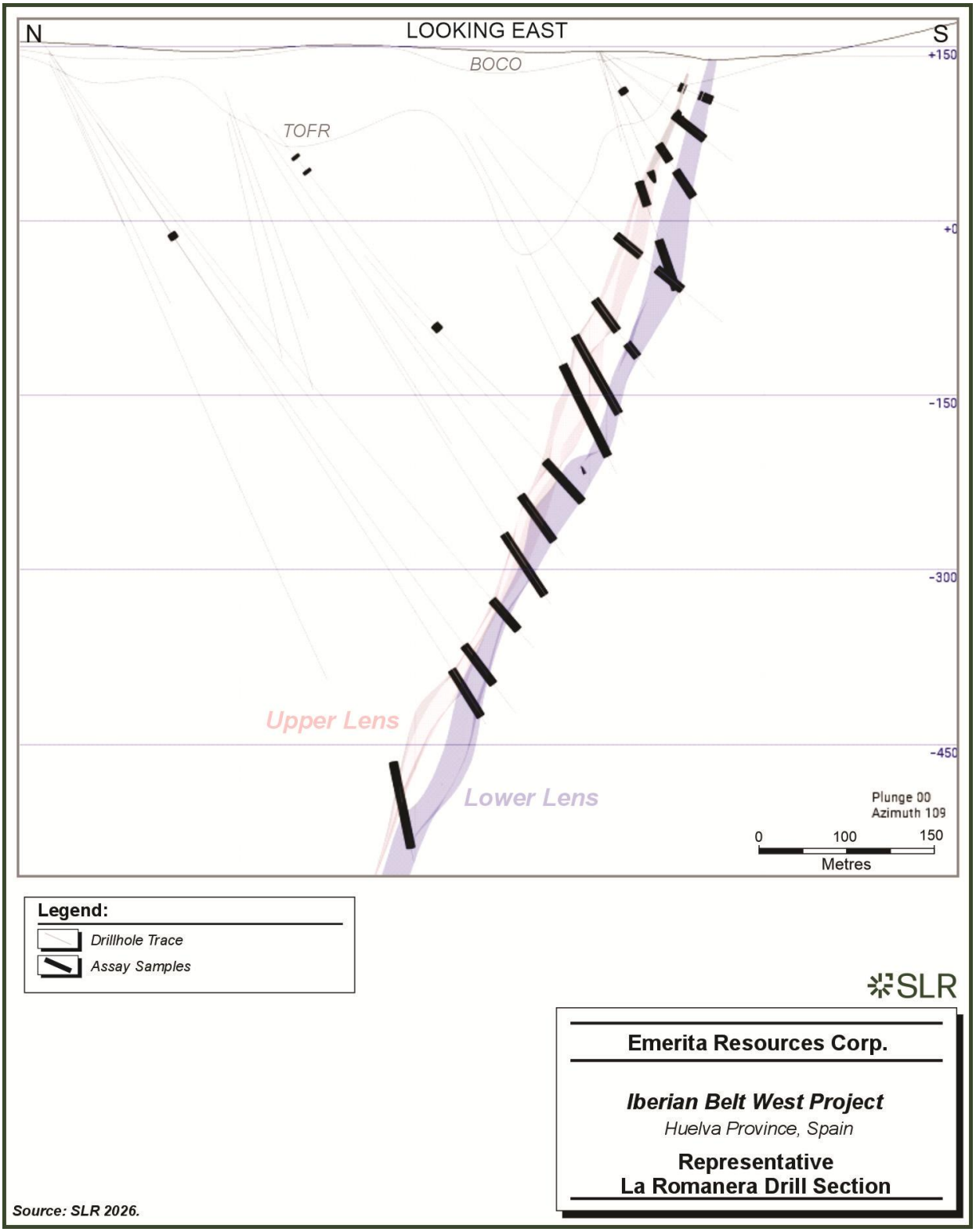


Figure 10-4: La Infanta Drill Plan

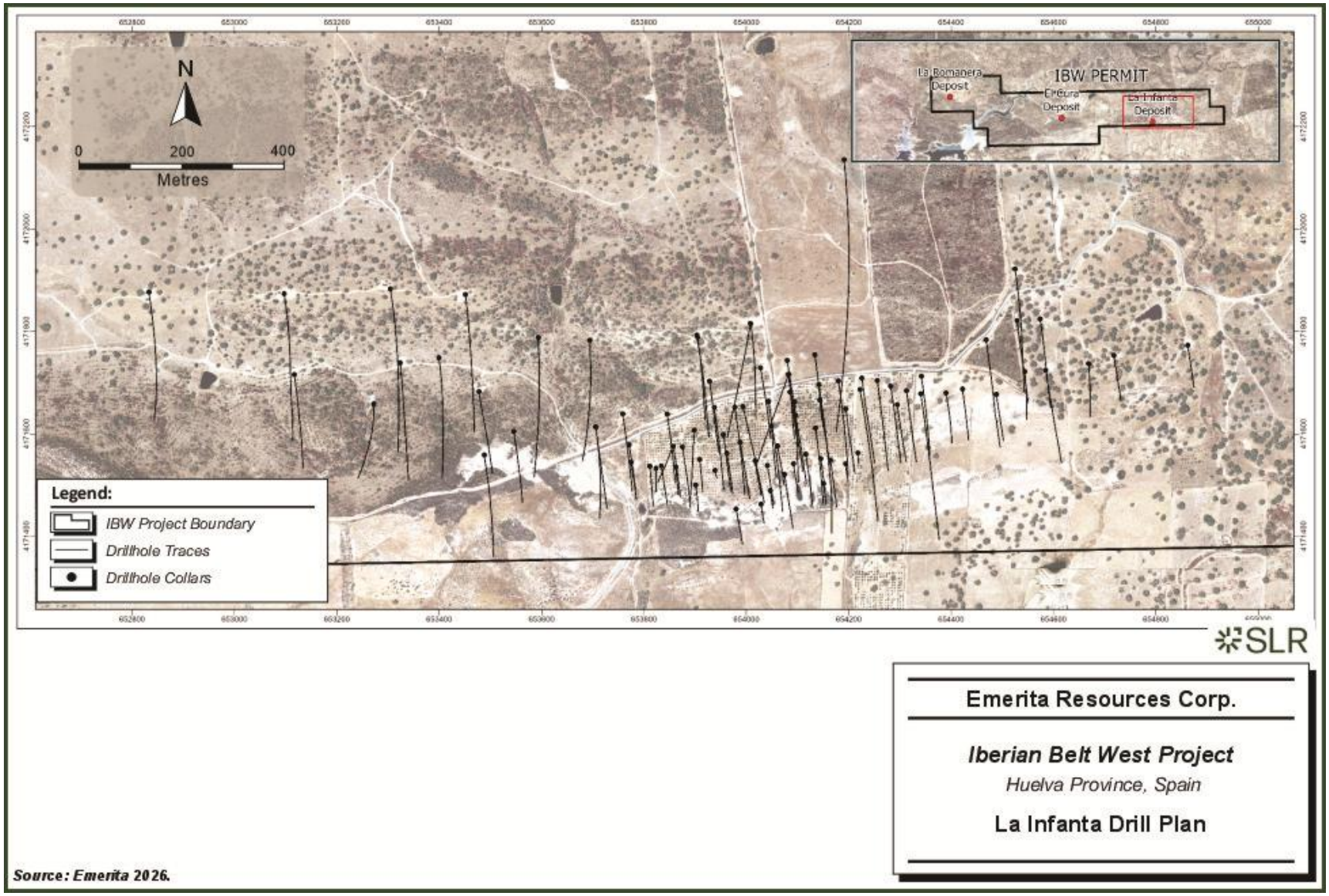


Figure 10-5: Representative La Infanta Drill Section

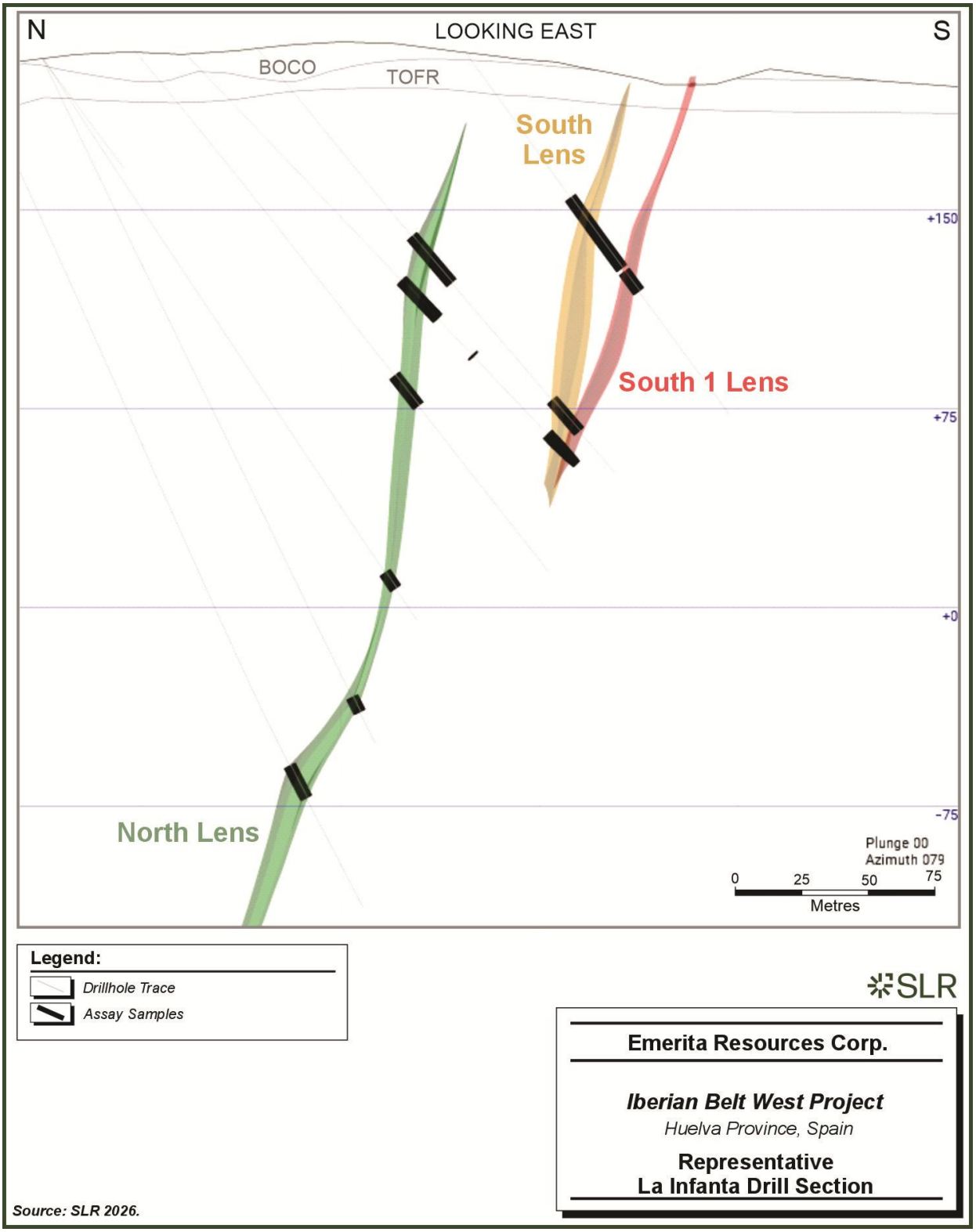


Figure 10-6: El Cura Drill Plan

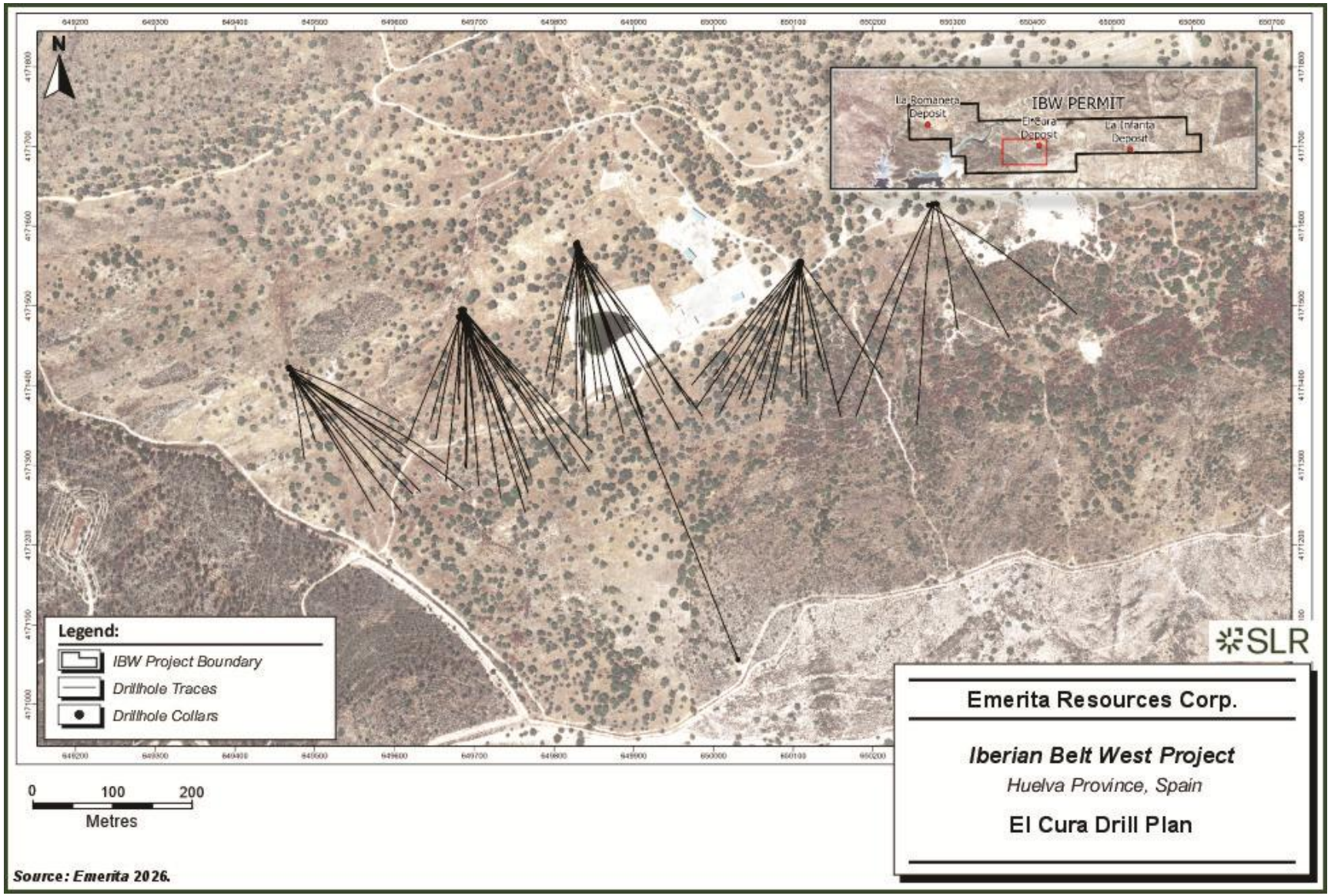
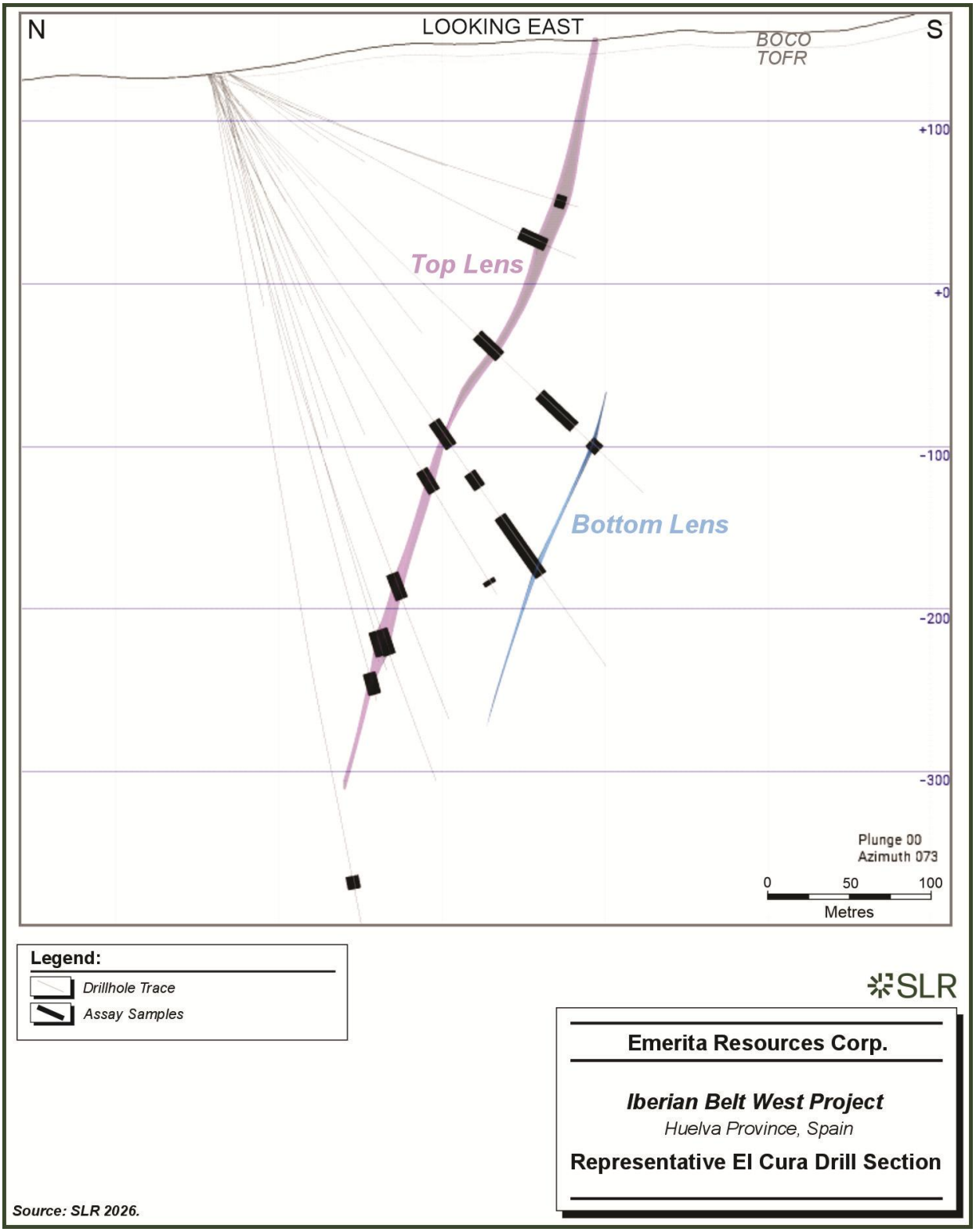


Figure 10-7: Representative El Cura Drill Section



10.3 Drilling Procedures

10.3.1 Drilling Method

All drillholes completed by Emerita at La Romanera, La Infanta, and El Cura are diamond drillholes. Drilling was conducted by specialist contractors under the supervision of Emerita personnel. Diamond drilling includes PQ (85 mm), HQ (63.5 mm), and NQ (47.6 mm) core diameters. For initial metres, just below the weathering zone, PQ is used. Then, the hole continues in HQ until the end of the hole. When downhole issues arise, NQ can occasionally be used. A typical diamond drilling operation at the Project is shown in Figure 10-8.

Figure 10-8: Diamond Drilling Operations at La Romanera



Source: Emerita 2023.

Drill core is extracted from the core barrel directly into core boxes at the drill rig. Each core box is marked with the drillhole ID and the from and to depths of the interval within each box. Drillers insert labelled core blocks into the box to record the depth at the end of each run.

10.3.2 Collar Survey

Surveying of all drillhole collar locations was done by Geoavance, an independent contractor. Geoavance uses a GEOMAX GPS, model ZENITH60, with serial number Z60ST272100139. This system includes an RTK GNSS receiver that supports differential positioning up to centimetre-level accuracy.

10.3.3 Downhole Survey

All drillholes are downhole surveyed at 10 m intervals to capture hole dip and azimuth. A summary of the tools used is provided in Table 10-2. Emerita is currently using the SPT MagCruiser with an optical depth counter (Figure 10-9).

Table 10-2: Summary of Downhole Survey Tools

Tool	Dip Precision	Azimuth Precision	Dip Range
GyroMaster™ 2074	± 0.05°	± 0.5°	-90° a +90°
GyroLogic™ 29	± 0.05°	± 0.3°	-85° a +85°
GyroLogic™ 11	± 0.05°	± 0.3°	-85° a +85°
Reflex EZ-TRACK™	± 0.25°	± 0.35°	-90° a +90°
MagCruiser™ MM013	± 0.05°	± 0.3°	-90° a +90°

Figure 10-9: GyroLogic SPT Downhole Survey Tool and Optical Depth Counter



Source: Emerita 2023.

10.3.4 Logging

Core boxes are collected from the rig and taken to the Emerita core shed where the core is logged and processed (Figure 10-10).

Figure 10-10: Emerita Core Processing Facility



Source: SLR 2026.

All data is captured in a relational database using MX Deposit software. The logging procedure is as follows:

- Core boxes are placed in order from left to right and the boxes are marked with the hole ID and metres.
- Core is fitted and oriented in one preferred direction.
- Core is wet and photographed.
- Core recovery and rock quality designation (RQD) is measured.
- Units and lithologies are logged. Descriptive logging includes colour, texture, alteration, structures, grain size, veining, presence/absence of mineralisation, type and composition of the mineralisation, and other relevant information.
- Assay sample intervals are marked on the boxes and the core using a permanent marker. Sampling is selective based on logging observations. Sample intervals do not cross lithological contacts.

- The photographs are uploaded into a company information storage system.
- Density measurements are taken on barren zones and sample intervals using the standard water displacement method (Section 11.2).

10.3.5 Core Recovery

Core recovery is calculated by dividing the length of a measured interval by the total length of the core run to determine the recovery percentage. Natural fractures are counted and grouped within the defined interval.

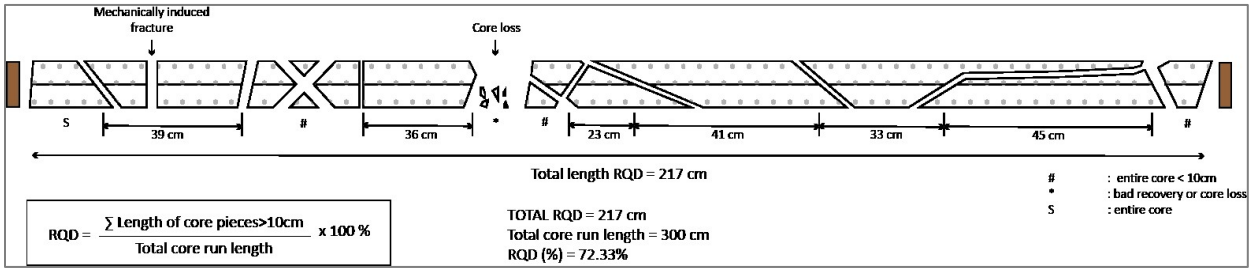
Average recovery percentage at La Romanera is 98.9%, at La Infanta is 95.5%, and at El Cura is 97.4%. No correlation between metal grades and core recovery has been observed. The QP considers that there are no material issues arising from drill core recovery and that the attained core recoveries are acceptable for use in Mineral Resource estimation.

10.3.6 Rock Quality Designation

RQD is the sum of all core fragments larger than 10 cm, measured along the centerline in a geotechnical interval, considering only natural discontinuities (Figure 10-11). This RQD length is then compared with the total core run length of the interval to obtain the RQD percentage.

RQD qualification at the Project was assigned using the Deere & Deere (1988) classification scheme. For La Romanera, the mean RQD is 88.9%, indicating that rock quality is good. For La Infanta, the mean RQD is 73.3%, indicating the rock quality is fair. For El Cura, the mean RQD is 68.5%, indicating the rock quality is fair.

Figure 10-11: Procedure for Measuring and Calculating RQD



Source: Modified from Deere & Deere 1988.

10.4 Interpretation of Relevant Results

Relevant drill sections showing the geological model for the La Romanera, La Infanta, and El Cura deposits are illustrated in Section 7.3. The drill assay results, geological logging, and geological model have enabled the 3D delineation of the VMS lenses for use in Mineral Resource estimation as outlined in Section 14.0.

The QP considers that drilling and core sample collection at the IBW Project are undertaken by competent personnel using procedures consistent with industry best practice. Drill angles are designed to intersect mineralised domains at a near-perpendicular angle, but given the nature of fan drilling, this is not always possible. The QP concludes that the samples are representative of the mineralisation and there is no evidence that the drilling or sample collection process has introduced a bias that could materially impact the accuracy and reliability of the results.

11.0 Sample Preparation, Analyses, and Security

11.1 Sampling Methods

11.1.1 Core

Emerita geologists manage the core sampling and select sampled zones based on lithology, texture, alteration, and mineralisation. To ensure sample size is within laboratory requirements, a minimum and maximum length is defined according to the diameter of the core (Table 11-1).

Table 11-1: Sample Length Depending on Core Diameter

Core Diameter	Minimum Length	Maximum Length
PQ	20 cm	100 cm
HQ	50 cm	150 cm
NQ	80 cm	200 cm
BQ	45 cm*	150 cm*
Note: Whole core sampled.		

Modal assay sample length is 1 m for all deposits. Samples are marked on the core and the core boxes with a permanent marker by two arrows, one at the beginning of the sample interval and the other at the end. The cut line is marked in the middle of the core following the apex of the foliation as a guide for the core saw operator.

Each sample is assigned a tag with a unique sample number and bar code. Samples are cut in half using a diamond core saw along the cut line. One half is collected for analysis by placing it in a sample bag together with the sample tag. The sampling record is preserved by the core box labels and the markup that is retained on the unsampled half of the core.

11.1.2 Soil

Soil sampling for geochemical analysis is supervised by a geologist. The procedure starts by locating the sample point in the field with a GPS. The sample is collected using a mattock or a pickaxe, depending on the hardness of the soil. The topsoil layer is removed until the bedrock is visible. The sampling depth is up to 30 cm to 40 cm, depending on the area.

Once the sample is collected with the mattock or pickaxe, it is double-sieved using a 0.5 mm mesh to pre-screen oversize: first to a bowl, and then from the bowl to a sample bag, which is closed with a cable tie (Figure 11-1).

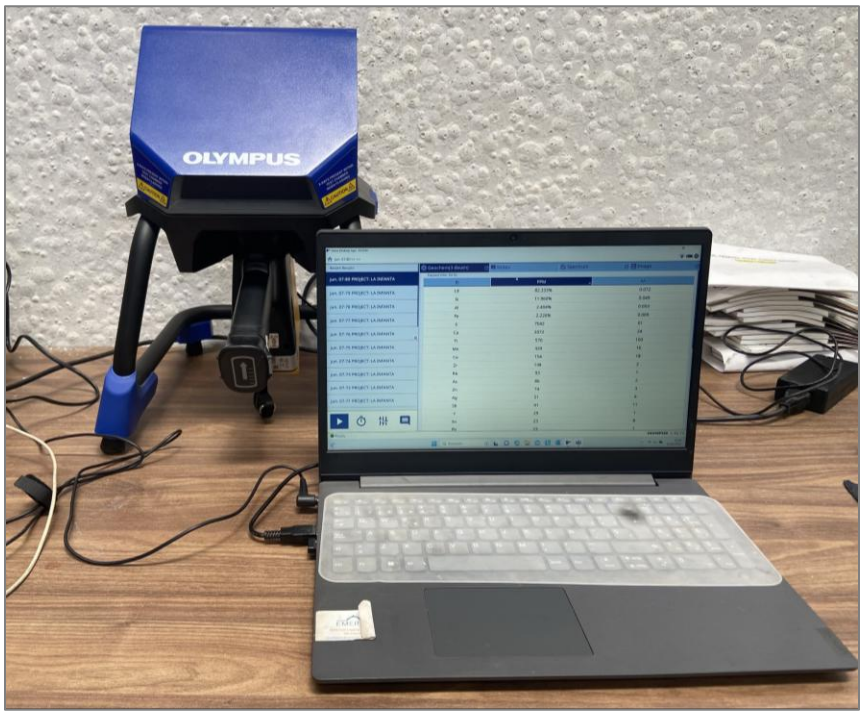
To date, the soil sample weights have been approximately 200 g. Each sample bag is labelled and analysed with an Olympus Vanta portable X-ray fluorescence (pXRF) device (Figure 11-2).

Figure 11-1: Soil Sampling Process



Source: Emerita 2023.

Figure 11-2: Olympus Vanta pXRF



Source: Emerita 2023.

11.2 Bulk Density

Bulk density measurements are performed by Emerita geological staff at the core logging facility on barren and mineralised zones using the following sample selection procedure:

- Lithological density samples. One sample of bulk lithology density every 10 m at 10 cm to 20 cm sample lengths.
- Ore density samples. One sample of bulk sample density within each assay sample at 10 cm to 20 cm sample length.

Weight measurements are taken for both dry and wet conditions to calculate the bulk density of the samples by using the following formula:

$$\boldsymbol{\rho} = \frac{\boldsymbol{x}}{(\boldsymbol{x}-\boldsymbol{y})}$$ where *x* represents the dry weight and *y* the immersed (wet) weight

Emerita uses a U.S. Solid brand USS-DBS28-30 model balance and a GRAM brand EH-6000 model balance for sample weighing. The precision of the balances are 0.01 g and 0.1 g, respectively. The method for the wet weighing is based on the suspension of the sample in a metal basket inside a water tank that allows the sample to be submerged (Figure 11-3).

Figure 11-3: U.S. Solid USS-DBS28-30 Balance Taking a Wet Weight for Bulk Density Calculation



Source: Emerita 2023.

A subset of bulk density measurements completed by Emerita (EMO) has been repeated by ALS Global (ALS) using the water displacement method (OA-GRA09). The subset included 110 samples from La Infanta, 51 samples from La Romanera, and 195 samples from El Cura.

Summary statistics for the repeat density measurements are listed in Table 11-2. Scatter plots for each deposit are presented in Figure 11-4. Results indicate strong measurement precision for El Cura and La Romanera and reasonable measurement precision for La Infanta. The scatter plots are colour-coded by lithology; a comparison of mean density by lithology is provided in (Table 11-3). Both show a potential weak bias towards higher semi-massive and massive sulphide densities in ALS measurements. This is not considered material, and the QP considers Emerita's density measurement procedure to be adequate, with notable improvements in precision in the more recent measurements from El Cura drilling.

Table 11-2: Summary Statistics for Density Reanalysis Results

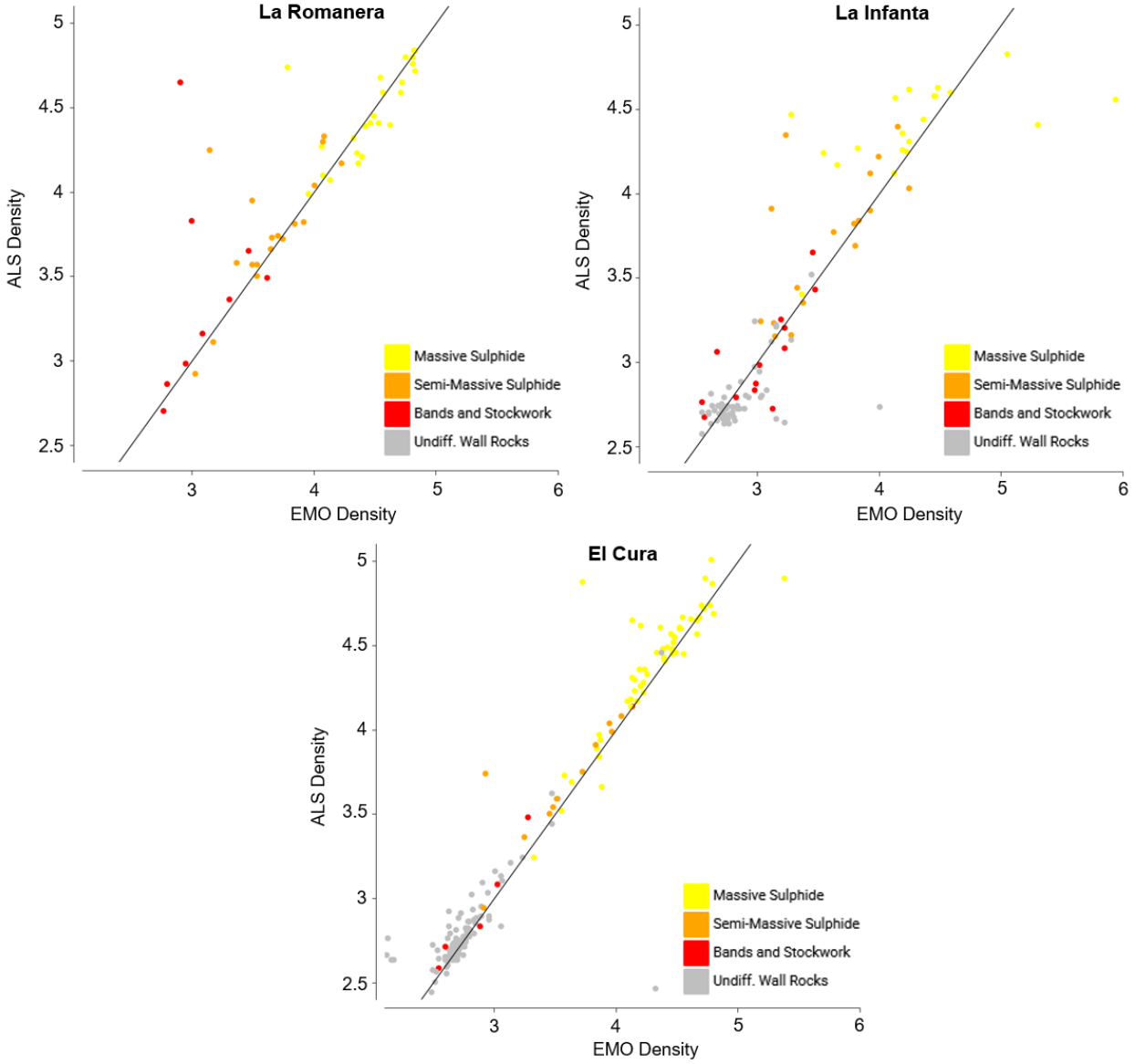
Deposit	Number of Pairs	EMO Mean (g/cm^3)	ALS Mean (g/cm^3)	EMO CV	ALS CV	Correlation Coefficient	% of Pairs <10% HARD
La Romanera	51	3.94	4.04	0.16	0.14	0.83	92.2
La Infanta	110	3.25	3.25	0.21	0.21	0.86	94.5
El Cura	195	3.24	3.30	0.24	0.24	0.97	96.9

Note:
1. CV = coefficient of variation; HARD = half absolute relative difference

Table 11-3: Summary Statistics for Density Reanalysis Results By Lithology

Deposit	Lithology	Number of Pairs	EMO Mean (g/cm^3)	ALS Mean (g/cm^3)	Difference	% Change
La Romanera	All	51	3.94	4.04	0.10	2.6%
	Massive Sulphide	24	4.47	4.48	0.00	0.1%
	Semi-Massive Sulphide	18	3.64	3.76	0.12	3.3%
	Banded and Stockwork	9	3.09	3.41	0.32	10.2%
	Undiff. Wall Rocks	0	0.00	0.00	0.00	0.0%
La Infanta	All	110	3.25	3.25	-0.01	-0.2%
	Massive Sulphide	20	4.28	4.38	0.10	2.4%
	Semi-Massive Sulphide	17	3.58	3.74	0.16	4.6%
	Banded and Stockwork	15	3.12	3.00	-0.12	-3.8%
	Undiff. Wall Rocks	58	2.84	2.78	-0.06	-2.2%
El Cura	All	195	3.24	3.30	0.05	1.6%
	Massive Sulphide	55	4.31	4.39	0.08	1.8%
	Semi-Massive Sulphide	11	3.55	3.68	0.13	3.7%
	Banded and Stockwork	6	3.07	3.14	0.06	2.1%
	Undiff. Wall Rocks	123	2.75	2.78	0.03	1.2%

Figure 11-4: Scatter Plots for Density Reanalysis Results (Coloured by Lithology)



Source: SLR 2026.

11.3 Sample Security

The Project core shed is located in Puebla de Guzman, 22 km from La Romanera, 16 km from El Cura, and 8 km from La Infanta. There are all-weather gravel and paved roads from each deposit area to the core shed. The drill core is transported to the core shed by Emerita or drill contractor personnel by pickup truck. All core boxes are carefully placed on the truck and secured by straps and a net. The number of boxes carried complies with national transportation rules and laws.

The integrity of the core boxes is inspected prior to beginning the logging and sampling process. The boxes are unloaded from the pickup and then the established core handling procedure is followed (see Section 11.1.1). At the end of the logging and sampling process, the core boxes are organised in covered pallets. If they are mineralised, pallets are stored in metal racks at the

core shed, so they can be quickly accessed if necessary. Pallets of unmineralized material are stored in an outside core farm adjacent to the core shed.

The samples sent for analysis are delivered to the laboratories in Seville by authorised Emerita personnel in a company vehicle. Laboratory reject material is brought back to the core shed by Emerita personnel and stored in large boxes.

The QP considers the sample security and chain of custody procedures used by Emerita to be of a high standard.

11.4 Laboratories

The laboratories used for geochemical analysis by Emerita are listed in Table 11-4. Only ALS was used for La Romanera core samples, El Cura core samples, and all IBW Project soil samples. Both ALS and AGQ Mining and Bioenergy S.L. (AGQ) laboratories were used for La Infanta core samples. These laboratories are independent of Emerita.

Table 11-4: Analytical Laboratories

Laboratory	Certification
ALS Global	ISO 17025:2017. INAB Registration No: 173T
AGQ Mining and Bioenergy S.L.	UNE-EN-ISO/IEC 17025:2017 for mining laboratory analysis

11.5 Sample Preparation and Analysis

11.5.1 ALS

11.5.1.1 Core

The sample preparation procedure followed by ALS Sevilla is listed in Table 11-5.

Table 11-5: ALS Sevilla Sample Preparation Procedures

Laboratory	Sample Preparation	Description
ALS Global	WEI-21	Received sample weight
	LOG-22	Sample login – Rcd w/o barcode
	CRU-QC	Crushing quality control (QC) test
	PUL-QC	Pulverizing QC test
	CRU-31	Fine crushing – 70% < 2 mm
	SPL-22Y	Split sample – Boyd rotary splitter
	PUL-32	Pulverize 1,000 gr to 85% <75 µm
	LOG-24	Pulp Login – Rcd w/o barcode

After sample preparation, ALS Sevilla then sends the pulps to the ALS Loughrea Laboratory, located in Ireland. A suite of 19 elements, including Cu, Pb, Zn, and Ag (code ME-ICPORE), is analysed for using an oxidising aqua regia digestion followed by inductively coupled plasma atomic emission spectrometry (ICP-AES).

ALS' ME-ICPORE method is applicable to base metal ores and is particularly used for massive sulphides, where oxidising agents ensure that the sulphides are fully decomposed. The method delivers the elements and detection ranges summarised in Table 11-6.

Table 11-6: Elements and Ranges of Analysis for the ME-ICPORE Method from ALS Global

Analyte	Detection Range	Units	Analyte	Detection Range	Units
Ag	1-1,500	ppm	Mn	0.005-50	%
As	0.005-30	%	Mo	0.001-10	%
Bi	0.005-30	%	Ni	0.001-30	%
Ca	0.01-50	%	P	0.01-20	%
Cd	0.001-10	%	Pb	0.005-30	%
Co	0.001-20	%	S	0.05-50	%
Cu	0.001-40	%	Sb	0.005-100	%
Fe	0.01-100	%	Tl	0.005-1	%
Hg	8-10,000	ppm	Zn	0.002-100	%
Mg	0.01-50	%			

Pulps are then sent to ALS Johannesburg to be analysed for gold via fire assay with an atomic absorption spectroscopy (code Au-AA23) or gravimetric (code Au-GRA21) finish (Table 11-7).

Table 11-7: Gold Analysis Range for the Au-AA23 and Au-GRA21 Methods from ALS Global

Method Code	Analyte	Detection Range	Units
Au-AA23	Au	0.005-10	ppm
Au-GRA21	Au	0.05-10,000	ppm

11.5.1.2 Soil

For soil geochemistry, sample preparation follows the PREP-41 method, which consists of drying the sample at <60°C, then sieving to -180 µm with an 80 mesh and retaining both fractions. A suite of element was analysed for using method ME-MS61L, which consists of a four-acid super trace analysis with lower detection limits (Table 11-8).

Table 11-8: Elements and Range of Analysis for the ME-MS61L Method from ALS Global

Analyte	Detection Range	Units	Analyte	Detection Range	Units	Analyte	Detection Range	Units
Ag	0.002-100	ppm	Hf	0.004-500	ppm	Sb	0.02-10000	ppm
Al	0.01-50	%	In	0.005-500	ppm	Sc	0.01-10000	ppm
As	0.02-10,000	ppm	K	0.01-10	%	Se	0.006-1000	ppm
Ba	1-10,000	ppm	La	0.005-10,000	ppm	Sn	0.02-500	ppm
Be	0.02-1,000	ppm	Li	0.2-10,000	ppm	Sr	0.02-10,000	ppm
Bi	0.002-10,000	ppm	Mg	0.01-50	%	Ta	0.01-500	ppm
Ca	0.01-50	%	Mn	0.2-100,000	ppm	Te	0.005-500	ppm
Cd	0.005-10,00	ppm	Mo	0.02-10,000	ppm	Th	0.004-10,000	ppm
Ce	0.01-10,000	ppm	Na	0.001-10	%	Ti	0.001-10	%
Co	0.005-10,000	ppm	Nb	0.005-500	ppm	Tl	0.002-10,000	ppm
Cr	0.3-10,000	ppm	Ni	0.08-10000	ppm	U	0.01-10,000	ppm
Cs	0.01-10,000	ppm	P	0.001-1	%	V	0.1-10,000	ppm
Cu	0.02-10,000	ppm	Pb	0.01-10000	ppm	W	0.008-10,000	ppm
Fe	0.002-50%	%	Rb	0.02-10000	ppm	Y	0.01-500	ppm
Ga	0.05-10,000	ppm	Re	0.0004-50	ppm	Zn	0.2-10,000	ppm
Ge	0.05-500	ppm	S	0.01-10	%	Zr	0.1-500	ppm

11.5.2 AGQ

A small proportion of La Infanta drill core samples (7.5%) have been analysed by AGQ. The sample preparation methods applied are listed in Table 11-9.

Table 11-9: AGQ Sample Preparation Procedures

Laboratory	Description
AGQ Mining and Bioenergy S.L.	Oven drying at 105°C
	Fine crushing, 70% < 2 mm
	Split Sample – riffle splitter
	Pulverize 250 g to 85% <75 µm

Geochemical analysis is via methods PE-4042 or PE-4043. Both are multi-element analyses designed for metallic ores and use an oxidising aqua regia digestion followed by ICP-AES for a suite of 37 or 38 elements, respectively, including Cu, Pb, Zn, and Ag (Table 11-10 and Table 11-11).

Table 11-10: Elements and Range of Analysis for the PE-4042 Method from AGQ

Analyte	Detection Range	Units	Analyte	Detection Range	Units	Analyte	Detection Range	Units
Al	200-100,000	ppm	Fe	200-200,000	ppm	S	500-100,000	ppm
Ag	5.00-100	ppm	Ga	5.00-1000	ppm	Sb	10.0-10,000	ppm
As	10.0-10,000	ppm	Hg	10.0-1000	ppm	Sc	5.00-10,000	ppm
Au	0.05-10	ppm	In	5.00-500	ppm	Se	10.0-500	ppm
B	10.0-10,000	ppm	K	500-200,000	ppm	Sn	10.0-10,000	ppm
Ba	5.00-10,000	ppm	Li	5.00-1000	ppm	Sr	5.00-10,000	ppm
Be	5.00-500	ppm	Mg	500-200,000	ppm	Ti	100-5000	ppm
Bi	10.0-10,000	ppm	Mn	5.00-10,000	ppm	Tl	5.00-10,000	ppm
Ca	500-200,000	ppm	Mo	10.0-1000	ppm	V	10.0-10,000	ppm
Cd	5.00-1000	ppm	Na	500-200,000	ppm	W	5.00-10,000	ppm
Co	5.00-1000	ppm	Ni	5.00-1000	ppm	Zn	100-10,000	ppm
Cr	10.0-1000	ppm	P	200-10000	ppm			
Cu	5.00-10,000	ppm	Pb	5.00-10,000	ppm			

Table 11-11: Elements and Range of Analysis for the PE-4043 Method from AGQ

Analyte	Detection Range	Units	Analyte	Detection Range	Units	Analyte	Detection Range	Units
Al	500-150,000	ppm	Fe	500-200,000	ppm	Pb	10.00-10,000	ppm
Ag	2.00-100	ppm	Ga	5.00-1000	ppm	S	500-200,000	ppm
As	10.0-10,000	ppm	Hg	10.0-1000	ppm	Sb	10.0-10,000	ppm
Au	0.05-100	ppm	In	5.00-1000	ppm	Sc	5.00-10,000	ppm
B	10.0-10,000	ppm	K	500-200,000	ppm	Se	10.0-500	ppm
Ba	50.00-10,000	ppm	La	50.0-10,000	ppm	Sn	10.0-10,000	ppm
Be	5.00-500	ppm	Li	10.00-10,000	ppm	Sr	5.00-10,000	ppm
Bi	10.0-10,000	ppm	Mg	500-200,000	ppm	Ti	100-10,000	ppm
Ca	500-200,000	ppm	Mn	25.0-10,000	ppm	Tl	5.00-10,000	ppm
Cd	5.00-2500	ppm	Mo	5.00-10,000	ppm	V	5.0-10,000	ppm
Co	5.00-10,000	ppm	Na	500-200,000	ppm	W	50.0-10,000	ppm
Cr	5.00-10,000	ppm	Ni	5.00-10,000	ppm	Zn	50.0-10,000	ppm
Cu	5.00-10,000	ppm	P	500-50,000	ppm			

PE-4014 is used to analyse for gold via a fire assay method (Table 11-12).

Table 11-12: Gold Analysis for the PE-4014 Method from AGQ

Analyte	Detection Range	Units
Au	0.05-100	ppm

11.6 QA/QC Protocol

11.6.1 Introduction

The implementation of a quality assurance and quality control (QA/QC) programme involves establishing appropriate procedures and the routine insertion of control samples to monitor the sampling, sample preparation, and analytical processes. Routine analysis of QC data has the following objectives:

- Identify and promptly correct any errors.
- Assess the reliability of sample assay data and the confidence in the data used for Mineral Resource estimation.

The Emerita QA/QC protocol is designed to measure and monitor accuracy, precision, and contamination.

11.6.2 Accuracy

Accuracy refers to the proximity of a measurement to a 'true' value. It is controlled by certified reference materials (CRMs). A CRM is a composite sample pulp of known matrix (rock type) and element content (certified mean and standard deviation), submitted to verify laboratory accuracy. The CRMs used by Emerita are listed in Table 11-13.

Table 11-13: Certified Mean Value and Standard Deviation of Emerita CRMs

CRM	Cu (%)	Pb (%)	Zn (%)	Au (ppm)	Ag (ppm)	S (%)
OREAS 620	0.175 ± 0.005	0.774 ± 0.024	3.12 ± 0.086	0.685 ± 0.021	38.4 ± 1.31	2.47 ± 0.094
OREAS 622	0.484 ± 0.013	2.19 ± 0.06	10.01 ± 0.258	1.85 ± 0.066	101 ± 4	7.50 ± 0.636
OREAS 623	1.72 ± 0.066	0.252 ± 0.01	1.01 ± 0.038	0.827 ± 0.039	20.4 ± 1.15	8.75 ± 0.630
OREAS 630b	0.052 ± 0.002	0.408 ± 0.021	1.10 ± 0.033	0.358 ± 0.013	19.1 ± 0.72	5.19 ± 0.168
CDN-ME-2204	0.257 ± 0.012	1.11 ± 0.04	2.41 ± 0.1%	1.013 ± 0.092	78 ± 7	Not Certified

11.6.3 Precision

Precision refers to the ability to repeat measurements under similar conditions. It is evaluated by inserting duplicate samples. Duplicate types implemented by Emerita include the following:

- **Field duplicate:** Sample of the same interval/site collected using the same sampling method as the original sample. Field duplicates are used to measure the precision of the entire sampling process, from the field to laboratory sample preparation and analysis. It is noted that field duplicate results are influenced by the nugget effect, i.e., small-scale variability of the mineralisation, which may cause significant variation between the original and the duplicate results.

- **Pulp duplicate:** Duplicate taken from the pulverised sample to measure the precision of the laboratory pulverising and analytical process. Variation should be minimal as the pulp should be homogeneous.

11.6.4 Contamination

Contamination refers to the unintentional alteration of a sample of one material with the presence of another material. This is evaluated by the insertion of the following types of blank samples:

- **Coarse blank (BLANK):** Coarse sample with values below detection for the elements of interest in the analytical method applied. Coarse blanks are subjected to and monitor contamination for the entire process of preparation and analysis.
- **Fine blank (BLANK F):** Pulp sample with values below detection for the elements of interest in the analytical method applied. Evaluates contamination during sample analysis.

Blanks have been prepared in the core shed by the following methods:

- **Coarse blank (BLANK):** The source of these materials has changed over time, including barren aggregate quarry material until November 2022, then blank material from ALS Global until July 2023, and silica sand from July 2023 to present. The preparation procedure consists of measuring 1 kg, placing it in a sample bag and closing it with a plastic clip.
- **Fine blank (BLANK F):** Fine blanks were bought from ALS Global until July 2023 and have since been derived from finely crushed silica sand. The preparation procedure consists of measuring 100 g of material and placing it in a zip-lock bag.

11.6.5 Quality Control Rules

Quality control rules define when a control sample is considered to have failed and needs to be investigated and are summarised in Table 11-14.

Table 11-14: Emerita Quality Control Rules

Rule	QC Sample	QC Measure	Failure Criteria
1	BLANK	Contamination	The result of a blank is 5 times greater than the average blank sample value.
2	CRM	Accuracy	The result of a CRM is greater than 3 standard deviations to its certified mean value.
3	CRM	Accuracy	The results of 2 adjacent CRMs are greater than 2 standard deviations (same side) from their certified mean values.

Once the possibility of having out of sequence samples has been ruled out, the pulps of the failed sample and the adjacent samples to the next accepted QC sample are sent for reanalysis.

If the failure is due to accuracy (CRM), the sample pulps are sent for reanalysis. If the failure is due to contamination (blank), the coarse rejects from the samples are sent for reanalysis. A new analysis request is generated for the samples to be reanalysed and the original label numbers are retained. Samples are reanalysed until QC results are satisfactory.

If there is suspicion of a problem during initial sampling in the core yard, or if there is breakage and/or contamination of the coarse rejects or pulps, the remaining half of the core will be taken as a sample for analysis. This is the only case where new label numbers are assigned because it corresponds to a resampling of the core.

11.7 QA/QC Results

11.7.1 La Romanera (ALS)

11.7.1.1 Introduction

The La Romanera MRE database includes 8,247 samples assayed by ALS. A total of 6,798 samples were original drill core samples and the remaining 1,449 were QC samples (Table 11-15). Total QC sample insertion rate exceeds the industry standard of 15%. Duplicate samples were only introduced from January 2023 onwards, which accounts for their lower insertion rate relative to other QC sample types.

Table 11-15: Summary of La Romanera Samples Analysed by ALS

Sample Type	Number of Samples	% of Total
Original	6,798	82.4
Control	1,449	17.6
• Duplicates	255	3.1
• CRMs	421	5.1
• Blanks	773	9.5
Total	**8,247**	**100**

11.7.1.2 Certified Reference Materials

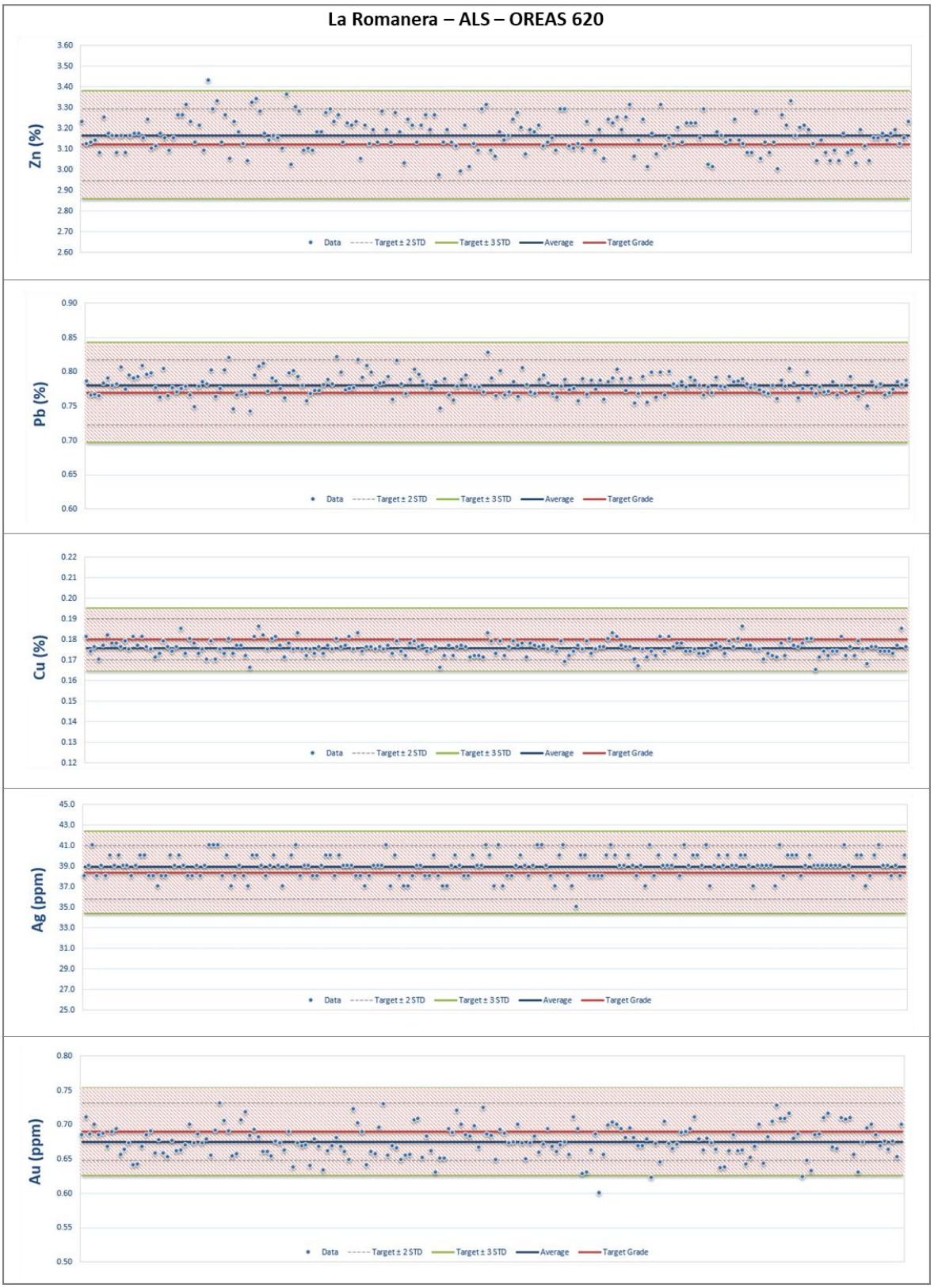
La Romanera CRM results for ALS are outlined in Table 11-16 and example CRM control charts are shown in Figure 11-5. Failure rates for each CRM (i.e., results outside ±3 standard deviations) were low for all elements analysed (Zn, Pb, Cu, Ag, Au, S), and no material bias is evident in the CRM control charts.

The CRMs used by Emerita for La Romanera drilling have lower sulphur grades (2.5% to 8.8%) than the typical sulphur grade range of La Romanera mineralisation (Indicated Resource average grade of 35.9%). Sulphur has not been included in the external CRM control charts presented in Figure 11-5 and internal laboratory QC results for CRMs with higher sulphur grades are instead presented in Figure 11-6. The internal laboratory control charts indicate acceptable accuracy, and the QP recommends routine insertion of CRMs with higher sulphur grades as part of Emerita's QA/QC protocol for La Romanera.

Table 11-16: Summary of La Romanera CRM Submissions to ALS

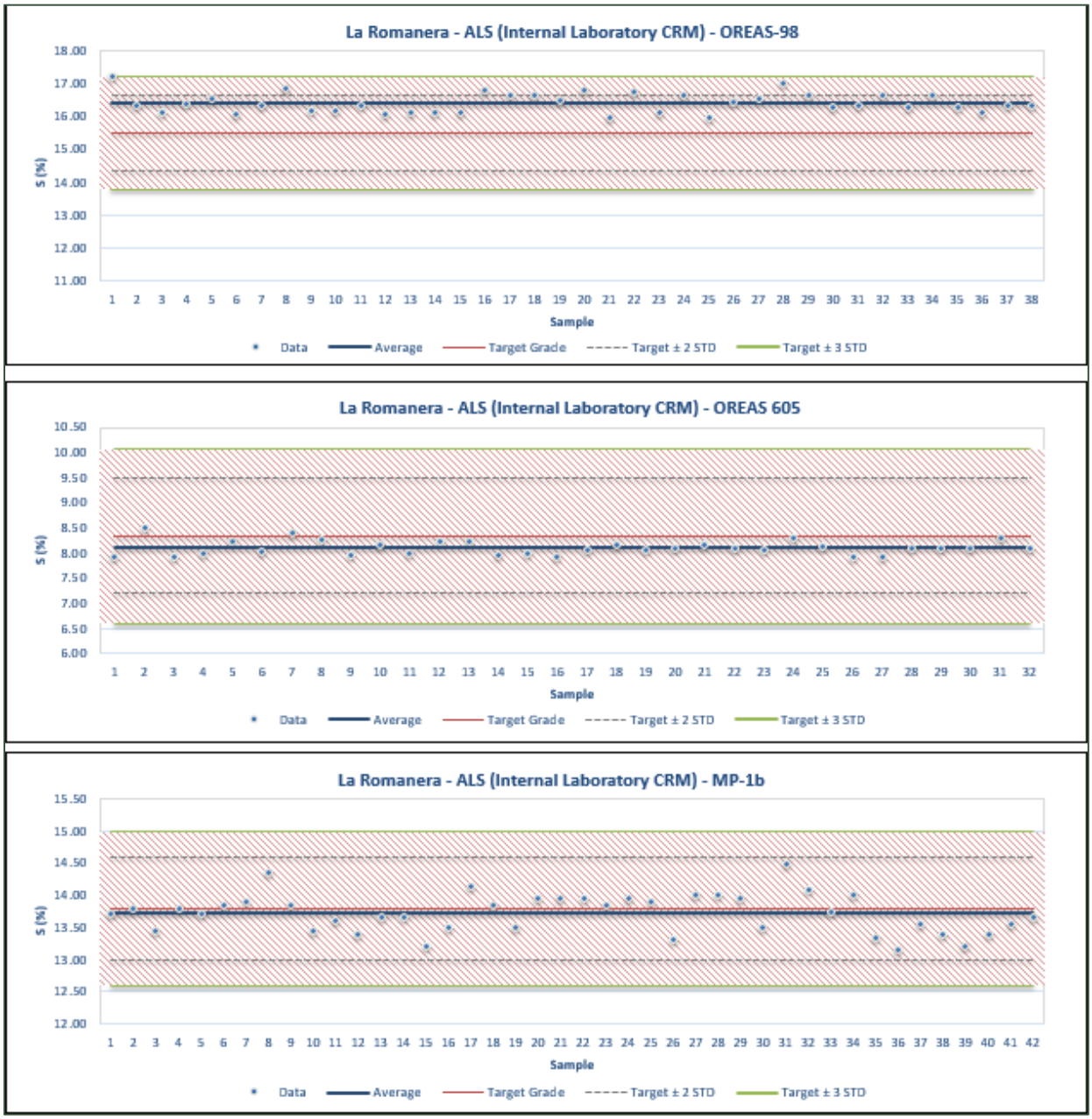
CRM	Number Samples	Samples Outside ± 2 Standard Deviations		Samples Outside ± 3 Standard Deviations		Certified Mean	Results Mean	Bias (%)
		Number Samples	% Samples	Number Samples	% Samples			
Zinc (%)								
OREAS 620	191	11	5.8	1	0.5	3.12	3.16	1.4
OREAS 622	15	0	0.0	0	0.0	10.01	10.02	0.1
OREAS 623	23	0	0.0	0	0.0	1.01	1.03	1.5
OREAS 630b	191	29	15.2	5	2.6	1.10	1.14	3.6
CDN ME-2204	1	0	0.0	0	0.0	2.41	2.41	0.0
Lead (%)								
OREAS 620	191	1	0.5	0	0.0	0.77	0.78	0.8
OREAS 622	15	0	0.0	0	0.0	2.19	2.18	-0.6
OREAS 623	23	0	0.0	0	0.0	0.25	0.25	-1.1
OREAS 630b	191	1	0.5	0	0.0	0.41	0.43	4.5
CDN ME-2204	1	0	0.0	0	0.0	1.11	1.11	0.0
Copper (%)								
OREAS 620	191	2	1.0	0	0.0	0.18	0.18	0.4
OREAS 622	15	1	6.7	1	6.7	0.48	0.50	2.6
OREAS 623	23	0	0.0	0	0.0	1.72	1.74	1.0
OREAS 630b	191	4	2.1	1	0.5	0.05	0.05	1.8
CDN ME-2204	1	0	0.0	0	0.0	0.26	0.26	0.8
Silver (ppm)								
OREAS 620	191	1	0.5	0	0.0	38.4	38.9	1.4
OREAS 622	15	0	0.0	0	0.0	101.0	103.3	2.3
OREAS 623	23	0	0.0	0	0.0	20.4	20.8	2.1
OREAS 630b	191	33	17.3	11	5.8	19.1	19.5	2.1
CDN ME-2204	1	0	0.0	0	0.0	78.0	83.0	6.4
Gold (ppm)								
OREAS 620	191	19	9.9	1	0.5	0.69	0.67	-1.5
OREAS 622	15	0	0.0	0	0.0	1.85	1.84	-0.6
OREAS 623	23	1	4.3	1	4.3	0.83	0.78	-5.2
OREAS 630b	191	11	5.8	5	2.6	0.36	0.35	-2.2
CDN ME-2204	1	0	0.0	0	0.0	1.01	1.03	1.2
Sulphur (%)								
OREAS 620	191	23	12.0	2	1.0	2.5	2.6	5.0
OREAS 622	15	0	0.0	0	0.0	7.5	8.1	8.3
OREAS 623	23	0	0.0	0	0.0	8.8	9.3	6.4
OREAS 630b	191	64	33.5	9	4.7	5.2	5.5	5.9

Figure 11-5: Example CRM Control Charts for OREAS 620 (La Romanera - ALS)



Source: SLR 2026.

Figure 11-6: Example Internal Laboratory CRM Control Charts for Sulphur (La Romanera - ALS)



Source: SLR 2026.

11.7.1.3 Duplicates

La Romanera duplicate results are outlined in Table 11-17 and Table 11-18, whilst example scatter plots for each duplicate type are shown in Figure 11-7. Plots show strong correlation between sample pairs and results are considered to demonstrate acceptable precision for sampling, sample preparation, and analysis.

Table 11-17: Summary Statistics for La Romanera Field Duplicate Submissions to ALS

Element	Number of Pairs	Mean Primary	Mean Duplicates	CV Primary	CV Duplicates	Correlation Coefficient	% of Pairs <20% HARD
Zn (%)	140	2.15	2.21	1.60	1.60	0.99	92.1
Pb (%)	140	1.02	1.03	1.55	1.49	0.98	85.7
Cu (%)	140	0.40	0.42	1.36	1.44	0.94	88.6
Ag (ppm)	140	46.63	46.25	1.21	1.18	0.99	86.4
Au (ppm)	140	1.05	1.04	1.50	1.52	0.99	87.9
S (%)	140	31.93	31.74	0.57	0.58	0.99	94.3

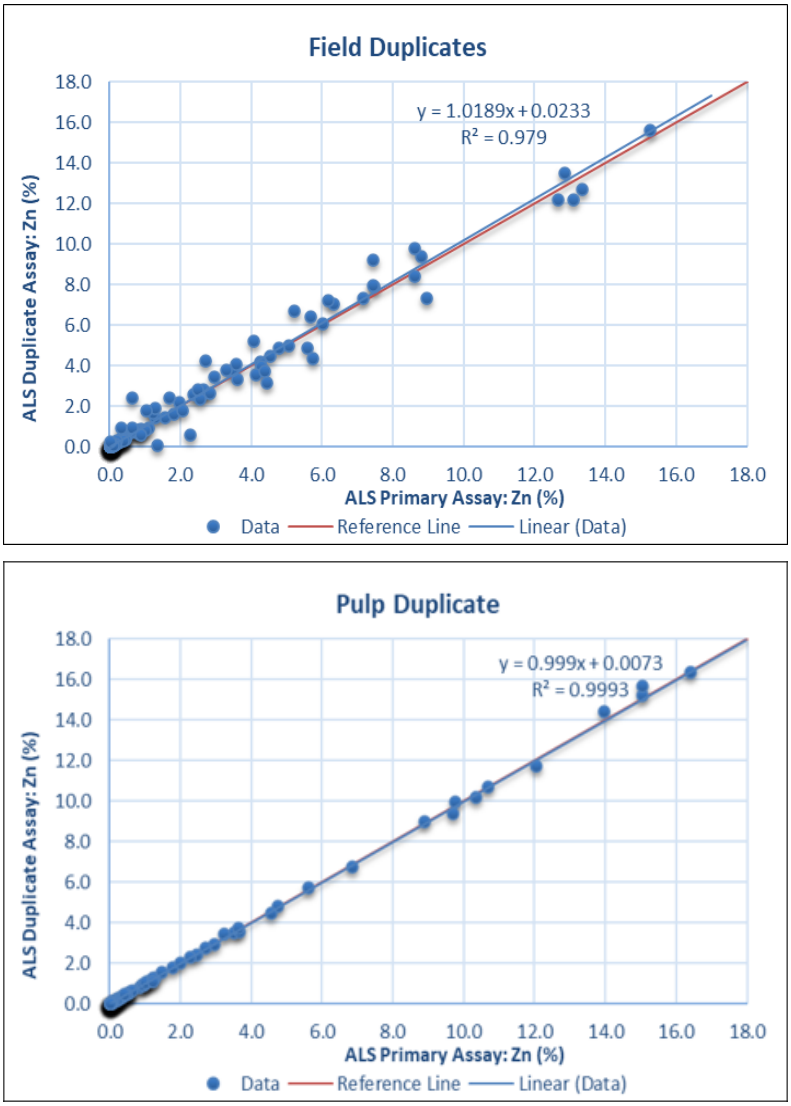
Note:
1. CV = coefficient of variation; HARD = half absolute relative difference

Table 11-18: Summary Statistics for La Romanera Pulp Duplicate Submissions to ALS

Element	Number of Pairs	Mean Primary	Mean Duplicates	CV Primary	CV Duplicates	Correlation Coefficient	% of Pairs <10% HARD
Zn (%)	115	1.93	1.93	2.13	2.13	1.00	96.5
Pb (%)	115	0.86	0.86	1.86	1.86	1.00	97.4
Cu (%)	115	0.27	0.27	2.31	2.34	1.00	93.9
Ag (ppm)	115	39.13	39.53	1.79	1.79	1.00	82.6
Au (ppm)	115	0.98	0.97	2.03	1.99	1.00	96.5
S (%)	115	25.15	25.15	0.76	0.76	1.00	100.0

Note:
1. CV = coefficient of variation; HARD = half absolute relative difference

Figure 11-7: Example Duplicate Scatter Plots for Zinc (La Romanera - ALS)



Source: SLR 2026.

11.7.1.4 Blanks

Results for La Romanera blanks analysed at ALS are listed in Table 11-19. Whilst some failures occurred, their frequency and severity do not indicate any material contamination issues.

Table 11-19: Summary of La Romanera Blank Submissions to ALS

Blank Type	Element	Unit	Number of Samples	Failure Limit	Number of Failures	Failure %
BLANK	Zn	%	261	0.023	2	0.8
	Pb	%	261	0.015	2	0.8
	Cu	%	261	0.006	2	0.8
	Ag	ppm	261	3.228	0	0.0
	Au	ppm	261	0.019	2	0.8
	S	%	261	0.196	1	0.4
BLANK F	Zn	%	512	0.019	0	0.0
	Pb	%	512	0.013	1	0.2
	Cu	%	512	0.006	10	2.0
	Ag	ppm	512	3.066	0	0.0
	Au	ppm	512	0.041	17	3.3
	S	%	512	0.145	1	0.2

11.7.2 La Infanta (ALS)

11.7.2.1 Introduction

The La Infanta MRE database includes 2,496 samples assayed by ALS. A total of 2,100 samples were original drill core samples and the remaining 409 were QC samples (Table 11-20). Total QC sample insertion rate exceeds the industry standard of 15%. Duplicate samples were only introduced from January 2023 onwards, which accounts for their lower insertion rate relative to other QC sample types.

Table 11-20: Summary of La Infanta Samples Analysed by ALS

Sample Type	Number of Samples	% Total
Original	2,100	84.1
Control	409	16.4
• Duplicates	49	1.9
• CRMs	141	5.6
• Blanks	219	8.8
Total	**2,496**	**100**

11.7.2.2 Certified Reference Materials

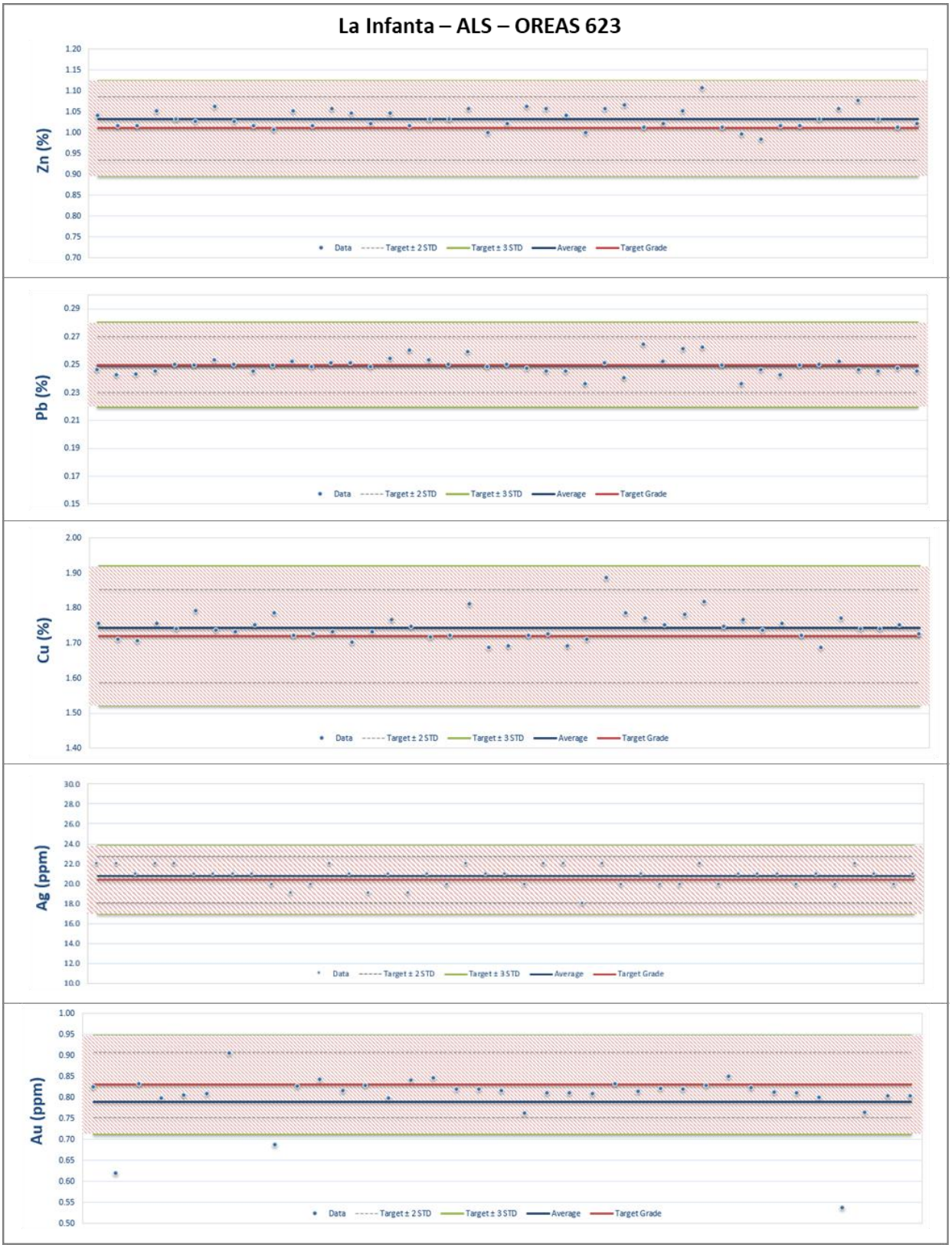
La Infanta CRM results for ALS are outlined in Table 11-21 and example CRM control charts are shown in Figure 11-8. Failure rates for each CRM (i.e., results outside ±3 standard deviations) were low for all elements analysed (Zn, Pb, Cu, Ag, Au, S), and no material bias is evident in the CRM control charts.

Sulphur grades at La Infanta are significantly lower than La Romanera and El Cura (Indicated Resource average grade of 6.7%). No pyrite concentrate production is envisaged and further analysis of internal laboratory sulphur CRM results has not been completed for La Infanta.

Table 11-21: Summary of La Infanta CRM Submissions to ALS

CRM	Number Samples	Samples Outside ± 2 Standard Deviations		Samples Outside ± 3 Standard Deviations		Certified Mean	Results Mean	Bias (%)
		Number Samples	% Samples	Number Samples	% Samples			
Zinc (%)								
OREAS 620	54	2	3.7	2	3.7	3.12	3.18	2.0
OREAS 622	33	2	6.1	2	6.1	10.01	9.97	-0.4
OREAS 623	43	1	2.3	0	0.0	1.01	1.03	2.1
OREAS 630b	10	1	10.0	0	0.0	1.10	1.12	2.2
CDN ME-2204	1	0	0.0	0	0.0	2.41	2.41	0.0
Lead (%)								
OREAS 620	54	0	0.0	0	0.0	0.77	0.78	0.6
OREAS 622	33	2	6.1	0	0.0	2.19	2.20	0.2
OREAS 623	43	0	0.0	0	0.0	0.25	0.25	-1.2
OREAS 630b	10	0	0.0	0	0.0	0.41	0.43	4.4
CDN ME-2204	1	0	0.0	0	0.0	1.11	1.08	-2.7
Copper (%)								
OREAS 620	54	0	0.0	0	0.0	0.18	0.18	0.7
OREAS 622	33	6	18.2	3	9.1	0.48	0.50	3.0
OREAS 623	43	1	2.3	0	0.0	1.72	1.74	1.3
OREAS 630b	10	1	10.0	1	10.0	0.05	0.05	2.7
CDN ME-2204	1	0	0.0	0	0.0	0.26	0.26	-0.4
Silver (ppm)								
OREAS 620	54	1	1.9	0	0.0	38.4	39.0	1.5
OREAS 622	33	1	3.0	0	0.0	101.0	103.5	2.5
OREAS 623	43	1	2.3	0	0.0	20.4	20.8	1.9
OREAS 630b	10	4	40.0	2	20.0	19.1	20.2	5.8
CDN ME-2204	1	0	0.0	0	0.0	78.0	75.0	-3.8
Gold (ppm)								
OREAS 620	54	3	5.6	2	3.7	0.69	0.67	-1.5
OREAS 622	33	2	6.1	0	0.0	1.85	1.82	-1.5
OREAS 623	43	4	9.3	4	9.3	0.83	0.79	-4.4
OREAS 630b	10	1	10.0	1	10.0	0.36	0.36	1.4
CDN ME-2204	1	0	0.0	0	0.0	1.01	1.09	7.1
Sulphur (%)								
OREAS 620	54	4	7.4	1	1.9	2.5	2.6	4.1
OREAS 622	33	1	3.0	0	0.0	7.5	8.1	8.0
OREAS 623	43	0	0.0	0	0.0	8.8	9.3	6.7
OREAS 630b	10	2	20.0	0	0.0	5.2	5.4	4.9

Figure 11-8: Example CRM Control Charts for OREAS 623 (La Infanta - ALS)



Source: SLR 2026.

11.7.2.3 Duplicates

La Infanta duplicate results for ALS are outlined in Table 11-22 and Table 11-23, whilst example scatter plots for each duplicate type are shown in Figure 11-9. Plots show strong correlation between sample pairs and results are considered to demonstrate acceptable precision for sampling, sample preparation, and analysis. The lower percentage of pulp duplicate pairs (52.6%) at less than 10% half absolute relative difference (HARD) for silver reflects reduced relative precision at very low sample grades close to the analytical detection limit.

Table 11-22: Summary Statistics for La Infanta Field Duplicate Submissions to ALS

Element	Number of Pairs	Mean Primary	Mean Duplicates	CV Primary	CV Duplicates	Correlation Coefficient	% of Pairs <20% HARD
Zn (%)	30	4.74	4.37	1.83	1.86	0.99	70.0
Pb (%)	30	2.60	2.28	1.97	1.94	1.00	76.7
Cu (%)	30	0.45	0.41	2.19	2.21	0.98	63.3
Ag (ppm)	30	56.77	48.63	2.65	2.37	0.99	60.0
Au (ppm)	30	0.19	0.18	1.88	1.81	1.00	96.7
S (%)	30	5.82	5.58	1.05	1.06	0.99	96.7

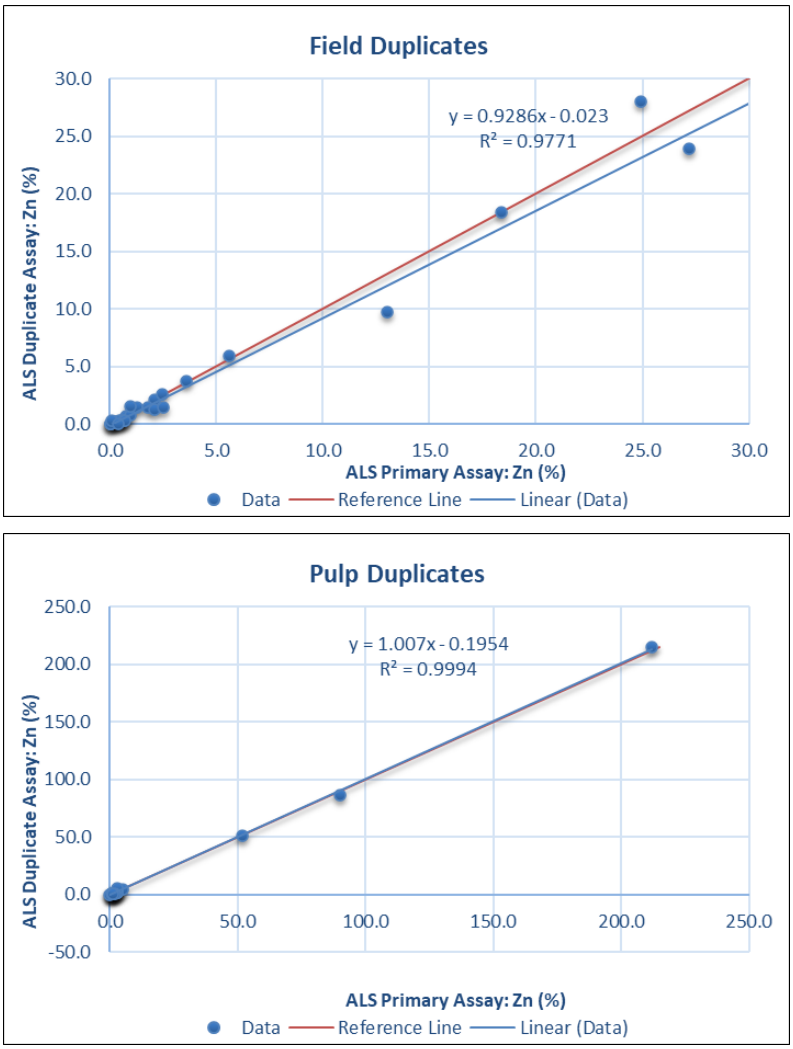
Note:
1. CV = coefficient of variation;

Table 11-23: Summary Statistics for La Infanta Pulp Duplicate Submissions to ALS

Element	Number of Pairs	Mean Primary	Mean Duplicates	CV Primary	CV Duplicates	Correlation Coefficient	% of Pairs <10% HARD
Zn (%)	19	2.31	2.30	2.88	2.89	1.00	88.2
Pb (%)	19	1.12	1.11	2.66	2.65	1.00	94.7
Cu (%)	19	0.18	0.17	2.65	2.64	1.00	89.5
Ag (ppm)	19	20.24	20.26	2.55	2.57	1.00	52.6
Au (ppm)	19	0.11	0.11	1.72	1.69	1.00	94.7
S (%)	19	4.10	4.09	1.26	1.26	1.00	100.0

Note:
1. CV = coefficient of variation

Figure 11-9: Example Duplicate Scatter Plots for Zinc (La Infanta - ALS)



Source: SLR 2026.

11.7.2.4 Blanks

Results for La Infanta blank samples analysed at ALS are presented in Table 11-24. Whilst some failures occurred, their frequency and severity do not indicate any material issues with sample contamination.

Table 11-24: Summary of La Infanta Blank Submissions to ALS

Blank Type	Element	Unit	Number of Samples	Failure Limit	Number of Failures	Failure %
BLANK	Zn	%	134	0.022	1	0.7
	Pb	%	134	0.016	1	0.7
	Cu	%	134	0.005	0	0.0
	Ag	ppm	134	3.284	0	0.0
	Au	ppm	134	0.018	0	0.0
	S	%	134	0.143	1	0.7
BLANK F	Zn	%	85	0.021	0	0.0
	Pb	%	85	0.016	0	0.0
	Cu	%	85	0.006	0	0.0
	Ag	ppm	85	3.147	0	0.0
	Au	ppm	85	0.034	3	3.5
	S	%	85	0.125	0	0.0

11.7.3 La Infanta (AGQ)

The La Infanta MRE database includes 201 samples assayed by AGQ. A total of 164 samples were original drill core samples and the remaining 37 were QC samples, comprising 10 CRMs and 27 blanks. AGQ samples represent 7.5% of the La Infanta database. QC results are in line with those for ALS.

11.7.4 El Cura (ALS)

11.7.4.1 Introduction

The El Cura MRE database includes 2,135 samples assayed by ALS. A total of 1,782 samples were original drill core samples and the remaining 353 were QC samples (Table 11-25). Total QC sample insertion rate exceeds the industry standard of 15%.

Table 11-25: Summary of El Cura Samples Analysed by ALS

Sample Type	Number of Samples	% Total
Original	1,782	83.5
Control	353	16.5
• Duplicates	122	5.7
• CRMs	126	5.9
• Blanks	105	4.9
Total	**2,135**	**100**

11.7.4.2 Certified Reference Materials

El Cura CRM results for ALS are outlined in Table 11-26. Example CRM control charts are shown in Figure 11-10. Failure rates for each CRM (i.e., results outside ±3 standard deviations), were typically low for all elements analysed (Zn, Pb, Cu, Ag, Au, S), and no material bias is evident in the CRM control charts.

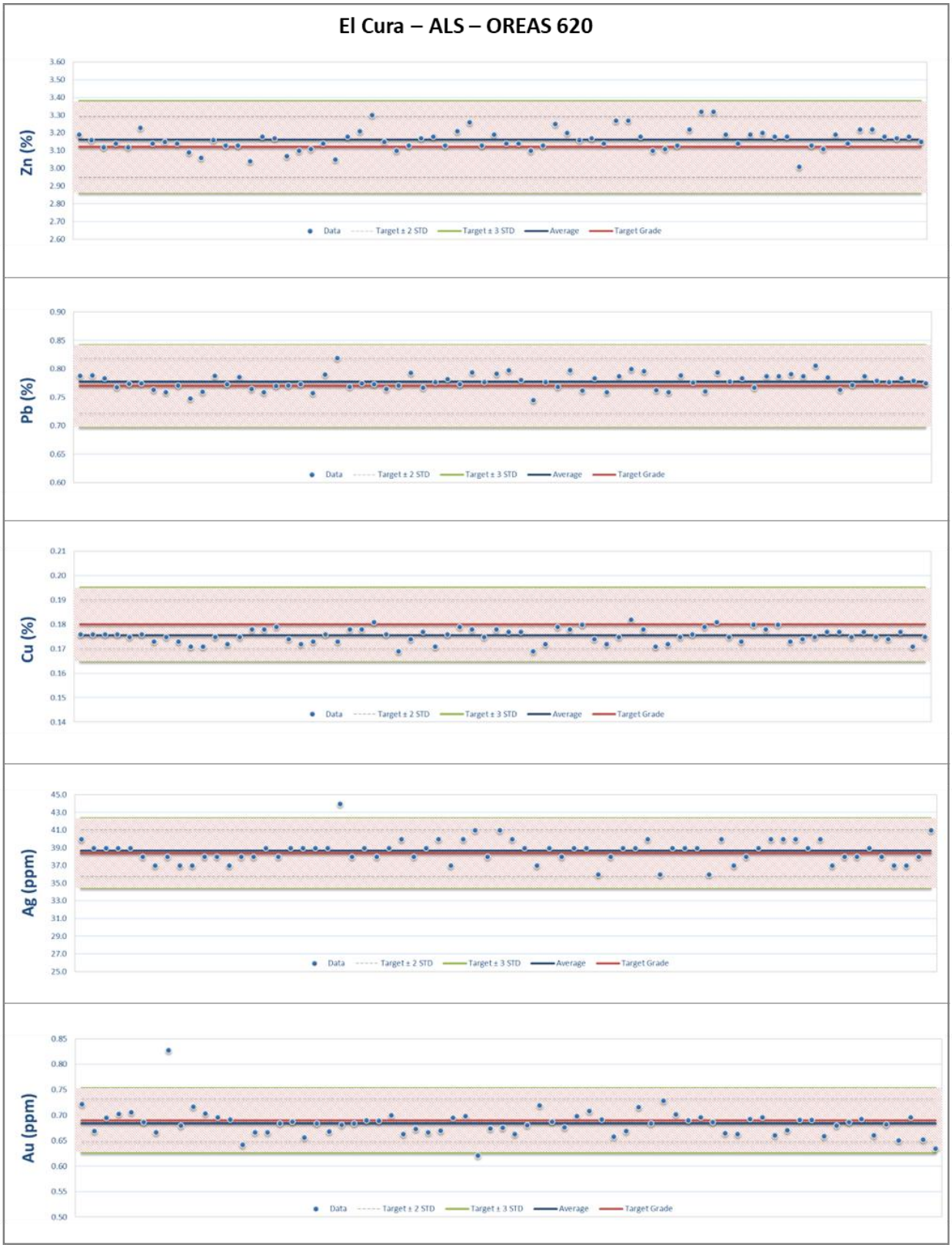
Higher grade copper CRMs (e.g. OREAS 623) were out of circulation during the El Cura drilling programmes. The QP recommends that additional CRMs with higher copper grades (0.5-2% Cu) are sourced and inserted into the El Cura sample sequence.

The CRMs used by Emerita for El Cura drilling have lower sulphur grades (2.5% to 5%) than the typical sulphur grade range of El Cura mineralisation (Indicated Resource average grade of 25.8%). Sulphur has not been included in the external CRM control charts presented in Figure 11-10 and internal laboratory QC results for CRMs with higher sulphur grades are instead presented in Figure 11-11. The internal laboratory control charts indicate acceptable accuracy, and the QP recommends routine insertion of CRMs with higher sulphur grades as part of Emerita's QA/QC protocol for El Cura.

Table 11-26: Summary of El Cura CRM Submissions to ALS

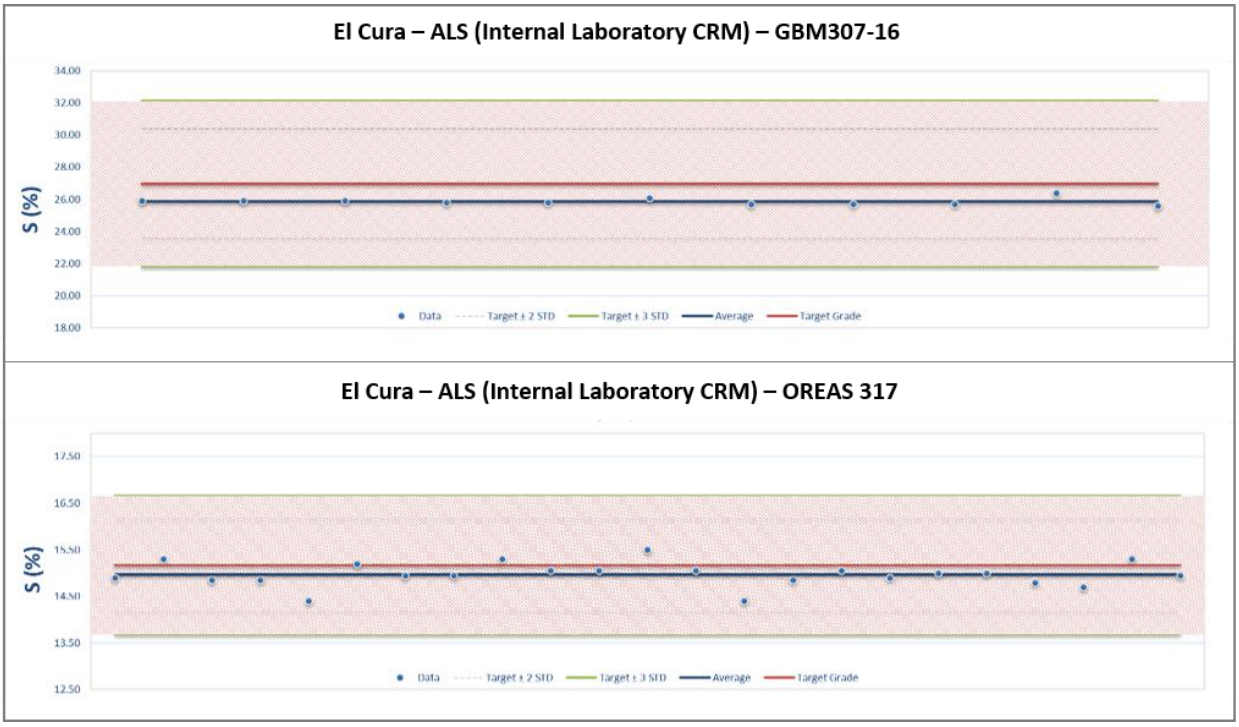
CRM	Number Samples	Samples Outside ± 2 Standard Deviations		Samples Outside ± 3 Standard Deviations		Certified Mean	Results Mean	Bias (%)
		Number Samples	% Samples	Number Samples	% Samples			
Zinc (%)								
OREAS 620	70	3	4.3	0	0.0	3.12	3.16	1.3
OREAS 630b	12	0	0.0	0	0.0	1.10	1.12	1.5
CDN ME-2204	44	0	0.0	0	0.0	2.41	2.41	0.1
Lead (%)								
OREAS 620	70	0	0.0	0	0.0	0.77	0.78	0.5
OREAS 630b	12	0	0.0	0	0.0	0.41	0.42	3.1
CDN ME-2204	44	0	0.0	0	0.0	1.11	1.11	0.1
Copper (%)								
OREAS 620	70	0	0.0	0	0.0	0.18	0.18	0.3
OREAS 630b	12	0	0.0	0	0.0	0.05	0.05	1.3
CDN ME-2204	44	0	0.0	0	0.0	0.26	0.26	1.2
Silver (ppm)								
OREAS 620	70	1	1.4	1	1.4	38.4	38.6	0.6
OREAS 630b	12	4	33.3	0	0.0	19.1	19.3	0.8
CDN ME-2204	44	0	0.0	0	0.0	78.0	79.1	1.4
Gold (ppm)								
OREAS 620	70	5	7.1	2	2.9	0.69	0.68	-0.1
OREAS 630b	12	1	8.3	0	0.0	0.36	0.35	-1.0
CDN ME-2204	44	1	2.3	0	0.0	1.01	1.05	3.2
Sulphur (%)								
OREAS 620	70	4	5.7	0	0.0	2.5	2.6	4.4
OREAS 630b	12	3	25.0	0	0.0	5.2	5.4	4.4

Figure 11-10: Example CRM Control Charts for OREAS 620 (El Cura - ALS)



Source: SLR 2026.

Figure 11-11: Example Internal Laboratory CRM Control Charts for Sulphur (El Cura - ALS)



Source: SLR 2026.

11.7.4.3 Duplicates

El Cura duplicate results for ALS are outlined in Table 11-27 and Table 11-28 and example scatter plots for each duplicate type are shown in Figure 11-12. Plots show strong correlation between sample pairs and results are considered to demonstrate acceptable precision for sampling, sample preparation, and analysis. The lower percentage of pulp duplicate pairs <10% HARD for Zn, Ag, and Au, reflects reduced relative precision at very low sample grades close to the analytical detection limit.

Table 11-27: Summary Statistics for El Cura Field Duplicate Submissions to ALS

Element	Number of Pairs	Mean Primary	Mean Duplicates	CV Primary	CV Duplicates	Correlation Coefficient	% of Pairs <20% HARD
Zn (%)	45	3.05	3.25	1.09	1.13	0.97	91.1
Pb (%)	45	1.35	1.45	0.96	1.02	0.97	95.6
Cu (%)	45	2.20	2.22	1.01	0.98	0.99	97.8
Ag (ppm)	45	69.34	70.80	0.65	0.72	0.96	93.3
Au (ppm)	45	2.47	2.27	0.98	0.87	0.83	95.6
S (%)	45	40.76	40.92	0.18	0.18	0.98	100.0

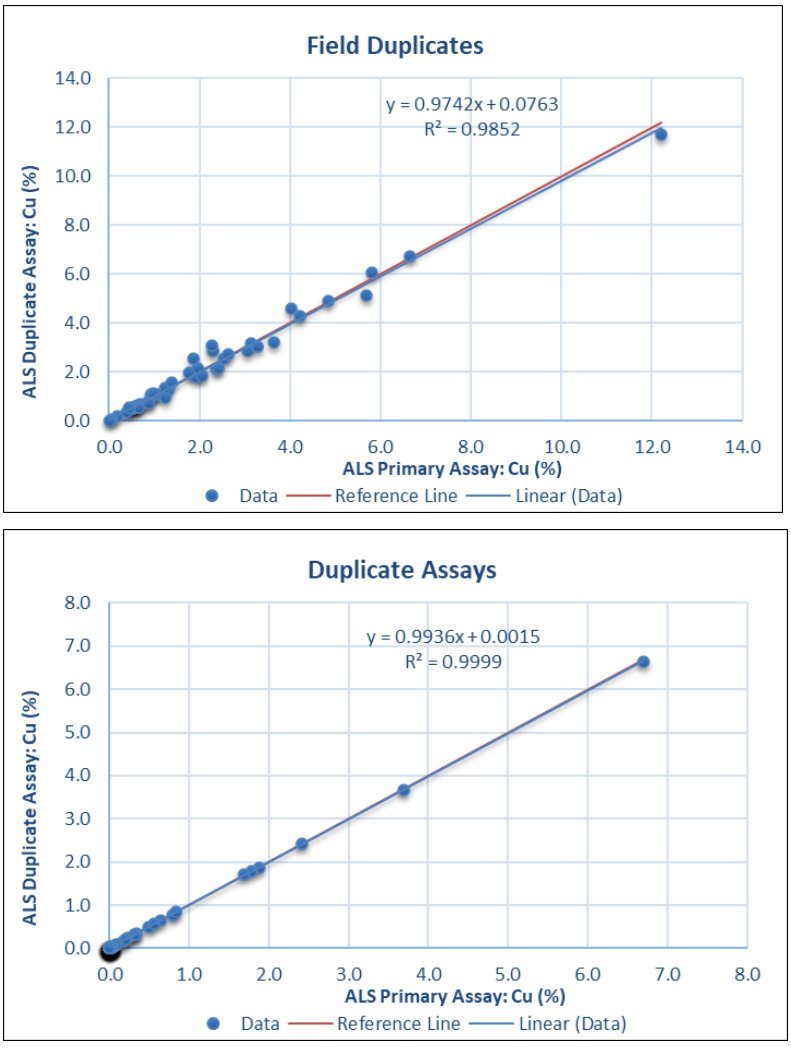
Note:
1. CV = coefficient of variation; HARD = half absolute relative difference

Table 11-28: Summary Statistics for El Cura Pulp Duplicate Submissions to ALS

Element	Number of Pairs	Mean Primary	Mean Duplicates	CV Primary	CV Duplicates	Correlation Coefficient	% of Pairs <10% HARD
Zn (%)	77	0.22	0.22	3.45	3.45	1.00	74.0
Pb (%)	77	0.11	0.11	2.38	2.39	1.00	92.2
Cu (%)	77	0.31	0.31	3.11	3.10	1.00	90.9
Ag (ppm)	77	6.55	6.63	2.48	2.49	1.00	61.0
Au (ppm)	77	0.23	0.24	2.40	2.42	1.00	79.2
S (%)	77	8.32	8.33	1.57	1.57	1.00	98.7

Note:
1. CV = coefficient of variation; HARD = half absolute relative difference

Figure 11-12: Example Duplicate Scatter Plots for Copper (El Cura - ALS)



Source: SLR 2026.

11.7.4.4 Blanks

Results for El Cura blank samples analysed at ALS are presented in Table 11-29. Whilst some failures occurred, their frequency and severity do not indicate any material issues with sample contamination.

Table 11-29: Summary of El Cura Blank Submissions to ALS

Blank Type	Element	Unit	Number of Samples	Failure Limit	Number of Failures	Failure %
BLANK	Zn	%	36	0.015	1	2.8
	Pb	%	36	0.013	1	2.8
	Cu	%	36	0.008	1	2.8
	Ag	ppm	36	3.264	1	2.8
	Au	ppm	36	0.015	1	2.8
	S	%	36	0.125	0	0.0
BLANK F	Zn	%	69	0.017	3	4.3
	Pb	%	69	0.015	3	4.3
	Cu	%	69	0.010	3	4.3
	Ag	ppm	69	4.094	0	0.0
	Au	ppm	69	0.022	3	4.3
	S	%	69	0.125	3	4.3

11.7.5 Summary and Recommendations

In the La Romanera, La Infanta, and El Cura MRE databases, the total QC sample insertion rates exceed the industry standard of 15% of samples analysed. Since introducing duplicate samples in January 2023, the proportion of different QC sample types has been optimised such that CRM, blank, and duplicate samples have individual insertion rates approximately 5%.

Whilst the CRMs used by Emerita have typically been appropriate for the grade distributions and mineralisation types for each deposit, the QP recommends that a high-grade copper CRM (e.g. OREAS 623) be implemented in the QA/QC protocol for El Cura, and a high-grade sulphur polymetallic CRM (e.g., OREAS 317) be inserted for El Cura and La Romanera. The QP also recommends that duplicate sample type is expanded to include a coarse duplicate submitted to the primary laboratory and a pulp duplicate submitted to an umpire laboratory. CRM, blank, and duplicate results demonstrate acceptable levels of accuracy, contamination, and precision in sampling, sample preparation, and analysis.

11.8 Adequacy of Procedures

The QP considers that the sampling, sample preparation, security, and analytical procedures for samples sent to both the ALS and AGQ laboratories have been conducted in accordance with acceptable industry standards, and the assay results generated following these procedures are suitable for use in Mineral Resource estimation.

12.0 Data Verification

12.1 Data Verification by Emerita

Data entry, validation, storage, and database management are carried out by Emerita geologists using established procedures. Only diamond core drilling completed by Emerita was included in the MRE. All data are stored in a cloud-based relational database using MX Deposit software. MX Deposit includes an in-built audit trail, data entry and import validation tools, and QA/QC plot generation. Emerita staff monitor the quality of the assay data in the databases using established QA/QC procedures. Drillhole data is imported directly from the cloud into Leapfrog modelling and estimation software.

12.2 Database Cut-Off Dates

Drilling is ongoing at the IBW Project. The cut-off date used to close the databases prior to Mineral Resource estimation is January 16, 2026.

12.3 Data Verification by the QP

12.3.1 Site Visit

Formal site visits have been undertaken by Frank Browning (March 16, 2023, May 3-5, 2023, February 10-12, 2025, and January 21, 2026), Alan Clarke (January 21, 2026), and Christopher Penna (January 21, 2026), and included the following inspections:

- Extent of exploration work completed to date.
- Review of drill core logging, sampling, sample preparation, analysis, and QA/QC procedures.
- Inspection of the core logging, sampling, and storage facilities.
- Inspection of drilling sites and operations.
- Inspection of selected drill core from La Romanera, La Infanta, and El Cura to confirm the nature of the mineralisation and the geological descriptions.
- Inspection of geology and mineralisation at the La Romanera, La Infanta, and El Cura surface outcrops and historical workings.
- Inspection of potential surface infrastructure sites.

12.3.2 Database Review

A review of the La Romanera, La Infanta, and El Cura drillhole databases was carried out by the QP and included the following checks:

- Comparison of a random selection of collar, survey, and assay database values with original data certificates.
- Verification that collar coordinates coincide with topographic surfaces and have been reported to the expected accuracy.
- Verification that downhole survey azimuth and inclination values display consistency and are within expected tolerances.

- Evaluation of minimum and maximum grade values to ensure they fall within laboratory detection limits.
- Evaluation of minimum and maximum sample lengths to ensure they fall within Emerita's stipulated sampling protocol.
- Assessing for inconsistencies in spelling or coding (typographic and case-sensitive errors).
- Ensuring full data entry and that a specific data type (collar, survey, lithology, and assay) is not missing and assessing for sample gaps or overlaps.
- Review of QA/QC procedures and results (as detailed in Section 11.0).

Overall, no significant issues in terms of data collection, data entry, or data storage were identified by the QP in the review of the electronic databases.

12.3.3 Limitations

The QP has not undertaken any independent check analysis of samples nor conducted any twin hole drilling to confirm the assays contained in the electronic databases. The QP does not consider referee samples necessary given the following findings:

- The procedures used by Emerita for sampling, logging, sample preparation, analysis, sample security, and data storage are considered to be robust.
- Routine monitoring of QA/QC data demonstrates an acceptable level of accuracy and precision.
- Laboratories employed are accredited and reputable.

12.3.4 Adequacy of Data

The verification procedures conducted by the QP confirmed the integrity of the data in the electronic databases. The QP is of the opinion that the verification procedures for the IBW Project comply with industry standards and that the databases are suitable for the purposes of Mineral Resource estimation, and for the purposes of this Technical Report.

13.0 Mineral Processing and Metallurgical Testing

13.1 Introduction

The process flowsheet and associated testwork programs have evolved significantly over the course of the Project, with successive metallurgical programs progressively advancing the flowsheet towards a more robust, simplified and unified processing approach for the three deposits.

Wardell Armstrong International (WAI) completed successive metallurgical testwork programs for the Project, beginning with Phase I testwork on La Romanera and La Infanta samples. Phase I established the initial flotation response of both deposits, producing bulk Cu-Pb and separate Zn concentrates for La Romanera and demonstrating the production of separate Cu, Pb and Zn concentrates for La Infanta. Building on these results and in line with Emerita's objectives, Phase II advanced the flowsheet towards a simplified and unified selective-flotation scheme. The Phase II program demonstrated that La Romanera, La Infanta and El Cura can be treated using a common flowsheet to produce separate Cu, Pb and Zn concentrates with acceptable recoveries of payable metals. Most recently, WAI completed additional testwork on samples from the El Cura deposit included in the MRE, together with testwork on the production of pyrite concentrate from the base-metal flotation tailings generated from all three deposits.

In parallel with WAI's testwork programs, alternative routes have been evaluated to maximize value recovery from the flotation tailings. For the purposes of this PFS, the base case assumes production of a pyrite concentrate from the base-metal flotation tailings for direct sale as a sulphur-bearing feedstock for acid production. Further PFP testwork is ongoing to assess the potential recovery of additional value from these tailings, providing a possible future alternative to direct sale of the pyrite concentrate.

The testwork programs have successfully established a unified selective-flotation flowsheet for the Project, under which material from all three deposits can be treated through a common circuit to produce separate Cu, Pb and Zn concentrates, followed by a fourth flotation stage to produce a potentially marketable pyrite concentrate.

13.2 Phase I Testwork

A report for the Phase I testwork was issued by WAI in June 2024 (ZT64-0940 La Romanera and La Infanta Project, Metallurgical Testwork Study). Phase 1 testing was completed in late 2023 on four composite samples, three from La Romanera (MET-1 to MET-3) and one from La Infanta (MET-4).

SLR notes that only the comminution test results for Phase I testwork were used in the PFS process design.

13.2.1 Sample Selection

Samples for Phase I comminution and flotation testwork comprised quarter-split HQ drill core and included the following characteristics:

- **MET-1**: La Romanera high gold / high arsenic 'polymetallic mineralisation' – Lower Lens.
- **MET-2**: La Romanera low zinc / high copper 'cupriferous mineralisation' – Upper and Lower Lenses.

- **MET-3**: La Romanera average zinc / copper 'polymetallic mineralisation' – Upper and Lower Lenses.
- **MET-4**: La Infanta semi-massive sulphide – North, South, and South 1 Lenses.

For La Romanera, core intervals were selected to provide reasonable spatial coverage and statistical representation of grade distributions for three mineralisation types. Polymetallic mineralisation **(MET-3)** is the dominant mineralisation type at La Romanera, contributing approximately 84% of Mineral Resource tonnage, of which approximately 13% **(MET-1)** has distinctly high Au-As content, whilst the balance, **16%**, is cupriferous mineralisation **(MET-2)**.

Metal associations are more consistent across La Infanta. Core intervals selected for La Infanta were designed to provide reasonable spatial coverage and statistical representation of grade distributions across the entire deposit.

Sample details are provided in Table 13-1 and the locations for each composite sample are illustrated in Figure 13-1 and Figure 13-2.

Table 13-1: Phase I Sample Details

Name	Sample Type	Deposit	Lens	Drillholes	Lens	Total Length (m)	Total Weight (kg)
MET-1	Zone composite: high Au/As	La Romanera	Lower	LR005, LR024, LR060, LR075, LR111, LR115, LR125	Lower	35.26	94.9
MET-2	Zone composite: high Cu / low Zn	La Romanera	Upper	LR006B, LR013, LR023, LR029, LR037, LR046, LR050, LR053, LR068, LR100, LR104, LR121, LR140	Upper	23.86	96.0
			Lower		Lower	16.30	
MET-3	Zone composite: average Cu/Zn	La Romanera	Upper	LR009, LR015, LR016, LR023, LR038, LR050, LR060, LR068, LR069, LR071, LR075, LR076, LR104, LR107, LR115, LR121, LR129, LR134, LR137, LR140, LR144	Upper	19.40	102.9
			Lower		Lower	20.84	
MET-4	Deposit composite	La Infanta	North	IN004, IN010, IN025, IN039B, IN045, IN058, IN060, IN060B, IN080	North	26.20	119.9
			South		South	6.25	
			South 1		South 1	5.45	

Figure 13-1: La Romanera – Phase I Sample Locations

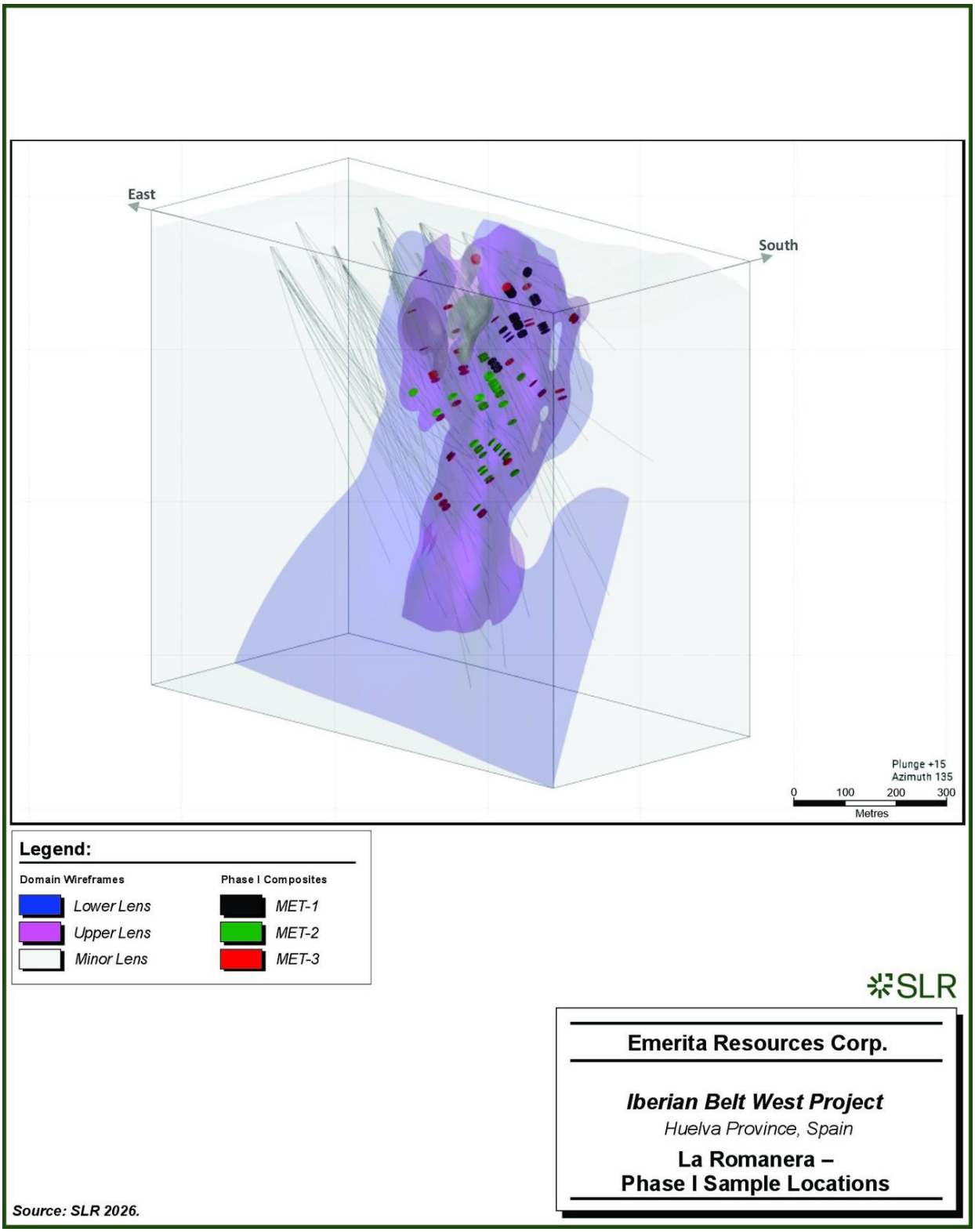
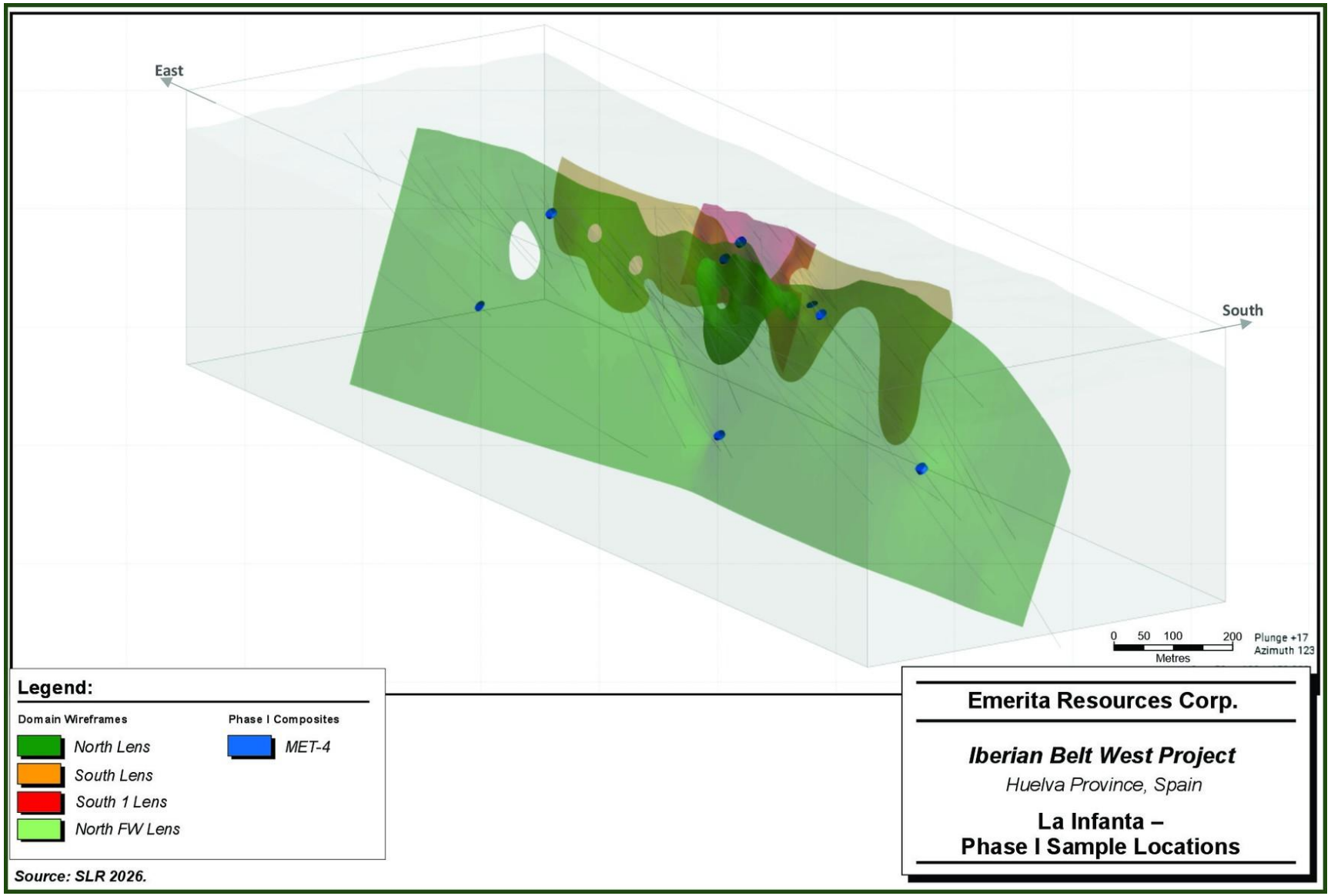


Figure 13-2: La Infanta – Phase I Sample Locations



13.2.2 Characterisation of Mineralised Material

The head assay results are summarised in Table 13-2.

Table 13-2: Phase I Head Assays

Sample ID	Head Grade (%), (*ppm)								
	Cu	Pb	Zn	Fe	As	Au*	Ag*	S_{TOT}	S_{SUL}
La Romanera MET-1	0.35	1.52	3.50	39.81	0.96	3.52	84.23	46.58	46.49
La Romanera MET-2	0.67	0.53	0.47	33.92	0.36	0.68	38.05	39.58	39.44
La Romanera MET-3	0.32	1.39	3.69	36.16	0.75	1.43	71.29	43.37	43.24
La Infanta MET-4	1.19	4.73	8.31	4.48	0.08	0.37	109.6	9.16	9.03

Mineralogical investigations determined that copper was mostly hosted by chalcopyrite across all four samples, with significant contributions from tetrahedrite. Lead was exclusively hosted by galena in all four samples. Zinc was exclusively hosted by sphalerite in MET-1 to MET-3 and was mostly hosted by sphalerite in MET-4, with minor siderite (2.1%).

13.2.2.1 Comminution Testwork

Each of the four composites were subject to a range of comminution testing including semi-autogenous grinding (SAG) Mill Comminution (SMC) testing, bond abrasion index testing (Ai), and bond ball mill work index (BWi) testing. The results are summarised in Table 13-3 to Table 13-5.

Table 13-3: SMC Test Results

Sample	Drop Weight Index (Dwi) (kWh/m³)	A	b	A*b	t_a	SAG Circuit Specific Energy (SCSE) (kWh/t)
La Romanera						
MET-1	8.1	77.6	0.70	54.3	0.32	8.38
MET-2	7.5	59.8	0.89	53.2	0.34	8.88
MET-3	8.6	85.2	0.60	51.1	0.30	8.64
La Infanta						
MET-4	4.4	61.3	1.17	71.7	0.59	8.21

Table 13-4: Bond Abrasion Index Test Results

Sample	Ai	Wear Rates (g/kWh)						
		Wet Rod Mill		Wet Ball Mill		Dry Ball Mill		Crushers
		Rod Media	Steel Liners	Ball Media	Steel Liners	Ball Media	Steel Liners	Liners
La Romanera								
MET-1	0.6159	143.14	13.62	134.20	10.12	17.80	1.78	34.47
MET-2	0.4189	132.10	12.10	117.71	8.99	14.68	1.47	26.35
MET-3	0.6747	145.86	14.01	138.39	10.41	18.63	1.86	36.89
La Infanta								
MET-4	0.2908	122.25	10.79	103.78	8.01	12.23	1.22	21.06

Table 13-5: Bond Ball Mill Work Index (BWi) Test Results

Sample	Feed, P_{80} (µm)	Product, P_{80} (µm)	BWi (kWh/t)
La Romanera			
MET-1	2,562	41	14.37
MET-2	2,466	43	14.79
MET-3	2,298	40	14.52
La Infanta			
MET-4	2,154	54	13.12

The SMC results showed the samples to be below average when compared against the JK Tech database of samples tested. The abrasion tests indicated the samples ranged from slightly abrasive to abrasive. The BWi values indicated the three La Romanera samples to be “hard” and the La Infanta sample to be “medium” in terms of ore hardness.

13.2.3 Flotation Testwork

The flotation testwork flowsheets varied between the four samples, although generally focussed on producing a bulk Cu-Pb concentrate and a separate Zn concentrate. La Romanera samples MET-1 and MET-3 performed very similarly under the same test conditions.

A series of rougher and open-circuit cleaner tests were undertaken on each sample before conducting locked cycle tests (LCTs). The results of the LCTs are summarised in Table 13-6 to Table 13-9.

Table 13-6: La Romanera MET-1 LCT Result

Test	Concentrate	Assay (%) *(ppm)						Recovery (%)					
		Cu	Pb	Zn	Au*	Ag*	S_{tot}	Cu	Pb	Zn	Au	Ag	S_{tot}
LCT1	Cu-Pb	7.23	36.79	2.31	5.13	1164.6	27.96	34.7	42.1	1.0	2.4	22.4	1.1
	Zn	0.87	3.28	49.01	2.33	181.1	32.78	16.8	15.1	86.0	4.4	14.0	5.0

Table 13-7: La Romanera MET-2 LCT Result

Test	Concentrate	Assay (%) *(ppm)						Recovery (%)					
		Cu	Pb	Zn	Au*	Ag*	S_{tot}	Cu	Pb	Zn	Au	Ag	S_{tot}
LCT1	Cu	18.32	9.2	2.9	1.80	366.0	37.37	70.8	43.8	14.5	6.5	20.7	2.6
LCT2	Cu	22.26	10.1	2.2	1.94	372.8	35.86	69.4	38.8	9.1	5.8	18.4	2.0

Table 13-8: La Romanera MET-3 LCT Result

Test	Concentrate	Assay (%) *(ppm)						Recovery (%)					
		Cu	Pb	Zn	Au*	Ag*	S_{tot}	Cu	Pb	Zn	Au	Ag	S_{tot}
LCT1	Cu-Pb	7.79	40.64	2.40	3.97	996.7	28.62	40.5	50.1	1.1	4.4	24.4	1.1
	Zn	0.63	2.05	49.66	1.25	138.3	35.12	12.7	9.7	84.1	5.3	13.0	5.1

Table 13-9: La Infanta MET-4 LCT Result

Test	Concentrate	Assay (%) *(ppm)						Recovery (%)					
		Cu	Pb	Zn	Au*	Ag*	S_{tot}	Cu	Pb	Zn	Au	Ag	S_{tot}
LCT1	Cu	29.23	6.89	5.79	11.17	1461.9	30.69	33.4	1.9	0.8	31.0	18.9	4.3
	Pb	6.03	44.11	20.44	1.11	624.6	22.81	52.2	91.6	22.4	23.4	61.0	24.0
	Zn	0.44	0.88	65.76	0.39	70.7	32.38	3.7	1.8	69.8	7.9	6.7	33.1
LCT2	Cu	24.77	11.10	6.74	7.38	1782.8	29.09	47.1	5.2	1.7	39.4	36.5	6.6
	Pb	5.40	54.92	14.04	0.60	509.5	21.64	33.4	84.1	11.4	10.3	33.9	15.9
	Zn	0.71	2.09	59.97	0.37	112.1	32.45	7.3	5.4	81.2	10.6	12.5	39.8

After initial rougher tests on samples MET-1 and MET-3 showed sequential flotation of copper and lead to be unsuccessful, the flotation regime opted for production of a semi-bulk Cu/Pb concentrate and a separate Zn concentrate.

The low head grades of lead and zinc in the La Romanera MET-2 sample meant that the flotation regime opted for copper flotation only after poor lead and zinc performance in the rougher flotation tests.

The La Infanta MET-4 sample was the only sample where sequential flotation of Cu, Pb, and Zn was found to be achievable.

13.3 Phase II Testwork

Phase II testing was conducted later in 2024 as a continuation of the earlier Phase I programme. The programme comprised four composite samples: two from La Romanera (MET-5 and MET-6), one from La Infanta (MET-7), and one blended sample combining material from La Romanera and La Infanta (MET-8). MET-5 was specifically designated for the evaluation of precious-metal recovery, focusing exclusively on gold and silver, while the remaining samples were used for the broader Phase II metallurgical programme. WAI issued the Phase II testwork report in December 2024, titled *ZT64-0940 La Romanera and La Infanta Project, Phase 2 Metallurgical Testwork (Base Metals)*.

In addition, in 2025, testwork was conducted on a separate composite sample from El Cura (MET-9) and similar testwork conducted as for MET 6-8. WAI issued a separate report for this work in March 2025 (ZT64-1147 El Cura Deposit, Metallurgical Testwork Report).

SLR notes that the LCT results for samples MET-6, MET-7, and MET-9 were subsequently used for the PFS process design.

Further work was conducted to float a fourth pyrite concentrate from the zinc flotation tails for all three deposit samples. These results were also incorporated into the process design and are described in Section 13.3.3.2.

The samples were subjected to a programme of rougher, cleaner, and locked cycle flotation testing to assess the effect of variations in feed grade and ore type on the production of Cu, Cu-Pb, Pb, and Zn concentrates.

An El Cura sample was additionally subjected to comminution testwork.

Apart from head assaying, no flotation or other tests were conducted on sample MET-5. No concurrent production is envisaged from La Romanera and La Infanta, meaning results of MET-8 testwork were not used in the PFS.

Metallurgical testwork on the MET-8 blend demonstrated that material from La Romanera and La Infanta can be processed jointly, achieving satisfactory metallurgical recoveries and saleable concentrate grades. Although concurrent production from the two deposits is not currently envisaged in the PFS mine plan, these results provide valuable technical flexibility should the joint processing of material from both deposits be considered in the future.

13.3.1 Sample Selection

Crushed drill core samples were provided by Emerita for Phase II flotation testing. Quartered HQ core from drillhole EC011 provided a 44 kg comminution sample for El Cura. Phase II samples included the following characteristics:

- **MET-5**: La Romanera high gold / low arsenic sample (electrum sample).
- **MET-6**: La Romanera deposit average – Upper and Lower Lenses.
- **MET-7**: La Infanta deposit average – North, South, and South 1 Lenses.
- **MET-8**: Composite of 30% La Infanta and 70% La Romanera.
- **MET-9**: El Cura deposit average – Top and Bottom Lenses.

For samples MET-6, MET-7, and MET-9, core intervals were selected to represent each deposit geographically along strike and down-dip. Selection criteria included approximating the average grades of the existing April 2025 Mineral Resource for each deposit. Sample selection at La Romanera represents a blend of the different mineralisation types tested during Phase II.

For metallurgical samples that informed PFS process design, details are summarised in Table 13-10 and the location of each sample is illustrated in Figure 13-3 to Figure 13-5.

Table 13-10: Phase II Sample Details

Name	Sample Type	Deposit	Drillholes	Lens	Total Length (m)	Total Weight (kg)
MET-6	Deposit composite	La Romanera	LR004, LR009, LR011, LR012, LR015, LR023, LR024, LR034, LR041, LR061, LR047, LR051, LR052, LR060, LR048, LR068, LR069, LR075, LR079, LR086, LR088, LR094, LR099, LR100, LR102, LR112, LR115, LR117, LR122, LR125, LR126, LR131, LR134, LR137, LR145, LR147, LR151, LR152, LR155, LR157, LR163, LR168	Upper	367.10	41.0
				Lower	474.27	
MET-7	Deposit composite	La Infanta	IN008, IN015, IN027, IN032, IN033, IN034, IN036, IN037, IN039, IN041, IN043, IN045, IN047, IN053, IN054, IN056, IN059, IN067, IN070, IN073, IN075, IN076, IN085	North	52.54	42.2
				South	32.30	
				South 1	8.00	
MET-9	Deposit composite	El Cura	EC002, EC003B, EC006, EC005, EC004, EC007, EC008, EC009, EC010, EC011, EC012, EC013, EC014, EC015	Top	54.40	90.0
				Bottom	16.90	

Figure 13-3: La Romanera – Phase II Sample Locations

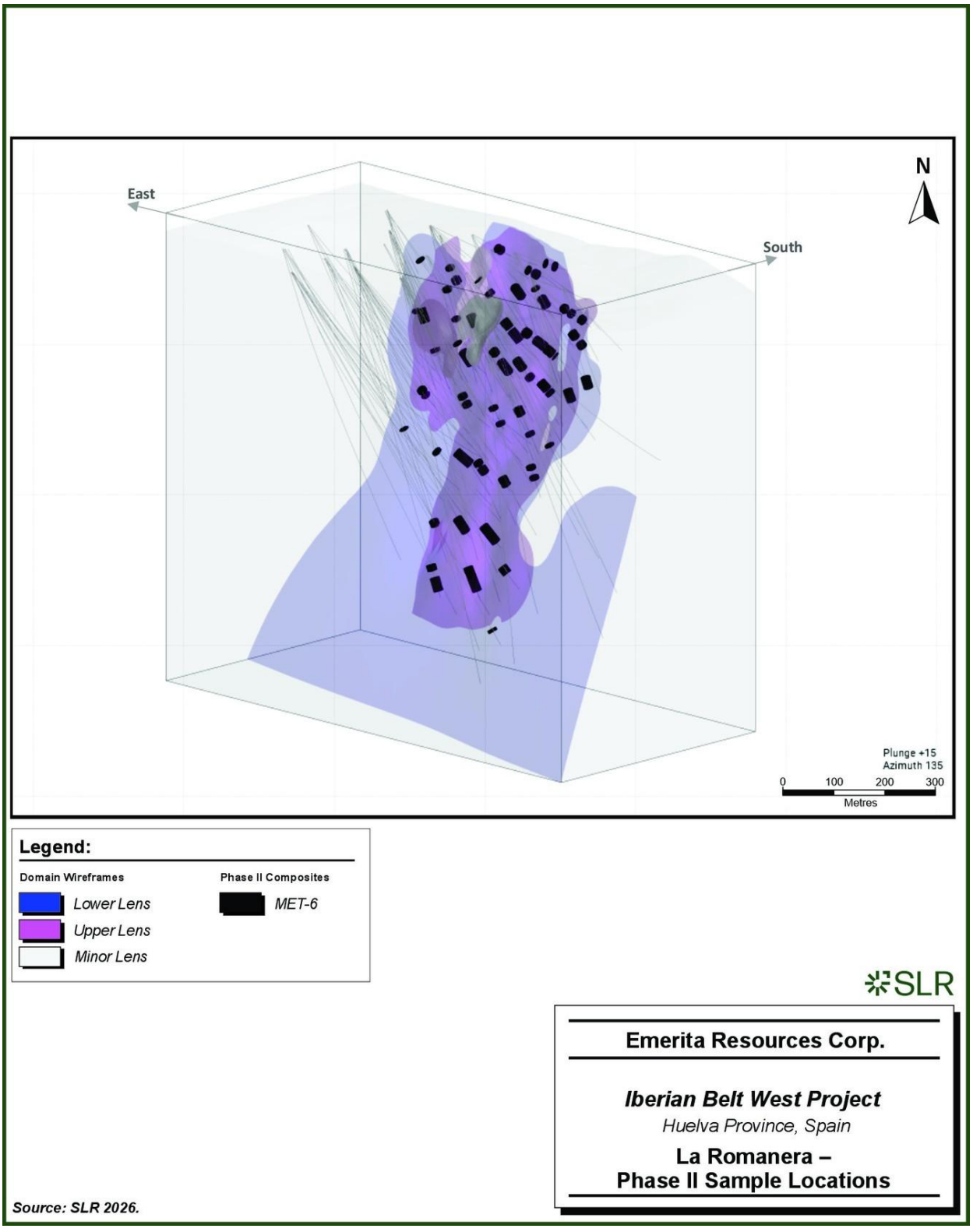


Figure 13-4: La Infanta – Phase II Sample Locations

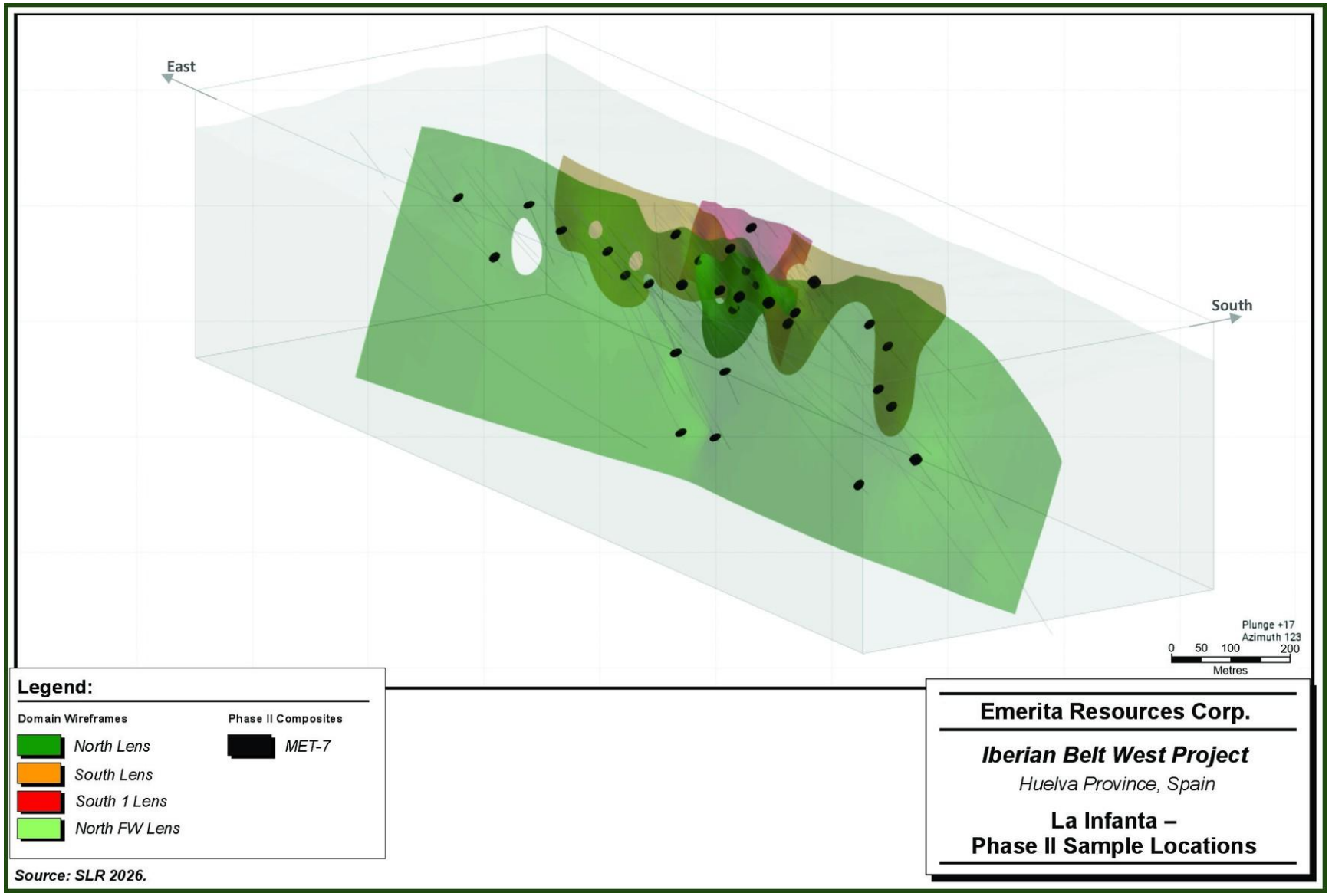
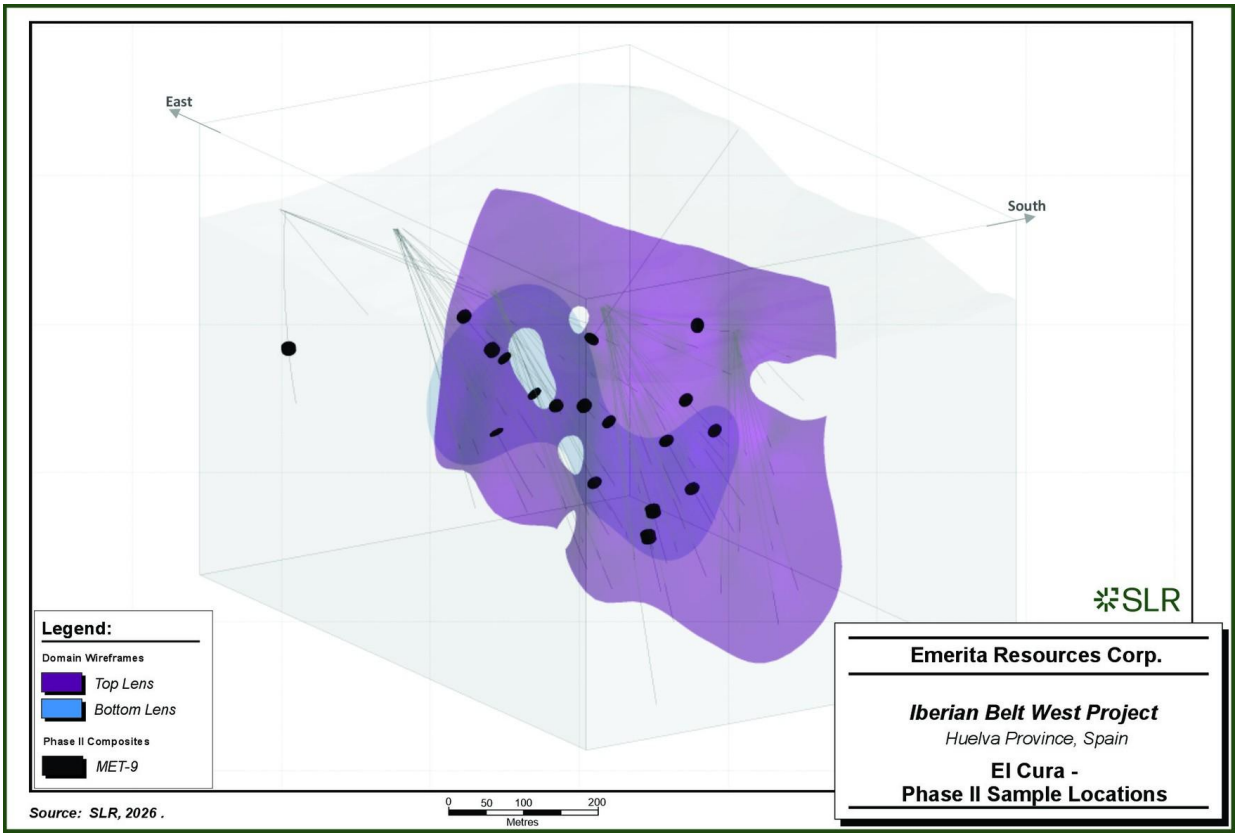


Figure 13-5: El Cura – Phase II Sample Locations



13.3.2 Characterisation of Mineralised Material

The head assays are summarised in Table 13-11.

Table 13-11: Phase II Head Assays

Sample ID	Assay (%), (*ppm)								
	Cu	Pb	Zn	Fe	As	Au*	Ag*	S_{TOT}	S_{SUL}
La Romanera MET-5	0.40	2.20	0.69	39.11	0.66	8.63	198.50	43.68	43.22
La Romanera MET-6	0.48	1.39	3.22	36.62	0.74	1.74	55.40	42.77	42.36
La Infanta MET-7	1.21	4.42	7.79	4.26	0.11	0.42	92.10	9.05	8.93
La Romanera + La Infanta MET-8	0.64	2.29	4.57	28.57	0.57	1.33	65.70	33.52	33.24
El Cura MET-9 Flotation Feed	1.67	0.59	1.13	27.94	0.28	1.61	41.26	33.57	33.44

As expected, the La Infanta composite (MET-7) had a much lower sulphur content than the other composite samples.

Mineralogical investigation for the MET-9 El Cura sample indicated that the Cu, Pb, and Zn are almost exclusively hosted by chalcopyrite, galena, and sphalerite respectively. The Fe and S are mostly hosted by pyrite.

13.3.2.1 Comminution Testwork

SMC, bond abrasion index tests, and ball mill work index tests were conducted, and the results are summarised in Table 13-12 to Table 13-14.

Table 13-12: SMC Results – El Cura

Sample	Drop Weight Index (Dwi) (kWh/m^3)	A	b	A*b	t_a	SAG Circuit Specific Energy (SCSE) (kWh/t)
MET-9	9.04	70.3	0.59	41.5	0.29	10.46

Table 13-13: Bond Abrasion (Ai) Results – El Cura

Sample	Ai	Wear Rates (g/kWh)						
		Wet Rod Mill		Wet Ball Mill		Dry Ball Mill		Crushers
		Rod Media	Steel Liners	Ball Media	Steel Liners	Ball Media	Steel Liners	Liners
MET-9	0.5754	141.1416	13.3439	131.1409	9.9126	17.2037	1.7204	32.7989

Table 13-14: Bond Ball Mill Work Index (BWi) Results – El Cura

Sample	Feed, P_{80} (µm)	Product, P_{80} (µm)	BWi (kWh/t)
MET-9	2,190	40	14.23

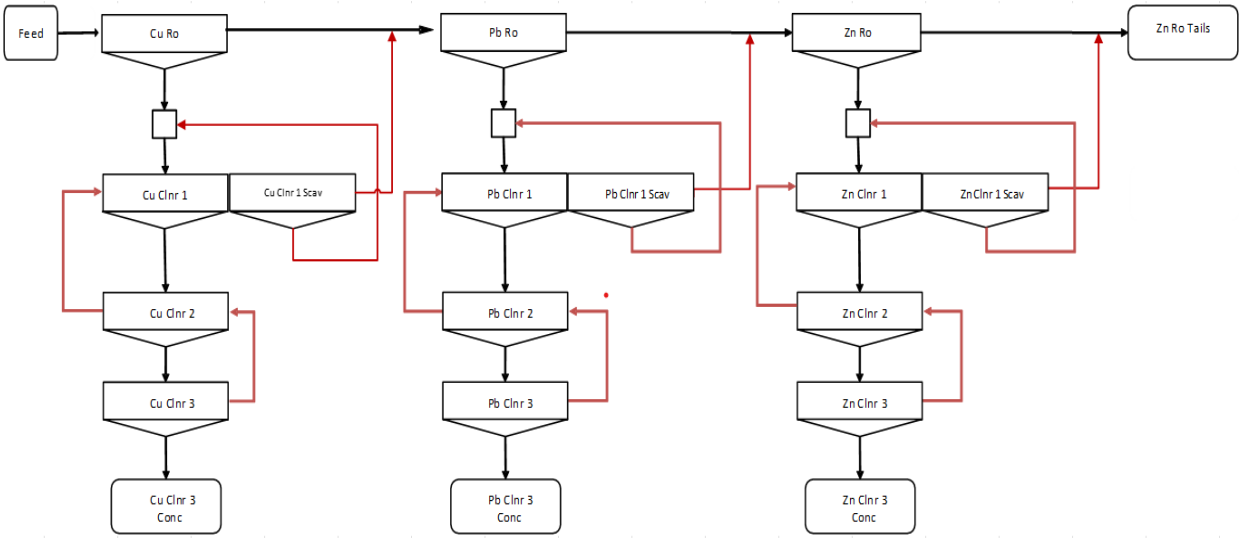
The SMC results showed MET-9 to be above average when compared against the JK Tech database of samples tested. The Ai results indicated the sample to be “medium abrasive”. The BWi results indicated the sample to be classified as “hard” with respect to ore grindability.

13.3.3 Flotation Testwork

Figure 13-6 shows the LCT testwork flowsheet used for all Phase II tests.

Conventional flotation reagents and conditions were used for a selective Cu-Pb-Zn flotation circuit. The primary grind size required was fine at 80% passing 38 µm. The Cu and Pb rougher concentrates were reground to 80% passing 15 µm and the Zn rougher concentrate was reground to 80% passing 10 µm.

Figure 13-6: Phase II LCT Testwork Flowsheet



Source: ZT64-0940 La Romanera and La Infanta Project, Phase 2 Metallurgical Testwork (Base Metals).

The LCT results for each of the three deposits (MET-6, MET-7, and MET-9) based on selective Cu-Pb-Zn flotation are summarised in Table 13-15 to Table 13-17. These are the results taken forward for use in the PFS process design.

The LCT results for the blended sample MET-8 are also included for reference in Table 13-18. As discussed above, although this composite does not represent the revised LOM schedule and was therefore not used as the basis for the PFS process design, the results demonstrate the technical feasibility of jointly processing material from La Romanera and La Infanta, with satisfactory metallurgical recoveries and concentrate grades.

Table 13-15: La Romanera MET-6 Locked Cycle Test Results

Test	Concentrate	Assay (%) *(ppm)								Recovery (%)							
		Cu	Pb	Zn	Fe	As	Au*	Ag*	S_{tot}	Cu	Pb	Zn	Fe	As	Au	Ag	S_{tot}
LCT1	Cu	20.43	11.14	5.39	23.22	0.60	7.72	986.8	34.58	41.5	7.3	1.5	0.7	0.8	4.1	14.2	0.7
	Pb	2.88	26.76	4.09	25.55	0.90	2.88	493.6	38.00	17.4	52.2	3.4	2.3	3.4	4.5	21.0	2.4
	Zn	0.72	1.16	50.10	9.65	0.52	1.25	137.8	36.98	8.3	4.3	78.7	1.7	3.7	3.7	11.2	4.4

Table 13-16: La Infanta MET-7 Locked Cycle Test Results

Test	Concentrate	Assay (%) *(ppm)								Recovery (%)							
		Cu	Pb	Zn	Fe	As	Au*	Ag*	S_{tot}	Cu	Pb	Zn	Fe	As	Au	Ag	S_{tot}
LCT1	Cu	20.18	21.09	6.64	11.94	0.95	4.01	1522.8	25.37	42.4	10.6	1.8	5.9	17.3	22.5	33.6	5.9
	Pb	5.79	47.89	16.59	3.24	0.52	0.92	639.7	22.06	39.7	78.3	14.7	5.2	31.1	16.8	46.1	16.7
	Zn	0.56	1.84	57.50	1.45	0.08	0.41	76.7	31.42	5.9	4.6	78.0	3.6	7.4	11.6	8.5	36.4

Table 13-17: El Cura MET-9 Locked Cycle Test Results

Test	Concentrate	Assay (%) *(ppm)								Recovery (%)							
		Cu	Pb	Zn	Fe	As	Au*	Ag*	S_{tot}	Cu	Pb	Zn	Fe	As	Au	Ag	S_{tot}
LCT2	Cu	22.89	5.52	2.46	29.81	0.16	2.35	198.8	36.83	79.4	53.0	13.3	5.7	3.0	9.8	33.1	6.3
	Pb	7.85	4.19	3.45	34.11	0.37	2.90	643.4	44.90	4.0	5.9	2.7	1.0	1.0	1.8	15.6	1.1
	Zn	2.92	1.02	45.20	13.84	0.16	2.17	316.4	36.79	2.8	2.7	67.9	0.7	0.8	2.5	14.7	1.8

Table 13-18: La Romanera/La Infanta MET-8 Locked Cycle Test Results

Test	Concentrate	Assay (%) *(ppm)								Recovery (%)							
		Cu	Pb	Zn	Fe	As	Au*	Ag*	S_{tot}	Cu	Pb	Zn	Fe	As	Au	Ag	S_{tot}
LCT1	Cu	25.84	11.56	5.52	21.14	0.59	5.26	1165.6	31.62	31.9	4.1	1.0	0.7	0.8	3.6	12.6	0.8
	Pb	5.63	36.37	9.36	16.16	0.90	2.32	674.0	30.19	38.7	72.6	9.4	3.1	6.9	8.8	40.5	4.2
	Zn	0.67	1.06	54.39	6.04	0.37	1.02	130.8	34.84	6.1	2.8	72.4	1.6	3.8	5.1	10.4	6.5

13.3.3.1 Concentrate Analysis

The final concentrates produced in the LCTs were submitted for detailed chemical analysis to a third-party laboratory. The main penalty elements of interest include As, Cd, Hg, Sb, Cl, and F, and assay results for these elements are summarised in Table 13-19.

Table 13-19: Penalty Elements in LCT Final Concentrates

Composite/Test	Product	Assay (ppm)					
		Cl	F	As	Cd	Hg	Sb
La Romanera MET-6	Cu Conc	<50	430	3,820	185	1,215	9,800
	Pb Conc	60	130	8,380	123	745	5,110
	Zn Conc	60	30	4,740	1,500	3,970	946
La Infanta MET-7	Cu Conc	50	4,150	6,010	325	435	43,700
	Pb Conc	<50	2,060	4,670	585	444	24,600
	Zn Conc	<50	220	505	2,110	1,245	1,460
El Cura MET-9	Cu Conc	70	<20	1,560	53	78	2,080
	Pb Conc	50	<20	1,790	57	94	3,140
	Zn Conc	60	240	1,570	1,130	1,180	4,630

An independent marketing report was commissioned by Emerita (Cuadri 2025) and, after review by SLR, it has been used as the basis for the metals payabilities and penalty element deductions applied for the net smelter return (NSR) calculations for each of the concentrates. The payabilities and deductions forecasted for each deposit, based on the composite sample LCT results provided in Table 13-15 to Table 13-17 and the independent marketing report, are summarized in the following subsections.

La Romanera – MET-6

- **The copper concentrate graded 20.4% Cu at a recovery of 41.5%.** A further 17.4% of the copper reported to the lead concentrate, where it may be payable based on either the lead price or an agreed percentage of the copper price, while a further 8.3% reported to the zinc concentrate, where it would typically not be payable.

  These results provided a clear basis for directing subsequent metallurgical optimisation towards the production of separate copper and lead concentrates, rather than a bulk Cu-Pb concentrate, with the objective of improving copper selectivity, recovery to the designated concentrate and overall payable metal value.

- **The lead concentrate graded 26.8% Pb at 52.2% recovery**. This grade is significantly less than normal benchmark levels for lead concentrates of approximately 50% Pb. Lead recovered in the copper and zinc concentrates at 7.3% and 4.3%, respectively, is normally unpayable.

- **The zinc concentrate graded 50.1% Zn at 78.7% recovery.** Zinc was recovered in the copper and lead concentrates at 1.5% and 3.4%, respectively, and is normally unpayable.

- Total gold recovered in the Cu, Pb, and Zn concentrates was 12.3%.

- Total silver recovered in the Cu, Pb, and Zn concentrates was 46.4%.

La Infanta – MET-7

- **The copper concentrate graded 20.2% Cu at 42.4% recovery**. Copper was recovered in the lead concentrate at 39.7% and is normally payable based on using either the lead price or a percentage of the copper price. Copper was recovered in the zinc concentrate at 5.9% and is normally unpayable.
- **The lead concentrate graded 47.9% Pb at 78.3% recovery**. Lead recovered in the copper and zinc concentrates at 10.6% and 4.6%, respectively, is normally unpayable.
- **The zinc concentrate graded 57.5% Zn at 78.0% recovery**. Zinc was recovered in the copper and lead concentrates at 1.8% and 14.7%, respectively, and is normally unpayable.
- Total gold recovered in the Cu, Pb, and Zn concentrates was 50.9%.
- Total silver recovery in the Cu, Pb, and Zn concentrates was 88.2%.

El Cura – MET-9

- **The copper concentrate graded 22.9% Cu at 79.4% recovery**. Copper recovered in the lead and zinc concentrates was 4.0% and 2.8%, respectively and is normally unpayable.
- **The lead concentrate graded only 4.2% Pb at 5.9% recovery.** This is a very low grade and recovery and therefore not included as a saleable concentrate, i.e., no lead concentrate will be produced.
- **The zinc concentrate graded 45.2% Zn at 67.9% recovery**. Zinc was recovered in the copper and lead concentrates at 13.3% and 2.7%, respectively, and is normally unpayable.
- Total gold recovered in the Cu and Zn concentrates was 12.3%.
- Total silver recovered in the Cu and Zn concentrates was 47.8%.

13.3.3.2 Pyrite Flotation

Pyrite is abundant, particularly in the La Romanera and El Cura deposits, and is reflected in their overall sulphur head grades. It also shows strong associations with a significant proportion of the precious metals not recovered to the base-metal concentrates. The recovery of an additional pyrite concentrate therefore represents a potential opportunity, supported by a market driven principally by sulphur content, with a benchmark grade of approximately 48% S and potential additional payability for the associated precious-metal content.

Further testwork was conducted to assess the production of an additional pyrite concentrate. The initial objective was to reduce the mass reporting to the downstream PFP process while concentrating the pyrite-associated precious metals. The testwork also demonstrated that the resulting pyrite concentrate met the principal characteristics of a potentially marketable product, providing the option either to process it through PFP or to sell it directly. WAI issued a separate report for La Romanera and La Infanta in February 2025 (ZT64-0940, La Romanera and La Infanta Project, Phase 2 Metallurgical Testwork (Gold Study), February 2025) and reported the El Cura work as part of the original flotation studies in March 2025 (ZT64-1147, El Cura Deposit, Metallurgical Testwork Report, March 2025).

Locked-cycle testing was not considered necessary at this stage because the open-circuit results demonstrated that a single, straightforward rougher-flotation stage could produce high-quality pyrite concentrates from La Romanera and El Cura, grading at or above approximately 48% S. The consistency of these results supports a practical and efficient route for producing potentially marketable pyrite concentrates from these deposits.

For La Romanera MET-6, 10 rougher flotation tests were performed on the combined rougher tailings sample, with Test FT1 taken as the optimum result.

For La Infanta MET-7, a single rougher flotation test was conducted on the combined rougher tailings sample.

For El Cura MET-9, two rougher tests were conducted on the LCT2 tails and an optimum result was selected.

Conventional flotation reagents were used based on the production of a bulk sulphide concentrate.

Table 13-20 summarises the optimal results for testing the Zn flotation tails for each of the three samples.

Table 13-20: Final Tails Pyrite Flotation Test Results

Test	Sample	Assay (%) *(ppm)								Recovery (%)							
		Cu	Pb	Zn	Fe	As	Au*	Ag*	S_{TOT}	Cu	Pb	Zn	Fe	As	Au	Ag	S_{TOT}
LA Romanera MET-6 Final Tails Pyrite Flotation Test Results																	
FT1	Combined	0.15	0.47	0.47	46.04	0.62	1.66	46.6	50.67	81.5	69.1	87.4	89.0	71.3	88.4	87.6	93.6
La Infanta MET-7 Final Tails Pyrite Flotation Test Results																	
FT1	Combined	0.16	0.32	0.29	15.86	0.18	0.61	22.7	17.08	38.6	27.2	36.6	66.0	74.5	65.3	61.1	76.8
El Cura MET-9 Final Tails Pyrite Flotation Test Results																	
LCT2 Py Rougher	LCT2 tails	0.36	0.25	0.18	40.35	0.47	1.85	27.5	48.09	80.8	66.5	68.5	85.2	91.8	87.4	87.6	91.1

Key results from the pyrite flotation include the following:

- For La Romanera MET-6, a pyrite concentrate grading 50.7% S at 93.6% S recovery was obtained, with 1.66 g/t Au and 46.6 g/t Ag.
- For La Infanta MET-7, a pyrite concentrate grading 17.1% S at 76.8% S recovery was obtained, with 0.61 g/t Au and 22.7 g/t Ag.
- For El Cura MET-9, a pyrite concentrate grading 48.1% S at 91.1% S recovery was obtained, with 1.85 g/t Au and 27.5 g/t Ag.

Testwork has demonstrated that the La Romanera and El Cura deposits can produce pyrite concentrates meeting or exceeding the benchmark sulphur grade of approximately 48% S for a saleable product. The associated gold and silver content could further enhance the commercial attractiveness and potential value of these concentrates.

A marketing report from Claight was used as the basis for providing NSR values for the pyrite concentrate. For further information, refer to Sections 21.0 and 22.0.

13.4 Metallurgical Testwork Summary

The Phase I metallurgical testwork programme focussed on composite samples from La Romanera and La Infanta and evaluated a flowsheet based on the production of a bulk Cu-Pb concentrate and a separate Zn concentrate. Sequential flotation to produce separate Cu, Pb, and Zn concentrates was evaluated in the LCT conducted on the La Infanta MET-4 sample. The Phase I results provided the basis for the optimisation testwork completed during Phase II, which focussed on developing a common sequential flotation flowsheet for the deposits and improving metal selectivity and payability. The comminution testwork conducted during Phase I was taken forward for use in the PFS process design for La Romanera and La Infanta.

Following review of the Phase I testwork programme results, a Phase II testwork programme was conducted based on sequential flotation on new composite samples from La Romanera and La Infanta but also including a later composite sample from El Cura. Additional comminution testwork was conducted for the El Cura composite sample.

The Phase II LCT results for the three composite samples (La Romanera MET-6, La Infanta MET-7, and El Cura MET-9) were subsequently taken forward for use in the PFS process design and final metallurgical balance.

LCT was also conducted on the MET-8 composite, comprising blended material from La Romanera and La Infanta. The results demonstrated that material from these deposits can be processed jointly through the sequential flotation flowsheet, achieving acceptable metallurgical recoveries and concentrate grades. Although MET-8 was not used as the basis for the PFS process design, the results confirm the technical flexibility to process blended feed from La Romanera and La Infanta, should this be required by future mine scheduling. Given the similarities between the mineralisation at El Cura and La Romanera, it is considered reasonable to expect that El Cura material could also be incorporated into a blended processing campaign. This potential should be confirmed through additional blend testwork during the next phase of metallurgical development.

Additionally, as part of the Phase II testwork programme, the final Zn flotation tails from the composite samples were subjected to an additional flotation stage. The initial objective was to reduce the mass reporting to the downstream PFP process by recovering a pyrite concentrate containing a significant proportion of the Au and Ag not recovered to the base-metal concentrates. The testwork demonstrated that a single, straightforward rougher-flotation stage

could effectively recover pyrite and associated precious metals. In particular, the La Romanera and El Cura samples produced high-quality pyrite concentrates with sulphur grades meeting or exceeding the benchmark grade of approximately 48% S for a saleable product. The associated gold and silver recoveries further enhance the potential commercial attractiveness and value of these concentrates. These results supported the inclusion of pyrite flotation in the PFS process design and final metallurgical balance, providing a simple and effective route for generating an additional potentially marketable product.

In terms of the base metal concentrates (Cu, Pb, and Zn) produced from the three deposit samples, generally acceptable recoveries and concentrate grades were achieved, supporting their potential sale to smelters or traders. Although the La Romanera MET-6 Pb concentrate grade was below the typical benchmark, its high silver content materially enhances its commercial attractiveness and potential value. A separate saleable Pb concentrate is not currently envisaged for El Cura MET-9. Certain concentrates contain penalty elements; however, the associated deductions have been incorporated into the NSR calculations using the marketing assumptions provided by Cuadri y de la Corte (2025). The La Romanera copper concentrate is expected to be marketable through a trader, providing an established route to market. Overall, the gold and silver content of the concentrates contributes additional payable value and enhances their marketability despite the presence of penalty elements. Further optimisation and variability testwork will provide opportunities to improve concentrate selectivity and grades and to better define and manage the distribution of deleterious elements.

Combined Au recoveries from all three base metals concentrates were low for La Romanera MET-6 and El Cura Met-9, at approximately 12%, but higher at approximately 50% for La Infanta MET-7.

Apart from La Infanta MET-7, high benchmark S grades were achieved at high S recoveries and mass splits to concentrate, i.e., high concentrate tonnage. Currently, the pyrite concentrate market is strong, and is based on benchmark sulphur grades of 48% S. These grades were achieved for both the La Romanera and El Cura samples tested, with additional payabilities from the gold and silver content determined from the marketing report.

Table 13-21 summarises the metallurgical balance incorporating the results of the LCTs on La Romanera MET-6, La Infanta MET-7, and El Cura MET-9, including the pyrite flotation tests conducted on each of the final Zn flotation tails. It is important to note that La Romanera represents 83% of the total resource tonnes.

Note also that the mass splits of the base metals concentrates were re-calculated based on the 2025 MRE head grades rather than the test sample head grades, but assuming the same test result metals recoveries and concentrate grades.

It should also be noted that the mass splits of the base-metal and pyrite concentrates were recalculated using the 2025 MRE head grades. The calculations were based on the experimental results obtained from the metallurgical testwork programmes, applying the measured metal recoveries and concentrate grades to the updated 2025 MRE feed grades to estimate the corresponding concentrate masses.

Table 13-21: Metallurgical Balance

										Recoveries					
	Concentrate	LOM	TPY	%Mass	Zn %	Pb %	Cu %	Ag ppm	Au ppm	Stot %	Zn %Rec	Pb %Rec	Cu %Rec	Ag %Rec	Au %Rec	S %Rec
MRE Q1-2025	FEED	21,470,000	1,200,000	100%	2.72	1.25	0.46	62.06	1.24	37.94	100.0%	100.0%	100.0%	100.0%	100.0%	100.0%
La Romanera	Cu Conc	202,534	11,320	0.9%	4.32	9.74	20.43	932.70	5.35	29.07	1.5%	7.3%	41.5%	14.2%	4.1%	0.7%
	Pb Conc	525,040	29,346	2.4%	3.74	26.76	3.30	533.48	2.28	36.52	3.4%	52.2%	17.4%	21.0%	4.5%	2.4%
	Zn Con	918,383	51,330	4.3%	50.10	1.26	0.90	162.73	1.08	38.83	78.7%	4.3%	8.3%	11.2%	3.7%	4.4%
	Pyr Conc	13,929,564	778,550	64.9%	0.61	0.48	0.19	44.91	1.48	50.67	14.4%	25.0%	26.8%	47.0%	77.5%	86.6%
	Tail-Final	5,894,480	329,454	27.5%	0.21	0.51	0.10	14.98	0.46	8.16	2.1%	11.2%	6.1%	6.6%	10.2%	5.9%
	Concentrate	LOM	TPY	%Mass	Zn %	Pb %	Cu %	Ag ppm	Au ppm	Stot %	Zn %Rec	Pb %Rec	Cu %Rec	Ag %Rec	Au %Rec	S %Rec
MRE Q1-2025	FEED	3,000,000	1,200,000	100%	5.28	3.01	0.81	81.48	0.37	7.28	100.0%	100.0%	100.0%	100.0%	100.0%	100.0%
La Infanta	Cu	51,181	20,472	1.7%	0.06	0.19	20.18	1606.49	4.87	25.11	1.8%	10.6%	42.4%	33.6%	22.5%	5.9%
	Pb	147,932	59,173	4.9%	0.16	47.89	6.54	762.04	1.26	24.65	14.7%	78.3%	39.7%	46.1%	16.8%	16.7%
	Zn	214,823	85,929	7.2%	57.50	1.94	0.67	96.38	0.60	37.03	78.0%	4.6%	5.9%	8.5%	11.6%	36.4%
	Pyr Conc	402,768	161,107	13.4%	0.79	0.40	0.28	43.70	0.88	17.08	2.0%	1.8%	4.7%	7.2%	32.1%	31.5%
	Tail-Final	2,183,296	873,318	72.8%	0.25	0.20	0.08	5.13	0.09	0.95	3.5%	4.7%	7.4%	4.6%	17.1%	9.5%
	Concentrate	LOM	TPY	%Mass	Zn %	Pb %	Cu %	Ag ppm	Au ppm	Stot %	Zn %Rec	Pb %Rec	Cu %Rec	Ag %Rec	Au %Rec	S %Rec
MRE Q1-2025	FEED	1,290,000	1,200,000	100%	1.87	0.82	1.49	45.90	1.44	32.57	100.0%	100.0%	100.0%	100.0%	100.0%	100.0%
El Cura	Cu	66,442	61,806	5.2%	4.83	8.43	22.89	294.97	2.74	40.14	13.3%	53.0%	79.4%	33.1%	9.8%	6.3%
	Pb	14,810	13,777	1.1%	4.44	4.19	5.14	625.36	2.22	32.05	2.7%	5.9%	4.0%	15.6%	1.8%	1.1%
	Zn	36,349	33,813	2.8%	45.20	0.79	1.48	238.89	1.29	20.40	67.9%	2.7%	2.8%	14.7%	2.5%	1.8%
	Pyr Conc	722,413	672,012	56.0%	0.37	0.37	0.30	26.27	1.93	48.09	11.0%	25.5%	11.2%	32.0%	75.1%	82.7%
	Tail-Final	449,986	418,592	34.9%	0.27	0.30	0.11	5.99	0.45	7.54	5.1%	12.9%	2.7%	4.6%	10.8%	8.1%
	Concentrate	LOM	TPY	%Mass	Zn %	Pb %	Cu %	Ag ppm	Au ppm	Stot %	Zn %Rec	Pb %Rec	Cu %Rec	Ag %Rec	Au %Rec	S %Rec
MRE Q1-2025	FEED	25,760,000	1,200,000	100%	2.98	1.44	0.56	63.51	1.15	34.10	100.0%	100.0%	100.0%	100.0%	100.0%	100.0%
IBW Project Total	Cu	320,156	14,914	1.2%	4.63	10.90	20.90	908.07	4.73	30.73	1.9%	9.4%	46.7%	17.8%	5.1%	1.1%
	Pb	687,782	32,040	2.7%	6.33	30.82	4.03	584.62	2.06	33.87	5.7%	57.3%	19.4%	24.6%	4.8%	2.7%
	Zn	1,169,555	54,482	4.5%	51.31	1.37	0.87	152.91	1.00	37.93	78.2%	4.3%	7.1%	10.9%	4.0%	5.0%
	Pyr Conc	15,054,745	701,308	58.4%	0.60	0.48	0.20	43.99	1.49	49.64	11.8%	19.3%	21.0%	40.5%	75.7%	85.1%
	Tail-Final	8,527,762	397,256	33.1%	0.22	0.42	0.10	11.98	0.36	6.28	2.5%	9.6%	5.8%	6.2%	10.5%	6.1%

13.4.1 Recommendations for Future Testwork

Metallurgical testwork has been completed for the IBW Project through Phases I and II. This work included mineralogical characterisation, comminution testing, open-circuit flotation optimisation and LCTs on samples from La Romanera, La Infanta and El Cura, selected based upon representativity, assessment of mineralisation and the processing route chosen at the time.

Metallurgical variability at La Romanera was initially addressed during Phase I through testing of three composite samples, MET-1, MET-2 and MET-3. These samples represented the principal mineralisation types initially identified within the deposit, including high Au-As polymetallic mineralisation, Cu-rich mineralisation and the predominant polymetallic mineralisation. The samples were selected from multiple drillholes to provide spatial coverage and representation of the grade distributions within the Upper and Lower Lenses. La Infanta and El Cura, being smaller deposits, were each represented in testwork by deposit-scale composite samples selected to reflect their principal mineralisation characteristics and resource grades as assessed by the MRE at the time.

However, the flotation flowsheets evaluated during Phase I differed from the final sequential-flotation flowsheet developed during Phase II. The metallurgical samples for Phase II were selected to represent the Indicated and Inferred Mineral Resources included in the 2025 MRE and the geological understanding available when the testwork programmes were designed.

For Phase II, only one LCT was performed for each composite sample representing the three deposits (MET 6, MET-7, and MET-9). Sample selection for each deposit composite was designed to align with average grades in the existing April 2025 IBW Project MRE. Subsequent changes in economic and technical parameters, including those associated with the revised PFS flowsheet, have caused a net reduction in reported MRE average grades relative to metallurgical sample head grades.

There is therefore a lack of variability test work for the mine schedule and selective flotation flowsheet proposed in this report.

The QP recommends that a sufficient number of variability samples for each deposit be tested at PFS-level to confirm metallurgical response and ore hardness variability across the respective deposits, in particular concentrate quality and the impact of deleterious elements, to ensure the flowsheet design is flexible to accommodate any such variability. A general rule of thumb is to allow for one sample per one million tonnes of resource and is also dependent on the identified domains and lithologies within each deposit that may require separate testwork. The lack of variability samples represents a risk that will need to be addressed in the next phase of testwork. In effect, only the one LCT result from Phase I, La Infanta MET-4, represents a variability sample based on the selective flotation flowsheet.

Sample selection for variability testwork should consider the lower average metal grades reported in the PFS MRE and Mineral Reserve estimate, local variation in mineralisation type at La Romanera, and blending of mineralisation from the three deposits, in line with the PFS production schedule.

Thickening and filtration testwork has not yet been completed on the base-metal concentrates, pyrite concentrates or final flotation tailings. The PFS design developed by Zenito Limited is based on industry benchmark data for these conventional unit operations. Thickening, rheology and filtration testing on bulk samples should be completed during the next phase of engineering to validate equipment sizing, operating parameters and product moisture assumptions.

SLR considers the lack of variability testwork to present a higher risk compared to the lack of thickening and filtration testwork, particularly with regards to concentrate quality and the impact of deleterious elements. The focus for the variability testwork programme should be on La Romanera, which comprises the bulk of the resource, although tests on blended samples conforming to the latest mine schedule should also be conducted.

For the PFS MRE and resulting lower head grades, and without variability testwork to assess the impact of this on metals recoveries and concentrate quality, the same methodology as for the difference between the metallurgical samples and Q1 2025 MRE head grades was used, i.e., recalculating the mass splits to concentrate assuming the same metals recoveries and concentrate grades. This results in lower annual concentrate production and higher annual tailings production. Future variability testwork will assess the impact of these lower head grades on metals recoveries and concentrate quality.

14.0 Mineral Resource Estimates

14.1 Introduction

The Mineral Resource estimates discussed in this Technical Report are located within Emerita's IBW Project, contained in the La Romanera, La Infanta, and El Cura polymetallic deposits. Mineral Resource estimation was completed by SLR using drillhole databases and mineralisation models developed by the Emerita geology team and subsequently verified and refined in collaboration with SLR.

14.2 Mineral Resource Estimate Data

14.2.1 General

Drillhole data used for Mineral Resource estimation were limited to surface diamond core drilling. The cut-off date for the databases was January 16, 2026. Historical drilling exists at all deposits, but was excluded from estimation due to an incomplete assay suite, lack of QA/QC support, and uncertain location accuracy. New Emerita drilling has replaced any historical drill coverage. A summary of the Mineral Resource databases is shown in Table 14-1.

Table 14-1: Summary of MRE Drillhole Databases

Deposit	Year	Number of Diamond Drillholes	Drill Metres	Number of Drill Samples	Drill Sample Metres	Number of Density Samples	Density Metres
La Romanera	2022	92	34,779.1	4,120	3,802.1	3,818	550.2
	2023	71	31,863.1	2,402	2,432.3	2,112	308.4
	2024	6	3,702.1	276	321.5	236	34.6
	Sub-Total	**169**	**70,344.3**	**6,798**	**6,556.0**	**6,166**	**893.2**
La Infanta	2021	31	4,511.3	896	939.9	803	116.8
	2022	38	10,796.9	894	875.9	795	120.1
	2023	22	5,666.8	449	450.8	395	56.3
	2025	1	672.2	25	29.9	24	2.9
	Sub-Total	**92**	**21,647.1**	**2,264**	**2,297**	**2,017**	**296**
El Cura	2023	6	2,118.8	82	85.7	56	8.1
	2024	26	9,896.2	605	684.7	444	62.9
	2025	59	19,235.0	1,087	1,271.3	758	104.5
	Sub-Total	**91**	**31,250.0**	**1,782**	**2,051.9**	**1,259**	**175.6**
IBW Project MRE Total		**352**	**123,241.3**	**10,844**	**10,904.4**	**9,442**	**1,365.0**

14.2.2 Software

Database import and preparation, wireframe modelling, statistical analysis, compositing, variographic analysis, block modelling, and grade estimation were undertaken using Leapfrog Geo and Leapfrog Edge software. Statistical and variographic analyses were also undertaken using Snowden Supervisor software.

14.2.3 Data Validation

The database was reviewed by the QP using the checks outlined in Section 12.3.2. Checks identified only minor errors that were corrected prior to resource modelling.

14.3 Geological Interpretation and Domaining

14.3.1 Mineralisation

La Romanera, La Infanta, and El Cura are classified as VMS deposits and occur as tabular strata-bound lenses of polymetallic (Zn, Pb, Cu, Ag, Au) sulphides. Surface drilling has so far defined six major sulphide lenses across the three deposits: the Upper and Lower lenses at La Romanera; the North, South, and South 1 lenses at La Infanta; and the Top Lens at El Cura.

Four minor parallel lenses at La Romanera (Lower HW1, Upper HW1, Upper HW2, and Upper HW3) and one at La Infanta (North FW1) capture significant intersections with interpreted continuity that sit outboard of the main mineralised zones. The Bottom Lens at El Cura is at a preliminary stage of exploration. Thus far, the number and grade of intersections do not support the definition of Mineral Resources for this domain and it has been excluded from resource estimation.

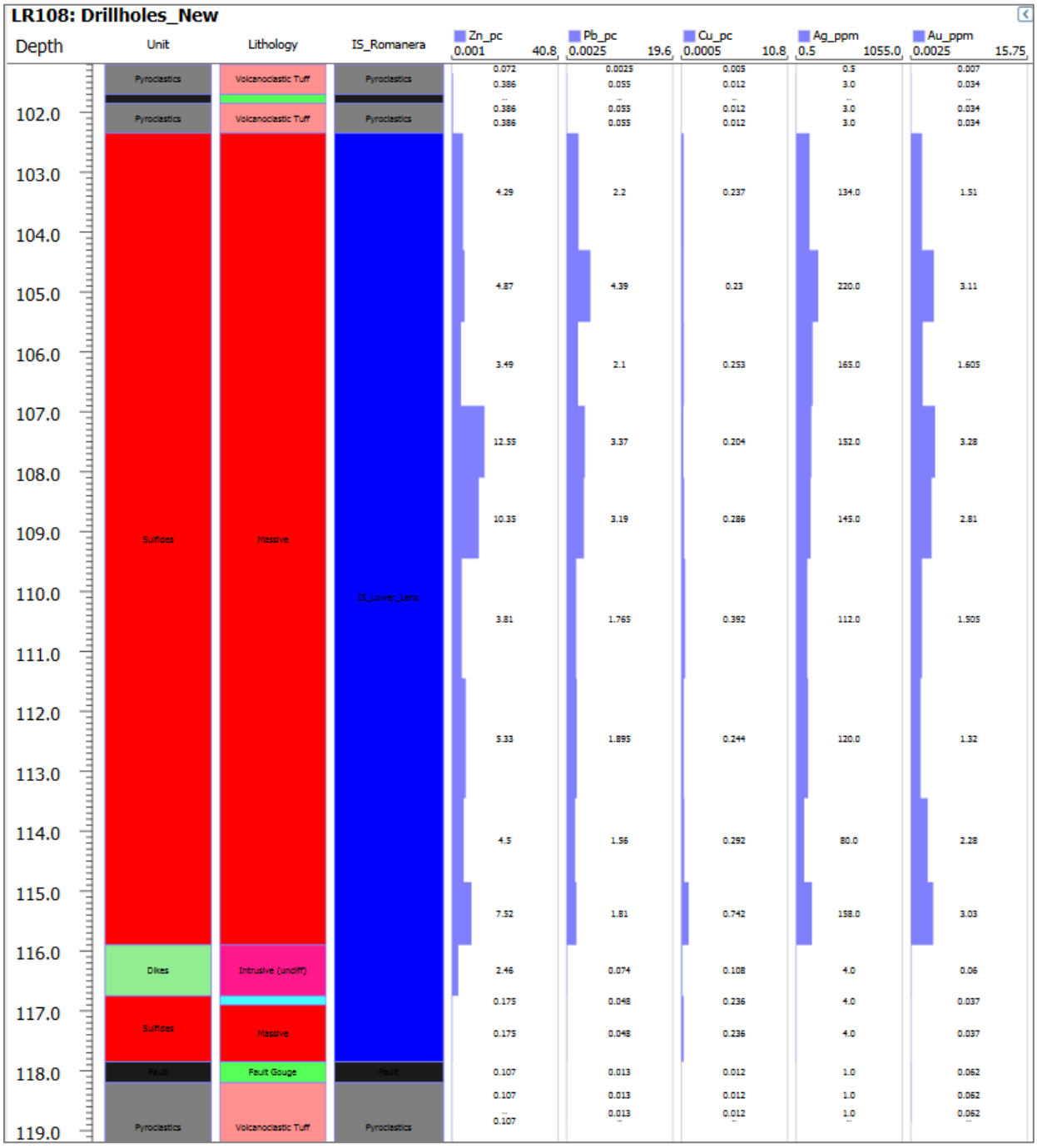
The geological interpretation used in the MRE was primarily informed by drillhole data. Emerita geologists used the Leapfrog Geo drillhole correlation tool to select sample intervals belonging to each sulphide lens based on lithology, mineralisation type, and assay grade (e.g. Figure 14-1). SLR developed wireframe boundary cut-off grades for each economic metal via inspection of log histograms and plots of average intercept length and grade with increasing cut-off. These nominal grade thresholds were used to audit and make minor adjustments to the first-pass interval selections, in order to optimise the inclusion of mineralised samples and the exclusion of unmineralized samples at lens margins.

The modelled sulphide lenses were used as domain wireframes in resource modelling. Low-grade (LG) envelopes were constructed to capture any sample grades above background in the volcanosedimentary wallrocks, enabling estimation of the grade of external waste for dilution modelling.

Each mineralised domain was modelled implicitly from interval selections using the Leapfrog Geo vein modelling tool. Wireframe contacts were snapped to sample boundaries. Drillhole samples were coded by domain prior to further statistical analysis and data processing.

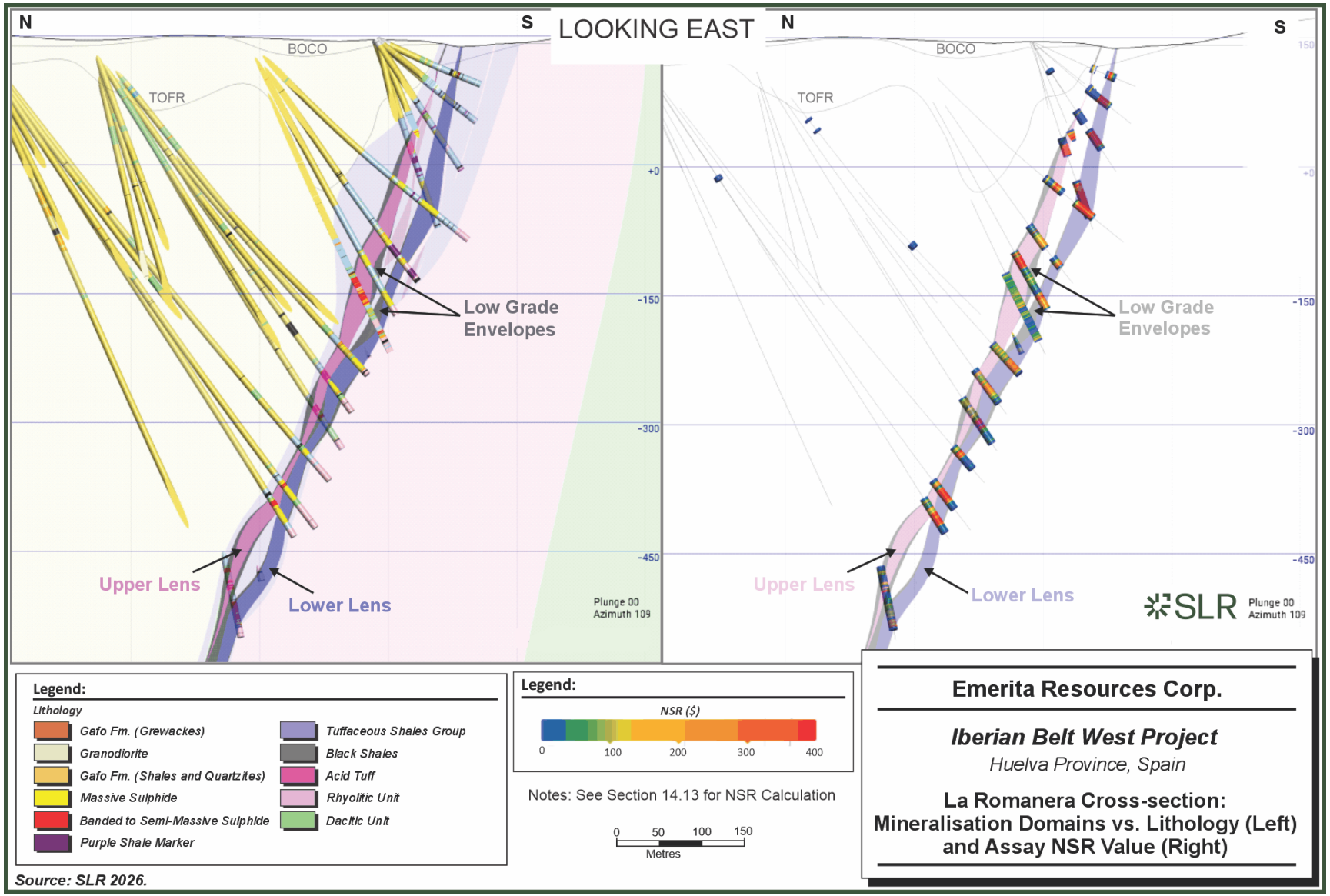
Cross-section and isometric views showing the mineralisation models for each deposit are provided in Figure 14-2 to Figure 14-7. The sample NSR values presented are based on the NSR calculation used in MRE reporting. They are provided for visual review only and have not been used in the domaining workflow.

Figure 14-1: Example of Interval Selection (IS_Romanera) Using Leapfrog Drillhole Correlation Tool



Source: Emerita 2023.

Figure 14-2: La Romanera Cross-section: Mineralisation Domains vs. Lithology (Left) and Assay NSR Value (Right)



Source: SLR 2026.

Figure 14-3: 3D View of La Romanera Mineralisation Domains and Input Interval Selections (Excluding LG Envelopes)

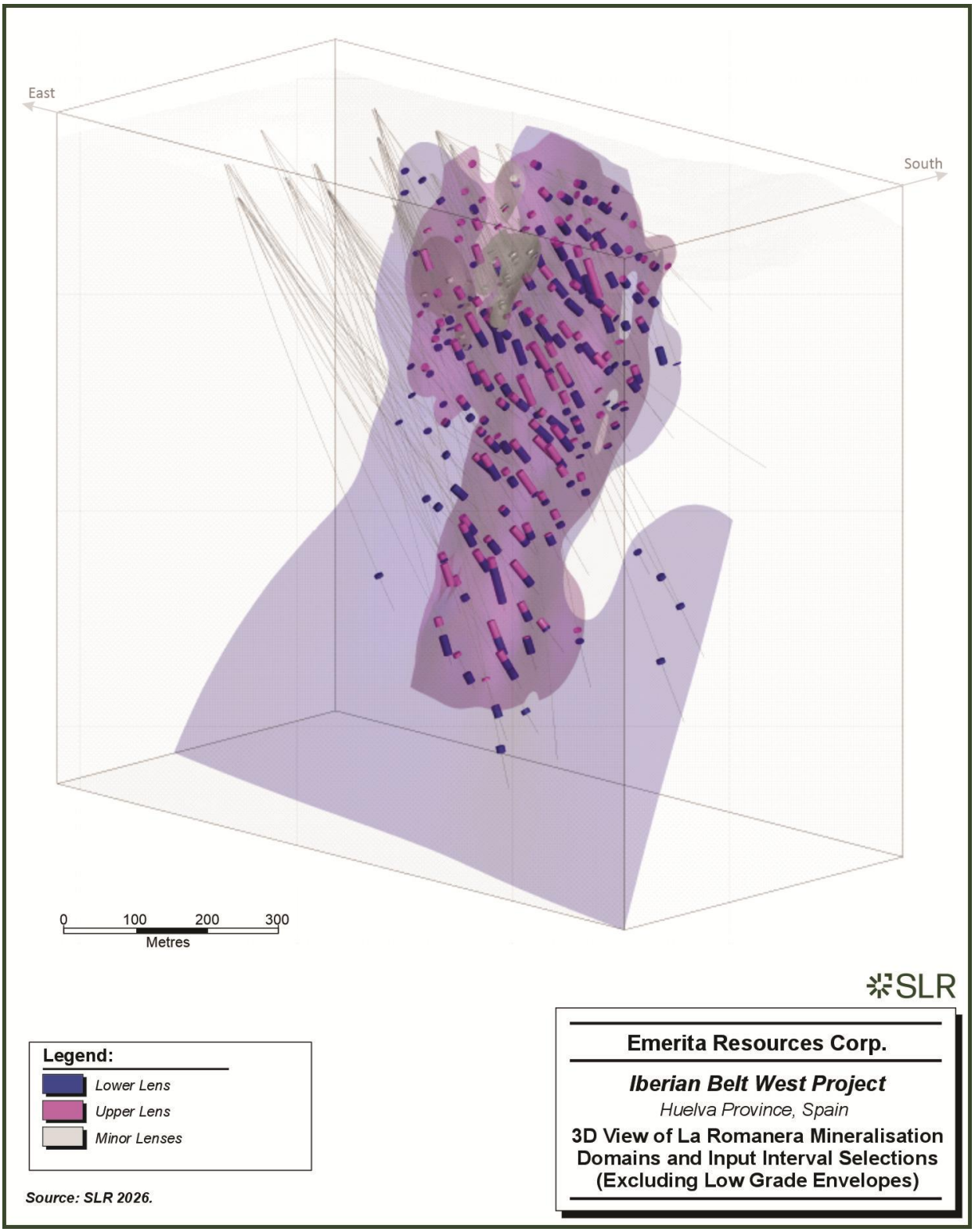
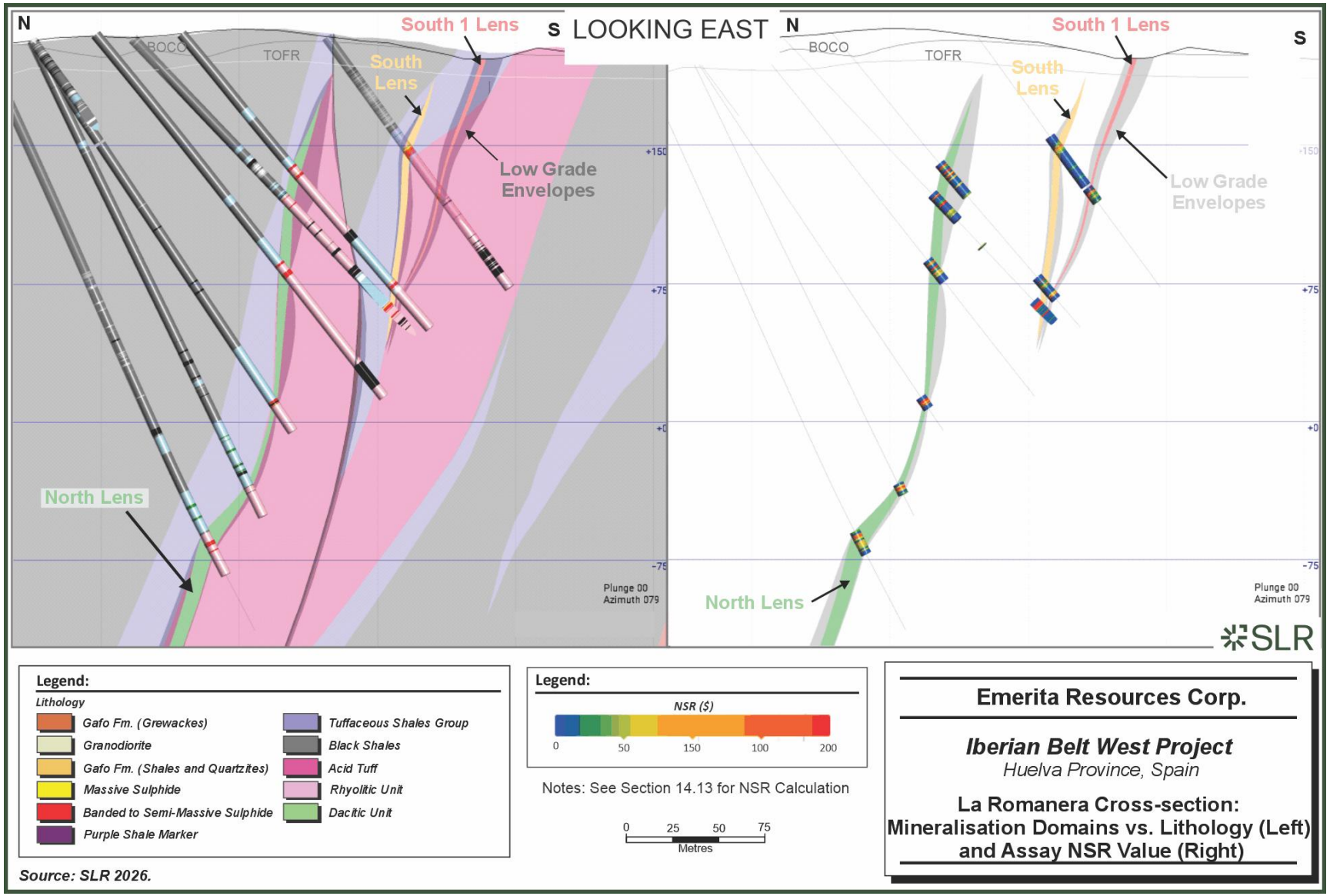


Figure 14-4: La Infanta Cross-section: Mineralisation Domains vs. Lithology (Left) and Assay NSR Value (Right)



Source: SLR 2026.

Figure 14-5: 3D View of La Infanta Domain Wireframes and Input Interval Selections (Excluding LG Envelopes)

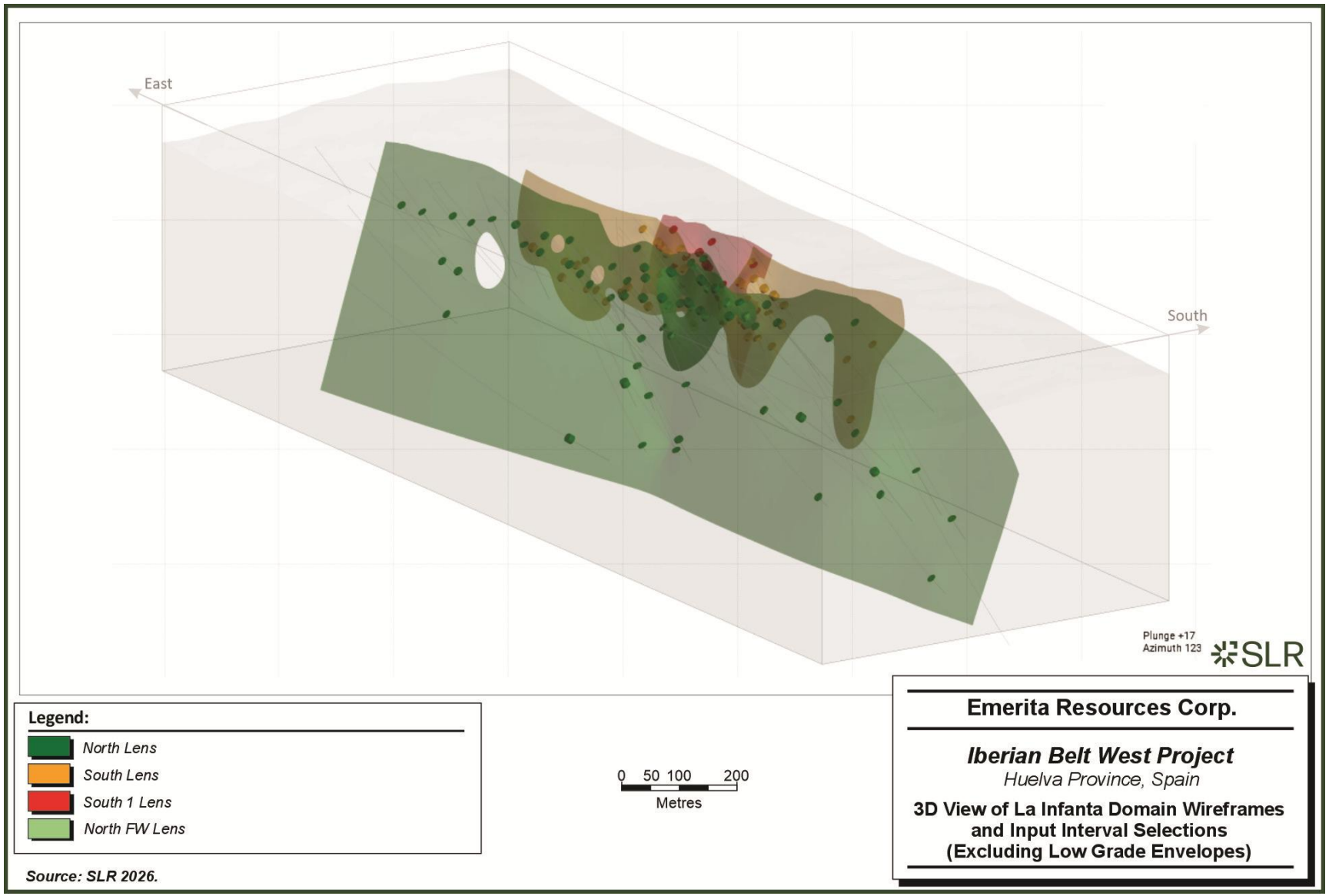


Figure 14-6: El Cura Cross-section: Mineralisation Domains vs. Lithology (Left) and Assay NSR Value (Right)

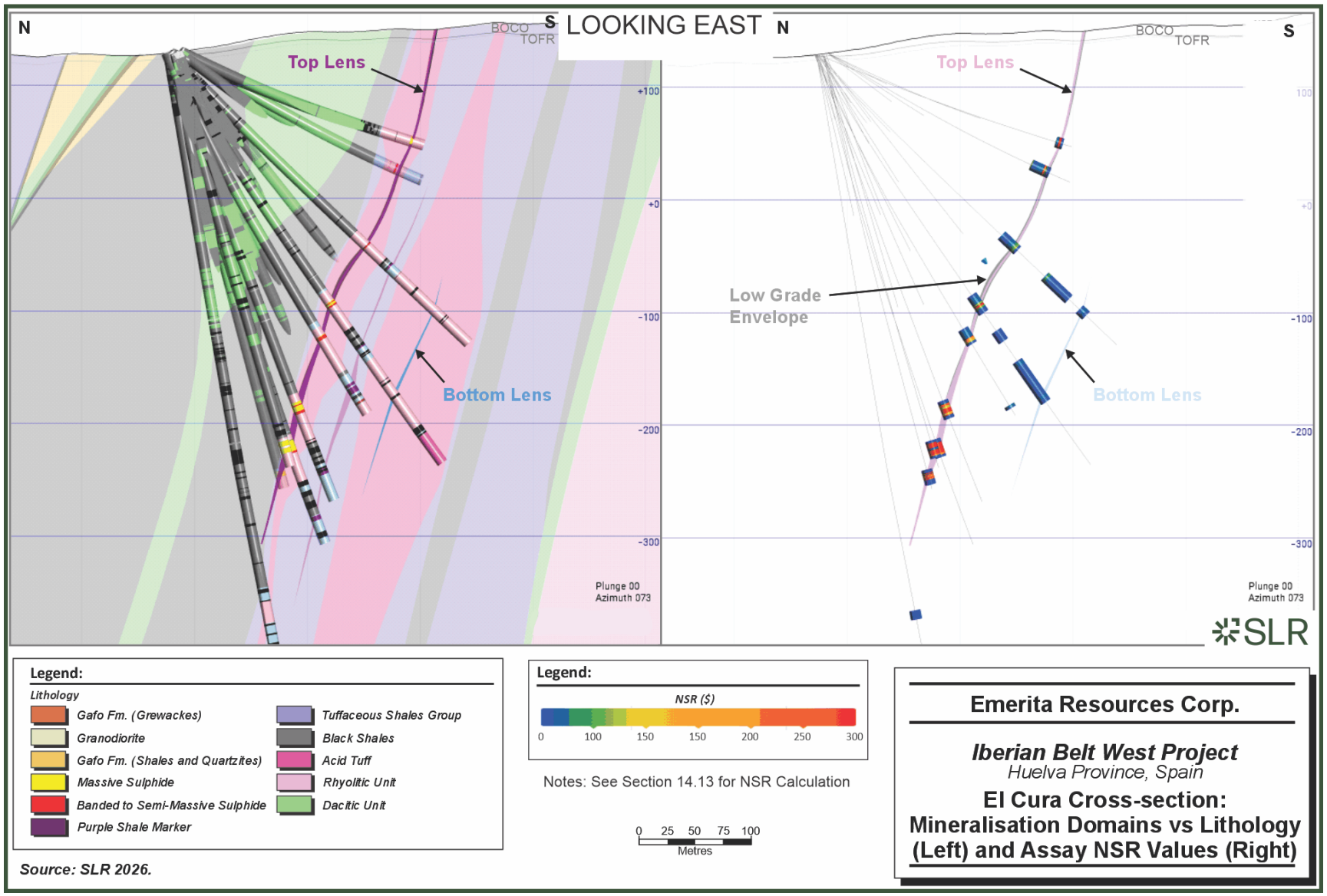
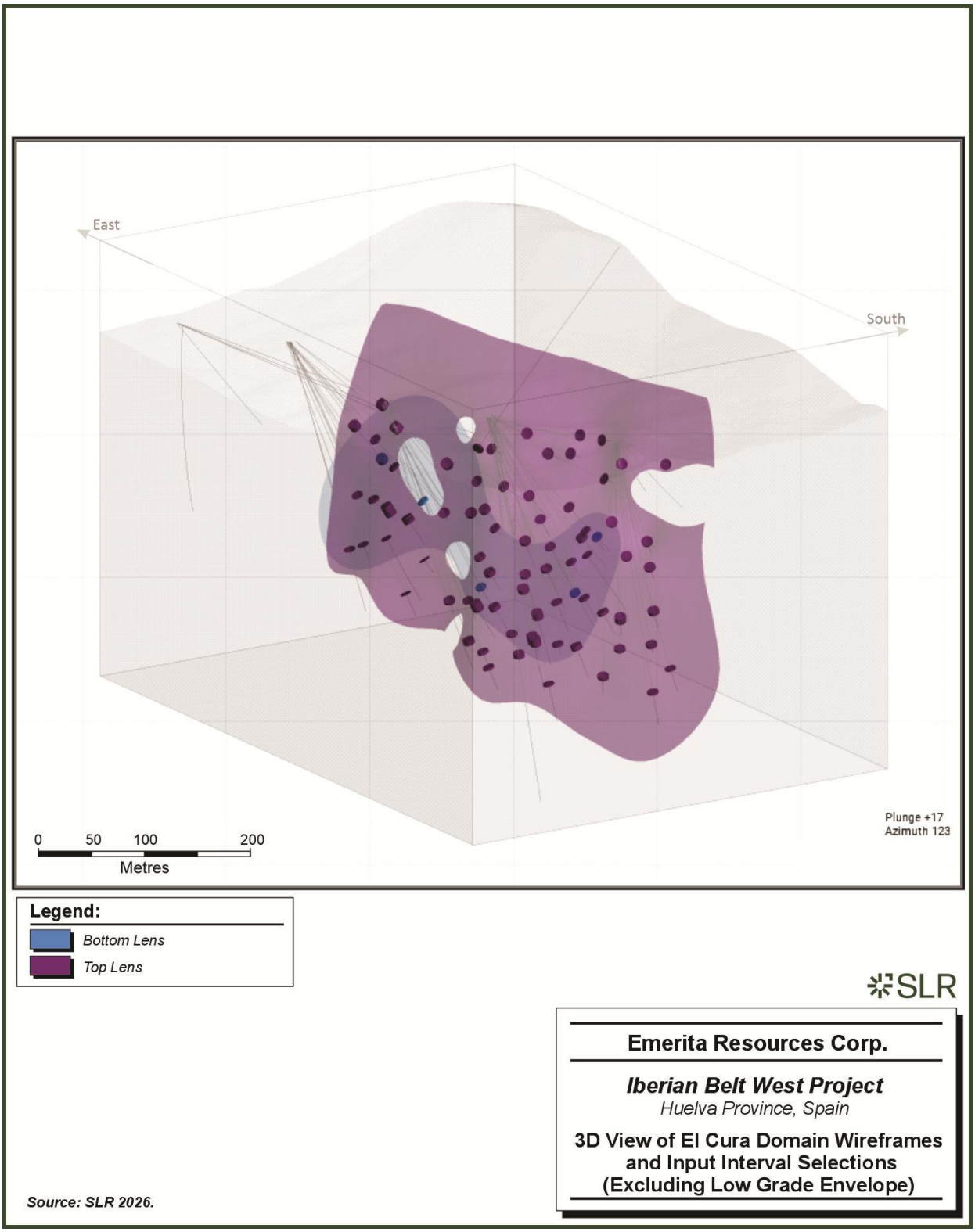


Figure 14-7: 3D View of El Cura Domain Wireframes and Input Interval Selections (Excluding LG Envelope)

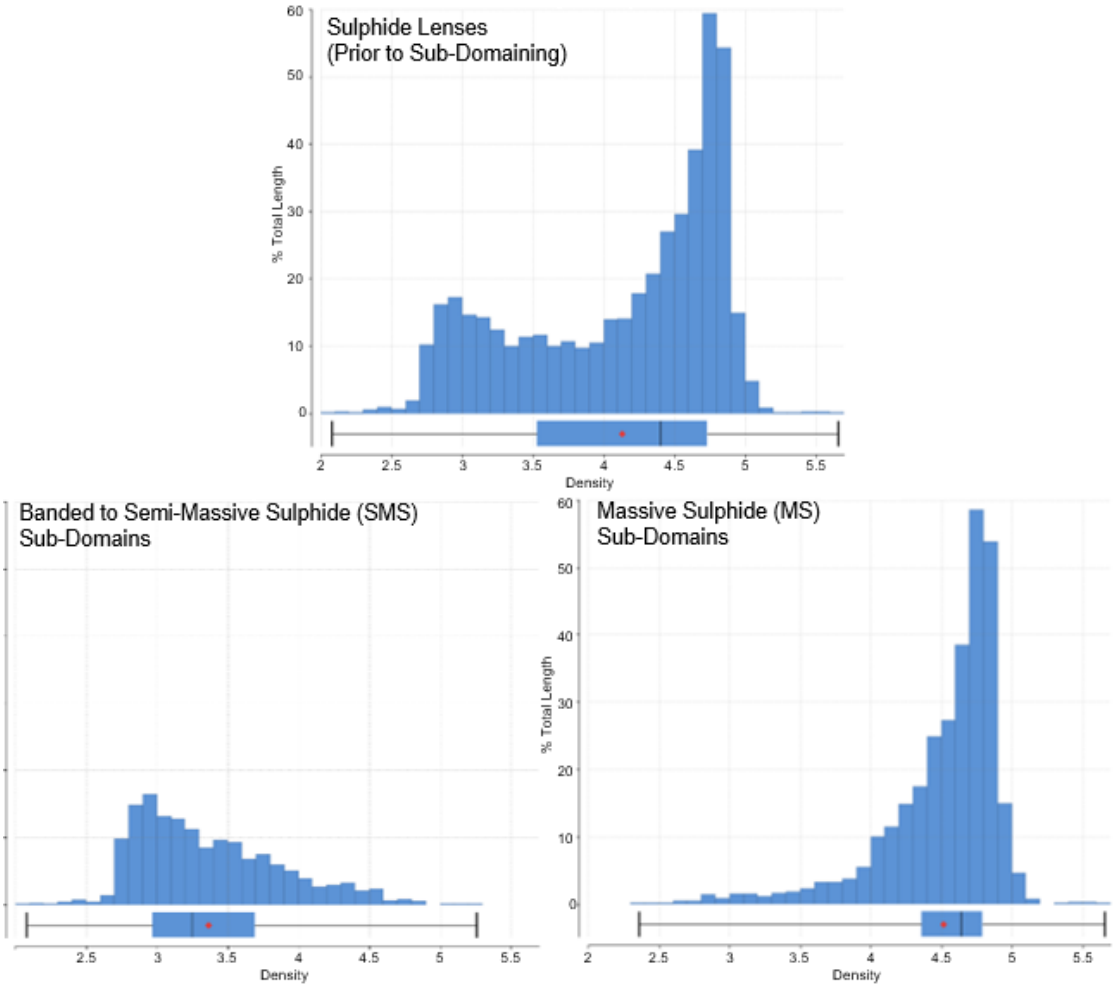


14.3.2 Mineralisation Style

La Romanera and El Cura are dominated by massive sulphide (MS) mineralisation, with lesser amounts of banded to semi-massive sulphide (SMS) occurring at domain margins. Sulphide content is typically lower at La Infanta, with banded to semi-massive sulphide the dominant mineralisation style.

At La Romanera, internal variability in mineralisation style results in bimodal distributions for density and sulphur in domain sample histograms. Sulphide lens width and the internal spatial continuity of non-massive sulphide intersections are sufficient to construct mineralisation style sub-domains. The impact of sub-domaining on the La Romanera density sample histogram is outlined in Figure 14-8.

Figure 14-8: La Romanera Density Sample Histograms



Source: SLR 2026.

The La Romanera mineralisation style sub-domains are shown in Figure 14-9 and were used to constrain density and sulphur estimation. Mineralisation style does not strongly control metal association or grade variability for base and precious metals, demonstrated by the overlap between massive (yellow) and banded to semi-massive (red) sulphide samples in the Cu-Zn scatter plot in Figure 14-10. The mineralisation style sub-domains have not been used in grade estimation for base and precious metals at La Romanera.

Figure 14-9: La Romanera Cross-section: Mineralisation Style Domains vs. Lithology (Left) and Sulphur (Right)

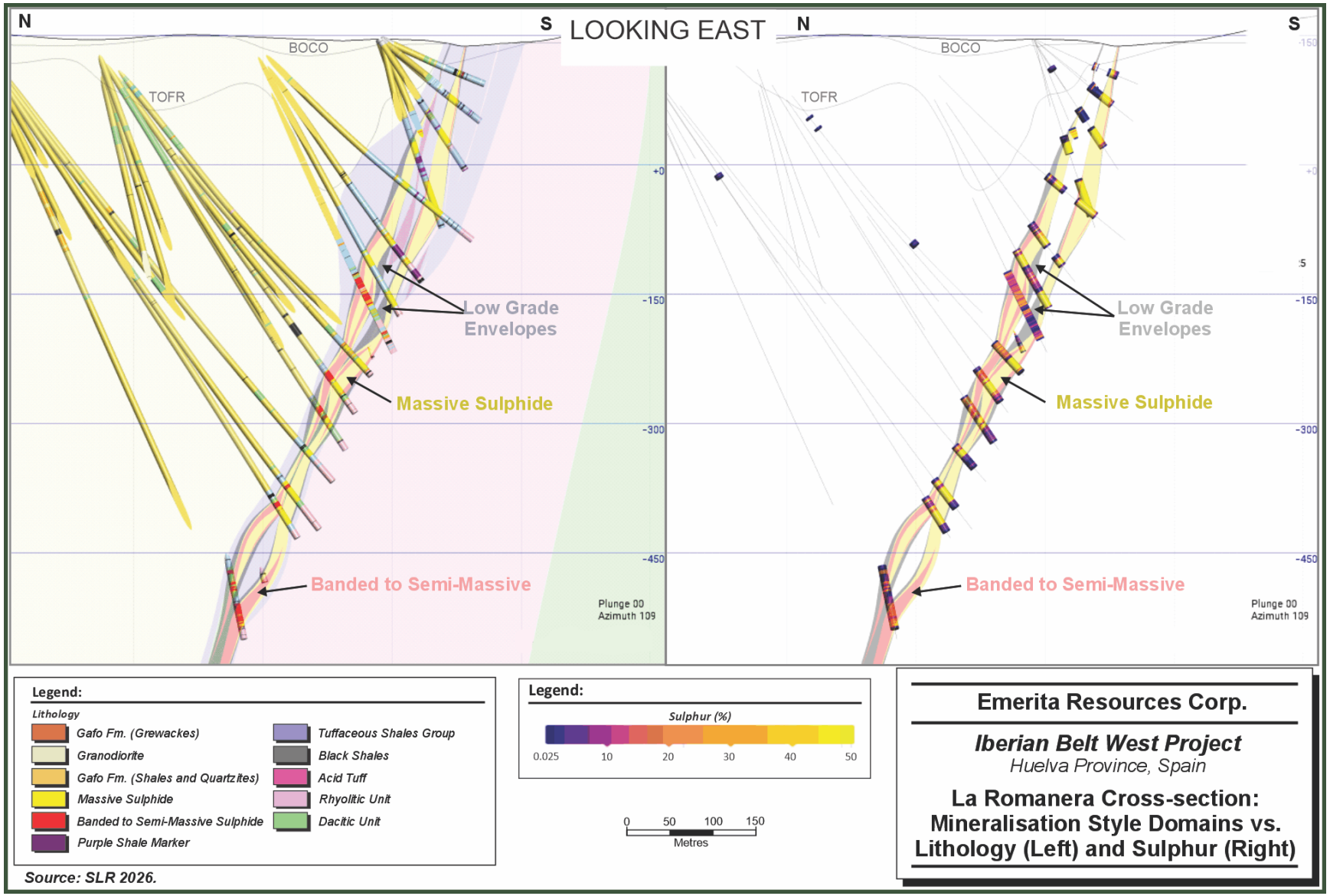
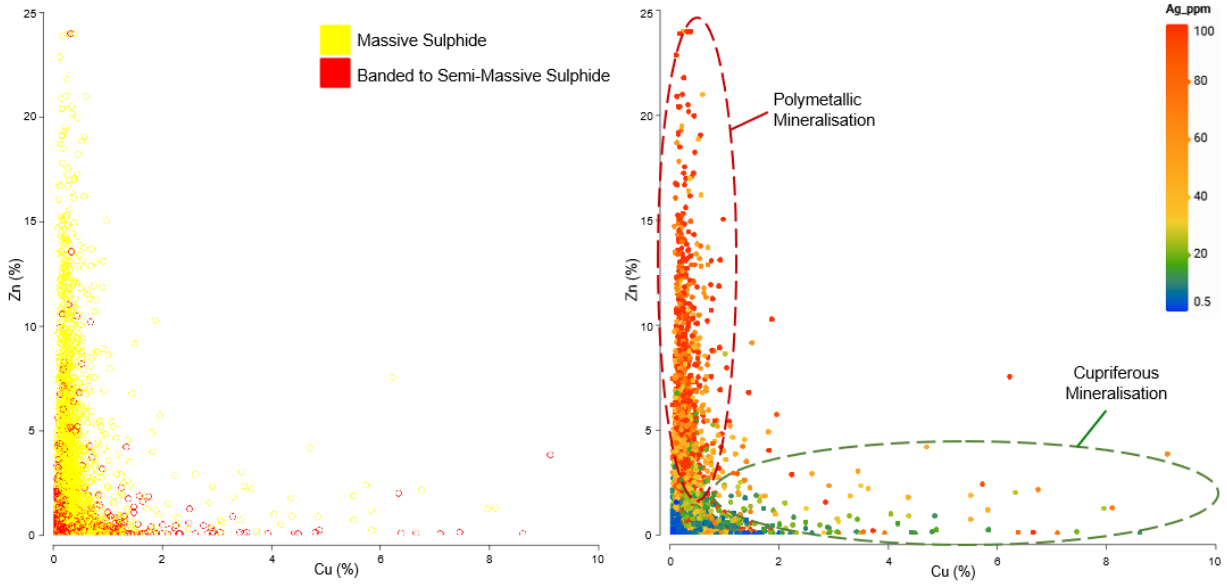


Figure 14-10 highlights two distinct metal associations at La Romanera: (1) High Zn-(Pb-Ag-Au) / low Cu 'polymetallic mineralisation' dominant, and (2) More localised regions of low Zn-(Pb-Ag-Au) / high Cu 'cupriferous mineralisation'. The spatial distribution and boundaries between the different mineralisation types within the sulphide lenses are complex and gradational. Internal variation in grade and metal association has been represented in the block model by interpolation, with mineralisation type subsequently evaluated at the stope scale to consider the impact of mining selectivity and planned dilution.

Figure 14-10: La Romanera Cu-Zn Sample Scatter Plots Coloured by Mineralisation Style (Left) and Ag Grade (Right)



Source: SLR 2026.

14.3.3 Weathering

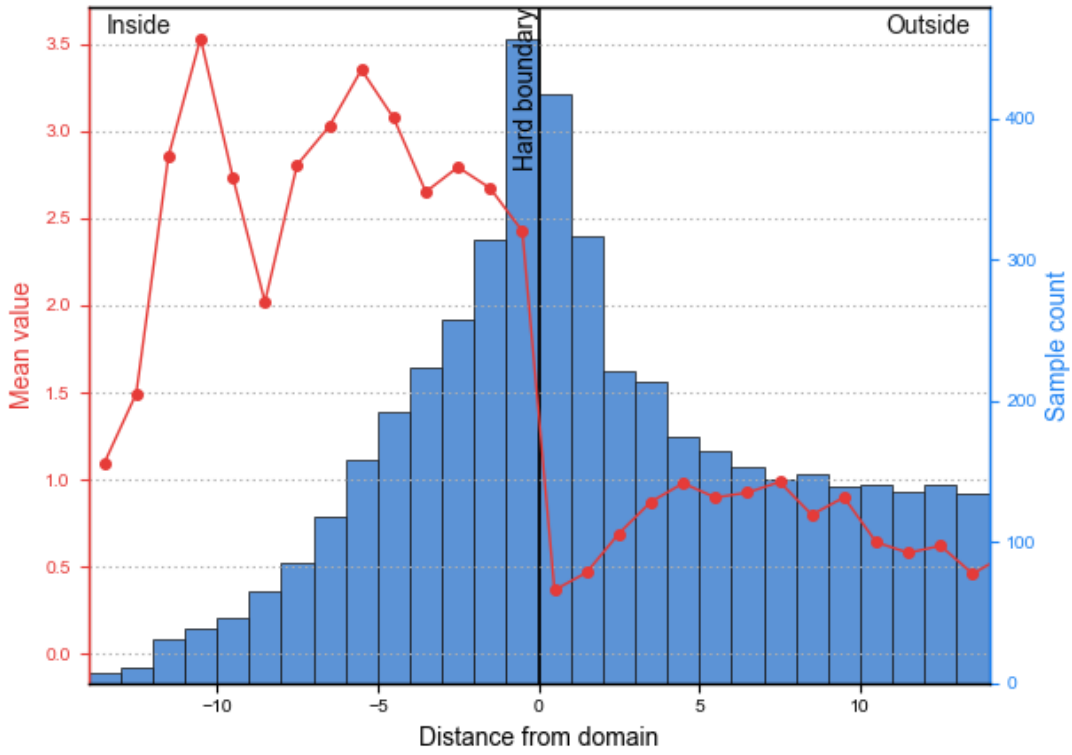
Weathering surfaces were constructed implicitly as Leapfrog Geo erosional and deposit surfaces from core logging observations, and used to split the mineralised domains into oxide, transition, and primary sulphide zones. Weathering surfaces are included in the cross-sections for each deposit shown in Figure 14-2, Figure 14-4 and Figure 14-6. There is limited drilling within the oxide and transition zones. Only the primary sulphide portion of each domain was used in grade estimation.

The QP considers all domains used in the MRE to be based on extensive geological knowledge and representative of the geology present at the deposits.

14.4 Boundary Analysis

Boundary analysis measures the rate of grade change across the contact between two domains. Plots for all metals and domains show a sharp step change consistent with hard boundary conditions. An example of boundary analysis for Zn across the La Romanera Lower Lens domain boundary is provided in Figure 14-11.

Figure 14-11: Zn Boundary Analysis for the La Romanera Lower Lens



Source: SLR 2026.

14.5 Compositing

Sample coverage and sample length are the same for each metal. Downhole compositing of assay samples was completed to avoid bias introduced when interpolating grade from samples of varying length. A 1 m downhole composite length was chosen for all deposits, in line with the modal assay sample length. Residual lengths below half the target composite length were added to the adjacent composite. Assay compositing was length and density weighted, and samples were not composited across mineralised domain boundaries.

Density is sampled over shorter 10 cm to 20 cm lengths. Density was first composited to the assay sample intervals. In the minority of cases where no density sample had been collected over an assay interval, a sulphur-density regression was used to derive a density value. This complete density dataset was then composited to 1 m lengths in line with the assay compositing procedure.

An example sulphur-density scatter plot for La Romanera is provided in Figure 14-12, whilst details of the sulphur-density regressions applied to each deposit are listed in Table 14-2.

Figure 14-12: Sulphur Density Scatter Plot and Regression (Red Line and Equation) for La Romanera

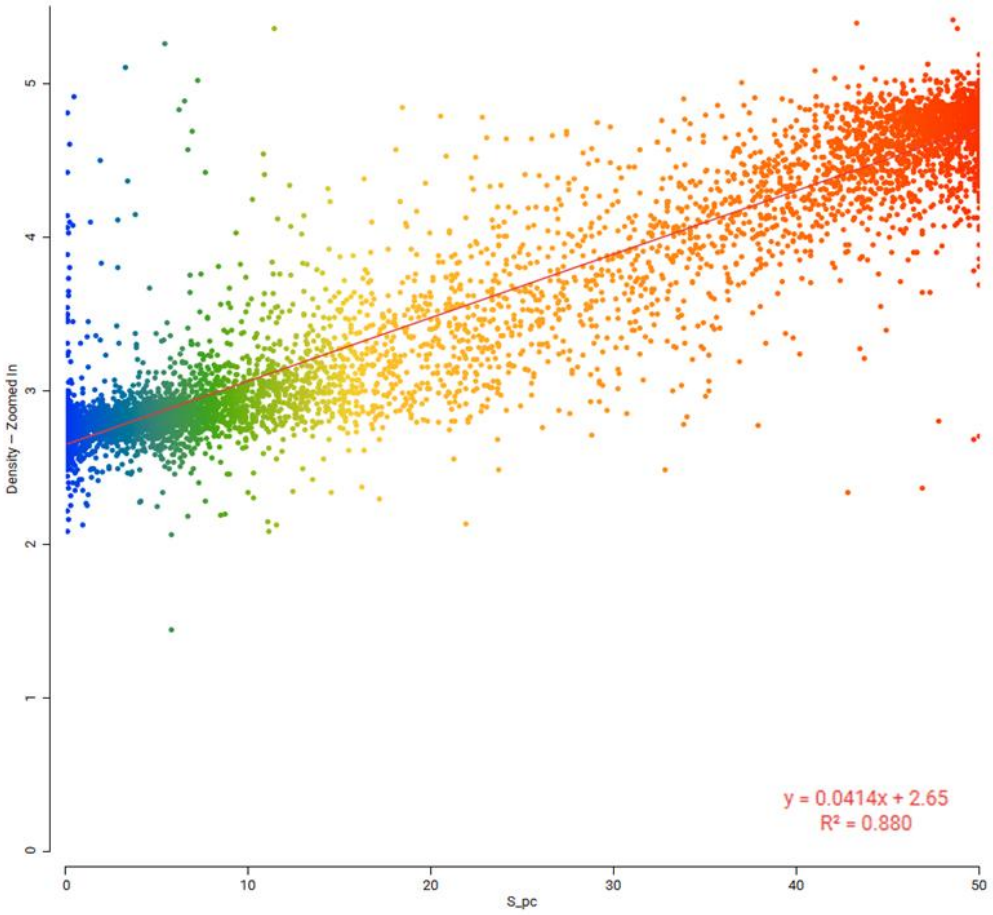


Table 14-2: Sulphur-Density Regressions per Deposit

Deposit	Sulphur-Density Regression	Density Sample Statistics		Density Sample Statistics after Regression		Regression-Based Density Values	
		Count	Mean (g/cm³)	Count	Mean (g/cm³)	Count	% of Dataset
La Romanera	[S_pc]*0.0414+2.65	6153	3.50	6798	3.51	645	9
La Infanta	[S_pc]*0.0535+2.59	1973	2.77	2264	2.77	291	13
El Cura	[S_pc]*0.039+2.53	1263	2.94	1782	2.89	519	29

14.6 Grade Capping

Capping was applied to isolated outlier values prior to variography and estimation. The outlier values are not considered to be representative of the general grade population and capping mitigates their impact on block estimation. The presence of outliers was assessed on a domain-by-domain basis using histograms, disintegration analysis, and statistical analysis of the composites. A summary of the grade capping thresholds and impact is shown in Table 14-3, Table 14-4 and Table 14-5 for each of the deposits.

Table 14-3: La Romanera Composite Capping Statistics by Domain

Domain	Metal	No. Comp.	No. Capped	% Capped	Raw Stats			Capped Stats		
					Max	Mean	CV	Max (Cap)	Mean	CV
Lower	Zn (%)	1836	15	0.8	39.14	2.75	1.40	18.00	2.71	1.32
	Pb (%)	1836	4	0.2	16.90	1.18	1.34	11.00	1.18	1.29
	Cu (%)	1836	12	0.7	7.32	0.47	1.37	4.20	0.46	1.23
	Ag (ppm)	1836	13	0.7	914	60	1.31	490	59	1.19
	Au (ppm)	1836	9	0.5	15.50	1.32	1.24	10.30	1.32	1.21
Lower MS	S (%)	1288	0	0	50.0	45.5	0.12	No Capping		
Lower SMS	S (%)	548	0	0	50.0	20.4	0.49	No Capping		
Upper	Zn (%)	1409	11	0.8	24.00	1.96	1.68	15.60	1.94	1.63
	Pb (%)	1409	3	0.2	11.17	0.99	1.44	8.10	0.99	1.43
	Cu (%)	1409	5	0.4	16.62	0.39	1.67	4.00	0.37	1.08
	Ag (ppm)	1409	6	0.4	471	56	1.10	320	56	1.08
	Au (ppm)	1409	11	0.8	10.92	1.00	1.18	6.00	0.98	1.09
Upper MS	S (%)	961	0	0	50.0	43.4	0.19	No Capping		
Upper SMS	S (%)	448	0	0	43.0	17.5	0.52	No Capping		
Lower HW1	Zn (%)	21	0	0	4.16	1.78	0.65	No Capping		
	Pb (%)	21	0	0	1.72	0.65	0.82	No Capping		
	Cu (%)	21	0	0	0.15	0.06	0.79	No Capping		
	Ag (ppm)	21	0	0	57	19	0.89	No Capping		
	Au (ppm)	21	0	0	2.20	0.74	1.01	No Capping		
	S (%)	21	0	0	44.1	21.9	0.68	No Capping		
Upper HW1	Zn (%)	12	0	0	8.90	2.56	1.08	No Capping		
	Pb (%)	12	0	0	5.06	1.66	1.01	No Capping		
	Cu (%)	12	0	0	0.63	0.35	0.46	No Capping		
	Ag (ppm)	12	0	0	154	63	0.80	No Capping		
	Au (ppm)	12	0	0	3.37	1.30	0.83	No Capping		
	S (%)	12	0	0	44.9	35.3	0.25	No Capping		

Domain	Metal	No. Comp.	No. Capped	% Capped	Raw Stats			Capped Stats		
					Max	Mean	CV	Max (Cap)	Mean	CV
Upper HW2	Zn (%)	6	0	0	13.00	4.62	0.86	No Capping		
	Pb (%)	6	0	0	5.25	2.42	0.70	No Capping		
	Cu (%)	6	0	0	0.75	0.37	0.67	No Capping		
	Ag (ppm)	6	0	0	213	114	0.69	No Capping		
	Au (ppm)	6	0	0	5.26	1.98	0.94	No Capping		
	S (%)	6	0	0	46.4	33.0	0.41	No Capping		
Upper HW3	Zn (%)	7	0	0	16.67	4.87	1.51	No Capping		
	Pb (%)	7	0	0	7.07	2.18	1.38	No Capping		
	Cu (%)	7	0	0	1.72	0.43	1.24	No Capping		
	Ag (ppm)	7	0	0	225	89	0.98	No Capping		
	Au (ppm)	7	0	0	1.03	0.72	0.38	No Capping		
	S (%)	7	0	0	43.3	34.4	0.24	No Capping		
Lower LG	Zn (%)	465	4	0.9	6.70	0.24	1.69	1.50	0.23	1.22
	Pb (%)	465	3	0.6	3.50	0.11	2.19	1.25	0.10	1.51
	Cu (%)	465	2	0.4	0.95	0.09	1.22	0.60	0.09	1.18
	Ag (ppm)	465	6	1.3	125.00	4.74	1.79	32.00	4.37	1.27
	Au (ppm)	465	4	0.9	2.75	0.13	1.37	0.70	0.12	1.00
	S (%)	465	0	0	44.9	8.5	0.79	No Capping		
Upper LG	Zn (%)	566	6	1.1	4.49	0.17	1.68	1.40	0.17	1.34
	Pb (%)	566	3	0.5	3.65	0.11	2.06	1.10	0.10	1.54
	Cu (%)	566	5	0.9	1.06	0.12	1.17	0.60	0.12	1.09
	Ag (ppm)	566	5	0.9	174.96	5.82	1.88	45.00	5.41	1.28
	Au (ppm)	566	0	0.0	0.94	0.16	0.94	0.94	0.16	0.94
	S (%)	566	0	0	44.8	8.9	0.78	No Capping		

Table 14-4: La Infanta Composite Capping Statistics by Domain

Domain	Metal	No. Comp.	No. Capped	% Capped	Raw Stats			Capped Stats		
					Max	Mean	CV	Max (Cap)	Mean	CV
North	Zn (%)	259	6	2.3	36.90	3.72	1.33	15.40	3.51	1.17
	Pb (%)	259	4	1.5	19.99	2.15	1.34	11.40	2.09	1.25
	Cu (%)	259	2	0.8	4.00	0.51	1.39	3.00	0.50	1.35
	Ag (ppm)	259	3	1.2	526.00	53.74	1.66	394.00	52.72	1.60
	Au (ppm)	259	0	0.0	2.47	0.31	1.21	No Capping		
	S (%)	259	0	0	27.3	6.1	0.71	No Capping		
South	Zn (%)	173	13	7.5	34.00	7.50	1.28	29.50	7.33	1.26
	Pb (%)	173	5	2.9	22.03	4.19	1.26	17.00	4.14	1.24
	Cu (%)	173	0	0.0	4.61	1.08	1.19	No Capping		
	Ag (ppm)	173	2	1.2	497.72	93.83	1.26	402.00	92.96	1.25
	Au (ppm)	173	0	0.0	1.92	0.33	0.99	No Capping		
	S (%)	173	0	0	28.2	8.4	0.87	No Capping		
South 1	Zn (%)	59	9	15.3	40.80	10.41	1.13	27.10	9.49	1.05
	Pb (%)	59	9	15.3	21.28	6.11	1.09	15.90	5.73	1.03
	Cu (%)	59	6	10.2	5.97	1.37	1.17	3.70	1.25	1.08
	Ag (ppm)	59	4	6.8	724.00	108.71	1.44	356.00	91.82	1.14
	Au (ppm)	59	0	0.0	2.30	0.40	1.06	No Capping		
	S (%)	59	0	0	27.9	10.3	0.79	No Capping		
North FW1	Zn (%)	52	0	0.0	6.60	1.63	0.78	No Capping		
	Pb (%)	52	0	0.0	6.75	1.20	1.03	No Capping		
	Cu (%)	52	0	0.0	0.19	0.04	1.15	No Capping		
	Ag (ppm)	52	0	0.0	18.00	5.05	0.84	No Capping		
	Au (ppm)	52	0	0.0	0.38	0.09	0.72	No Capping		
	S (%)	52	0	0	5.9	3.1	0.33	No Capping		
North LG	Zn (%)	445	2	0.4	10.26	0.42	1.67	2.60	0.40	1.29
	Pb (%)	445	0	0.0	5.23	0.30	1.57	No Capping		
	Cu (%)	445	2	0.4	1.62	0.04	2.79	0.75	0.04	2.17
	Ag (ppm)	445	4	0.9	243.52	5.92	2.58	56.00	5.26	1.64
	Au (ppm)	445	1	0.2	2.02	0.12	1.31	1.05	0.12	1.17
	S (%)	445	0	0	18.7	2.7	0.62	No Capping		

Domain	Metal	No. Comp.	No. Capped	% Capped	Raw Stats			Capped Stats		
					Max	Mean	CV	Max (Cap)	Mean	CV
South LG	Zn (%)	103	2	1.9	4.63	0.61	1.26	3.00	0.58	1.07
	Pb (%)	103	0	0.0	2.35	0.33	1.20	No Capping		
	Cu (%)	103	1	1.0	1.07	0.05	2.47	0.50	0.04	1.61
	Ag (ppm)	103	0	0.0	39.00	4.11	1.53	No Capping		
	Au (ppm)	103	0	0.0	0.60	0.08	1.51	No Capping		
	S (%)	103	0	0	8.9	2.4	0.55	No Capping		
South 1 LG	Zn (%)	209	2	1.0	18.58	0.53	3.05	4.00	0.41	1.57
	Pb (%)	209	1	0.5	8.36	0.28	2.44	3.70	0.26	1.78
	Cu (%)	209	1	0.5	2.98	0.07	3.20	0.80	0.06	1.72
	Ag (ppm)	209	2	1.0	242.09	5.90	3.25	50.00	4.55	1.31
	Au (ppm)	209	2	1.0	1.61	0.12	1.54	0.70	0.11	1.19
	S (%)	209	0	0	18.2	3.2	0.82	No Capping		

Table 14-5: El Cura Composite Capping Statistics by Domain

Domain	Metal	No. Comp.	No. Capped	% Capped	Raw Stats			Capped Stats		
					Max	Mean	CV	Max (Cap)	Mean	CV
Top	Zn (%)	316	0	0.0	10.48	1.54	1.42	No Capping		
	Pb (%)	316	0	0.0	5.16	0.75	1.24	No Capping		
	Cu (%)	316	2	0.6	14.50	1.44	1.20	7.70	1.41	1.11
	Ag (ppm)	316	0	0.0	195	41	0.86	No Capping		
	Au (ppm)	316	2	0.6	10.73	1.34	0.99	7.70	1.32	0.92
	S (%)	316	0	0.0	50.0	32.5	0.44	No Capping		
Top LG	Zn (%)	80	2	2.5	3.78	0.21	2.80	0.80	0.13	1.44
	Pb (%)	80	2	2.5	2.11	0.09	3.41	0.30	0.05	1.42
	Cu (%)	80	3	3.8	0.75	0.07	1.74	0.20	0.05	1.08
	Ag (ppm)	80	3	3.8	22	3	1.29	13	3	1.03
	Au (ppm)	80	1	1.3	0.53	0.10	1.02	0.36	0.10	0.96
	S (%)	80	0	0.0	33.0	10.5	0.76	No Capping		

14.7 Metal Correlations

Correlation statistics were undertaken to identify relationships between estimated variables. Bivariate relationships are broadly consistent within a given deposit and have been reproduced in the block model by maintaining stable variogram and/or search orientations for correlated variables.

Correlation statistics for La Romanera and El Cura composites show moderate to strong positive correlations between all variables except for Cu (Table 14-6 and Table 14-8). Correlation statistics for La Infanta composites exhibit moderate to strong positive correlations between all variables (Table 14-7).

Table 14-6: Correlation Matrix for Metals and Density for La Romanera

	Zn	Pb	Cu	Ag	Au	S	Density
Zn	1.00	0.82	0.08	0.52	0.36	0.48	0.50
Pb	0.82	1.00	0.10	0.72	0.52	0.51	0.53
Cu	0.08	0.10	1.00	0.17	0.14	0.37	0.34
Ag	0.52	0.72	0.17	1.00	0.65	0.55	0.57
Au	0.36	0.52	0.14	0.65	1.00	0.54	0.55
S	0.48	0.51	0.37	0.55	0.54	1	0.95
Density	0.50	0.53	0.34	0.57	0.55	0.95	1.00

Table 14-7: Correlation Matrix for Metals and Density for La Infanta

	Zn	Pb	Cu	Ag	Au	S	Density
Zn	1.00	0.96	0.91	0.83	0.49	0.90	0.74
Pb	0.96	1.00	0.89	0.82	0.49	0.89	0.74
Cu	0.91	0.89	1.00	0.89	0.56	0.86	0.68
Ag	0.83	0.82	0.89	1.00	0.63	0.77	0.64
Au	0.49	0.49	0.56	0.63	1.00	0.57	0.44
S	0.90	0.89	0.86	0.77	0.57	1.00	0.74
Density	0.74	0.74	0.68	0.64	0.44	0.74	1.00

Table 14-8: Correlation Matrix for Metals and Density for El Cura

	Zn	Pb	Cu	Ag	Au	S	Density
Zn	1.00	0.88	0.24	0.60	0.47	0.26	0.28
Pb	0.88	1.00	0.30	0.66	0.49	0.30	0.32
Cu	0.24	0.30	1.00	0.62	0.57	0.47	0.42
Ag	0.60	0.66	0.62	1.00	0.62	0.49	0.49
Au	0.47	0.49	0.57	0.62	1.00	0.52	0.48
S	0.26	0.30	0.47	0.49	0.52	1.00	0.86
Density	0.28	0.32	0.42	0.49	0.48	0.86	1.00

14.8 Variography

Continuity analysis and variogram modelling were conducted using normal score transformed capped composites. For Zn, Pb, Cu, Ag, and Au, this included the Lower and Upper lenses at La Romanera, the North and South lenses at La Infanta, and the Top Lens at El Cura. For density, this included the Lower Lens MS and SMS sub-domains at La Romanera, the North and South Lenses at La Infanta and the Top Lens at El Cura. No variography has been completed for sulphur.

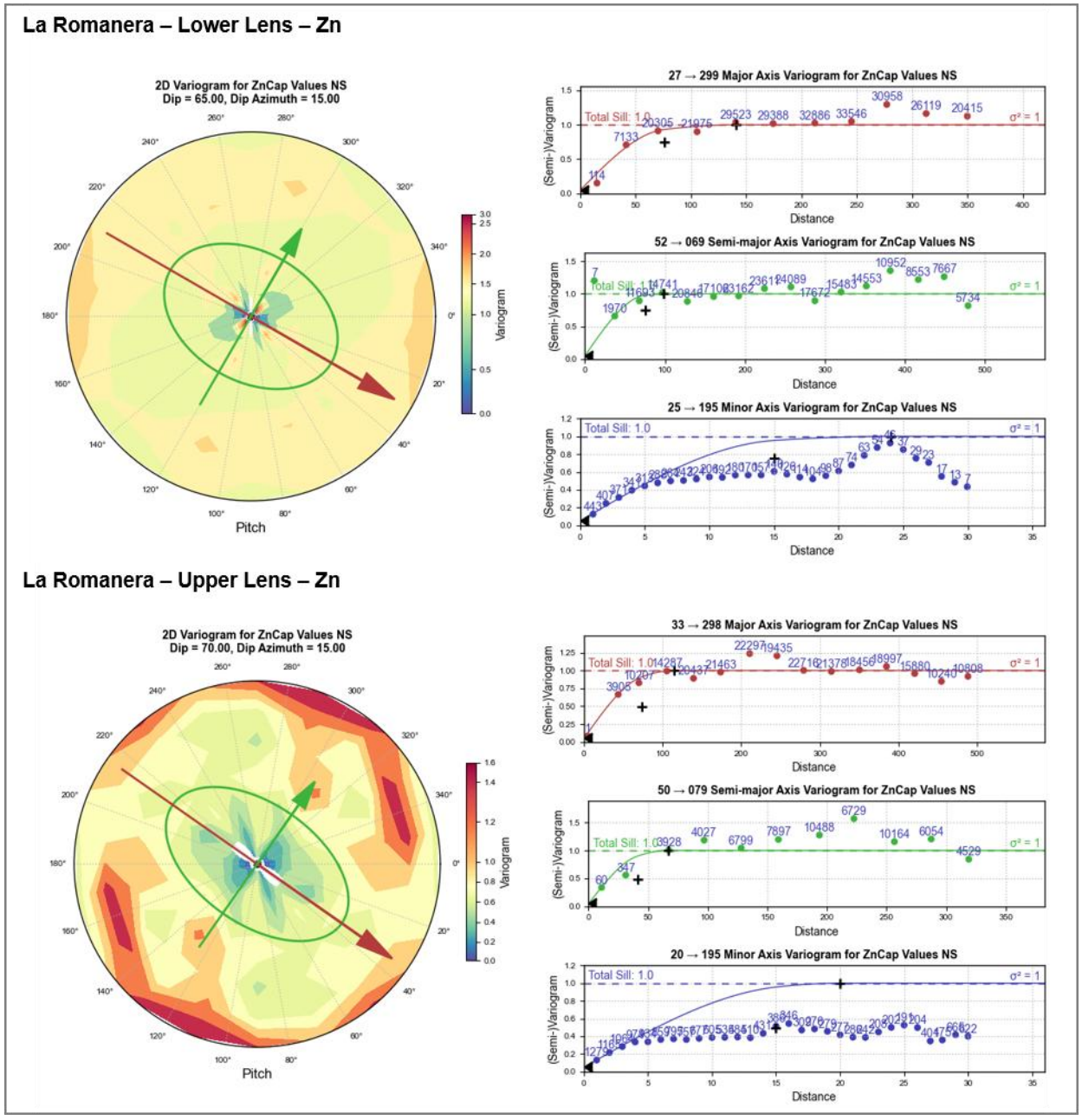
Continuity analysis was undertaken prior to variography to determine the major, semi-major, and minor axes of continuity based on spatial correlation between sample pairs. Down-dip continuity maps were aligned with the domain wireframes, then examined alongside their underlying variograms to determine the plunge of the major axis.

Directional variograms were created in the orientations defined by the continuity analysis. Nugget variances were derived from a downhole variogram. Variogram models typically consist of a nugget and two spherical structures.

Examples of the continuity analysis and modelled variograms are provided for La Romanera (Figure 14-13), La Infanta (Figure 14-14), and El Cura (Figure 14-15). Normal score variogram model parameters were back-transformed for use in estimation. The resulting model parameters for all variables are listed in Table 14-9, Table 14-10 and Table 14-11.

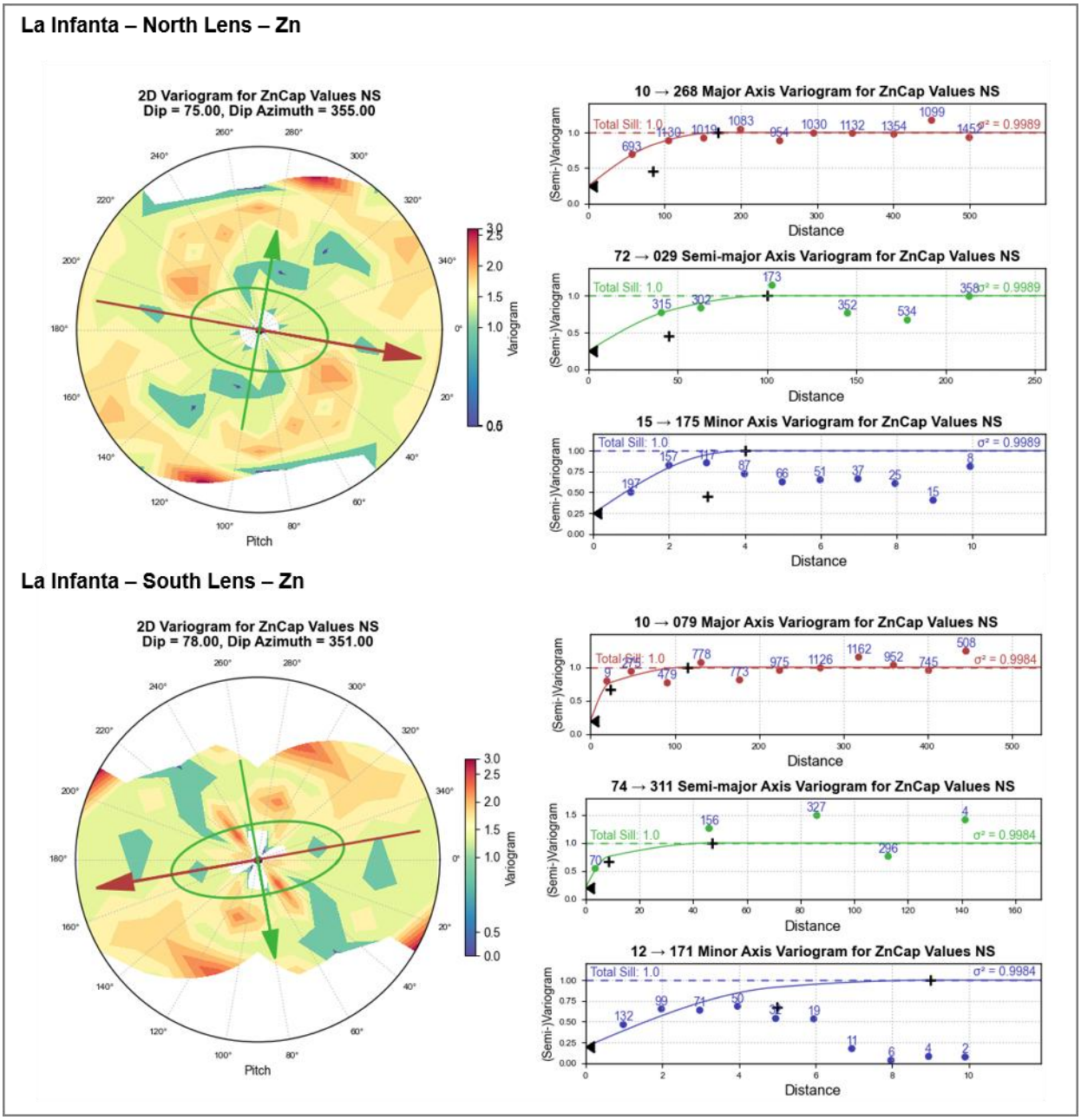
The QP considers the overall quality of the experimental variograms to be acceptable and are generally based on a significant number of composite pairs which have been appropriately domained. At La Romanera, confidence in the modelled variograms is high, with clearly defined continuity displayed by the experimental variograms. Variogram structure is less clear for La Infanta and El Cura, and confidence is therefore lower.

Figure 14-13: La Romanera - Zn Normal Score Down-Dip Continuity Maps and Directional Variograms



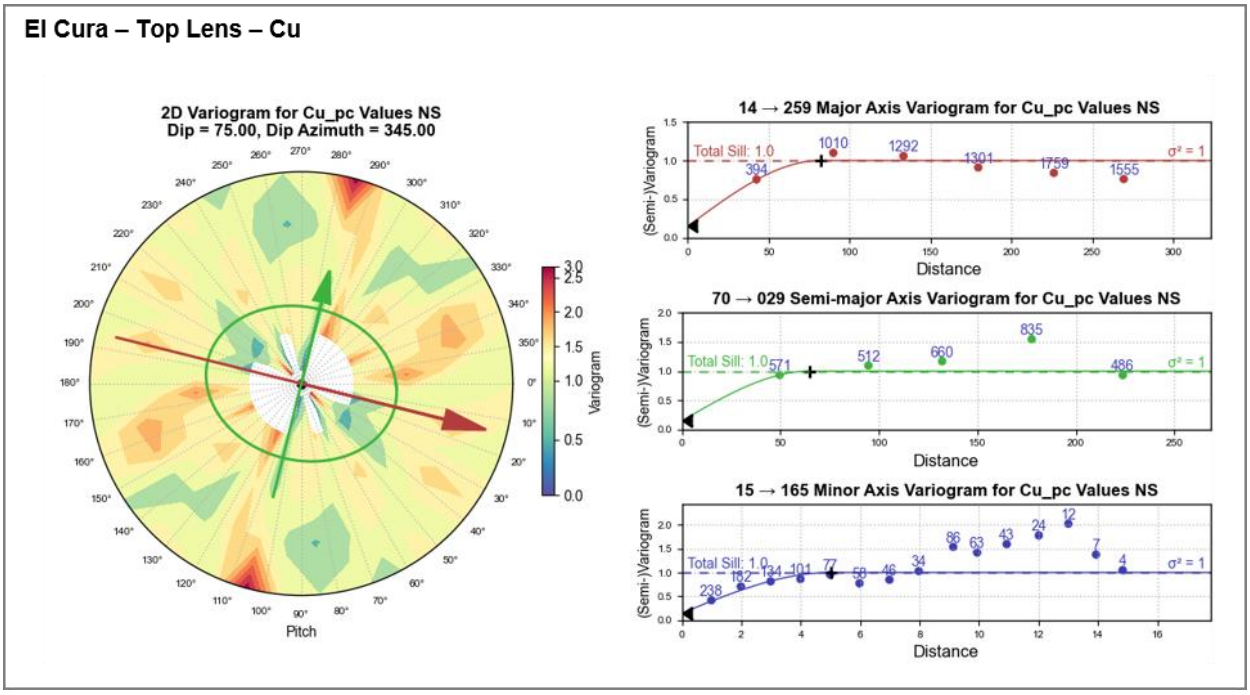
Source: SLR 2026.

Figure 14-14: La Infanta – Zn Normal Score Down-Dip Continuity Maps and Directional Variograms



Source: SLR 2026.

Figure 14-15: El Cura – Cu Normal Score Down-Dip Continuity Maps and Directional Variograms



Source: SLR 2026.

Table 14-9: La Romanera Variogram Model Parameters

Domain	Variable	Rotation (Degrees) (Dip/DipDir/Pitch)	Nugget Effect	Structure 1				Structure 2			
				Sill	Axis Distance (m)			Sill	Axis Distance (m)		
					Major	Semi-Major	Minor		Major	Semi-Major	Minor
Lower	Zn	65 / 15 / 30	0.07	0.74	76	75	15	0.19	141	98	24
	Pb	65 / 15 / 30	0.04	0.31	90	43	8	0.65	90	60	20
	Cu	65 / 15 / 30	0.14	0.56	77	70	4	0.3	121	70	25
	Ag	65 / 15 / 50	0.05	0.59	135	89	9	0.36	150	126	25
	Au	65 / 15 / 50	0.04	0.49	92	95	9	0.47	180	95	26
Lower MS	Density	65 / 15 / 25	0.18	0.37	50	70	2.2	0.45	87	70	19
Lower SMS	Density	65 / 15 / 25	0.21	0.52	56	64	2.8	0.27	150	95	16
Upper	Zn	70 / 15 / 35	0.07	0.58	74	41	15	0.35	115	67	20
	Pb	70 / 15 / 35	0.08	0.55	49	16	10	0.37	109	78	20
	Cu	70 / 15 / 50	0.17	0.29	91	58	3	0.54	91	60	15
	Ag	70 / 15 / 30	0.05	0.66	70	60	15	0.29	90	60	18
	Au	70 / 15 / 30	0.1	0.18	105	15	3	0.72	105	73	18

Table 14-10: La Infanta Variogram Model Parameters

Domain	Variable	Rotation (°) (Dip/DipDir/Pitch)	Nugget Effect	Structure 1				Structure 2			
				Sill	Axis Distance (m)			Sill	Axis Distance (m)		
					Major	Semi-Major	Minor		Major	Semi-Major	Minor
North	Zn	75 / 355 / 10	0.31	0.25	85	45	3	0.44	170	100	4
	Pb	75 / 355 / 10	0.2	0.65	95	59	2.7	0.15	155	100	6
	Cu	75 / 355 / 10	0.11	0.67	60	74	2.2	0.22	140	80	6
	Ag	75 / 355 / 30	0.22	0.59	115	54	2.5	0.19	130	75	4
	Au	75 / 355 / 10	0.07	0.42	90	70	2	0.51	250	230	6.5
	Density	75 / 355 / 10	0.3	0.47	135	95	3	0.23	150	105	8
South	Zn	78 / 351 / 170	0.28	0.46	23	8.5	5	0.26	115	47	9
	Pb	78 / 351 / 170	0.36	0.37	30	4	5	0.27	58	50	10
	Cu	78 / 351 / 170	0.19	0.3	22	6	6	0.51	125	45	10
	Ag	78 / 351 / 170	0.25	0.3	28	8	3	0.45	120	70	10
	Au	78 / 351 / 160	0.23	0.43	125	4	3.7	0.35	125	45	9
	Density	79 / 351 / 170	0.29	0.47	35	6	2.5	0.23	50	45	6

Table 14-11: El Cura Variogram Model Parameters

Domain	Variable	Rotation (°) (Dip/DipDir/Pitch)	Nugget Effect	Structure 1				Structure 2			
				Sill	Axis Distance (m)			Sill	Axis Distance (m)		
					Major	Semi-Major	Minor		Major	Semi-Major	Minor
Top	Zn	75 / 345 / 33	0.21	0.21	58	80	7	0.59	118	85	7
	Pb	75 / 345 / 33	0.19	0.26	85	50	7	0.56	110	50	7
	Cu	75 / 345 / 14	0.2	0.8	82	65	5	-	-	-	-
	Ag	75 / 345 / 24	0.16	0.69	100	60	3	0.15	100	60	7
	Au	75 / 345 / 42	0.28	0.32	155	85	2.4	0.41	180	85	7
	Density	75 / 345 / 48	0.1	0.44	54	50	6	0.46	270	155	6

14.9 Block Modelling

Block models defining the mineralised zones were constructed in Leapfrog Edge using the domain wireframes. The upper limit of the block model was restricted by a topographic surface. A parent block size of 20 m x 20 m x 5 m was used for all deposits. To effectively represent domain volume, sub-cell splitting was enabled at domain boundaries. The models were rotated to align with the general strike and dip of the deposits. Full block model parameters are outlined in Table 14-12.

Table 14-12: Block Model Parameters

Parameter	La Romanera			La Infanta			El Cura		
	X	**Y**	**Z**	**X**	**Y**	**Z**	**X**	**Y**	**Z**
Block Size (m)	20	20	5	20	20	5	20	20	5
Sub-Block Count	8	8	16	16	16	16	16	16	16
Base Point	645780	4172623	440	652663	4171567	425	649130	4171187	297
Rotation (°)	**Azimuth**	**Dip**	**Pitch**	**Azimuth**	**Dip**	**Pitch**	**Azimuth**	**Dip**	**Pitch**
	16	70	0	352	78	0	342	76	0

14.10 Estimation Methodology

Estimation for Zn, Pb, Cu, Ag, Au, S, and density was undertaken on the blocks defined within each domain. The domains were treated as hard boundaries, and as such, composites from an adjacent domain could not be used in the grade estimation of another domain.

Ordinary kriging (OK) was used as the estimation method for domains where a suitable variogram was derived. Inverse distance weighting squared (IDW2) was used for the remaining domains and for sulphur.

Grade estimation was primarily performed in a three-pass plan, with the second and third passes using progressively larger search radii to estimate blocks not estimated on the previous pass. Search radii were guided by the variography and data spacing. For OK domains, the first-pass maximum search distance was set to 1 to 1.5 times the nominal drillhole spacing. Intermediate and minimum search distances were then scaled to reproduce the geometric anisotropy defined by the variogram model for each variable. First-pass search distances for IDW2 domains were based solely on the general drillhole spacing. For all domains, the second-pass search corresponded to twice the first-pass search, and the third-pass search corresponded to three times the first-pass search. Dynamic anisotropy was employed to align the search orientation with the local domain orientation.

The minimum and maximum sample numbers for the first estimation pass were guided by Quantitative Kriging Neighbourhood Analysis (QKNA). First pass block estimates were typically required to be informed by a minimum of two drillholes. Minimum sample and drillhole requirements were relaxed in higher estimation passes and distance-based capping was selectively applied to limit grade extrapolation.

Sample weighting during grade estimation was determined by the variogram model parameters for the OK method. A small volume of blocks containing negative grade estimates due to negative kriging weights were set to the analysis detection limit for a given variable. Discretisation was set at 3 x 3 x 3 for all variables and domains.

Estimation parameters are listed for La Romanera in Table 14-13, La Infanta in Table 14-14, and El Cura in Table 14-15.

Table 14-13: La Romanera Grade Estimation Parameters

Domain	Interpolant	Variable	Pass	Ellipsoid Ranges (m)			Number of Samples			Distance Based Cap	
				Max.	Int.	Min.	Min.	Max.	Max. per Hole	Cap	Distance (% of Ellipsoid)
Lower	OK	Zn	1	75	52	13	8	20	4		
			2	150	104	26	4	16			
			3	225	156	38	1	16			
		Pb	1	75	50	17	8	20	4		
			2	150	100	33	4	16			
			3	225	150	50	1	16			
		Cu	1	75	43	15	8	20	4		
			2	150	87	31	4	16			
			3	225	130	46	1	16			
		Ag	1	75	63	13	8	20	4		
			2	150	126	25	4	16			
			3	225	189	38	1	16			
		Au	1	75	40	11	8	20	4		
			2	150	79	22	4	16			
			3	225	119	33	1	16			
Lower MS	OK	Density	1	75	60	16	8	20	4		
			2	150	121	33	4	16			
			3	225	181	49	1	16			
	IDW2	S	1	75	50	20	8	20	4		
			2	150	100	40	4	16			
			3	225	150	60	1	16			
Lower SMS	OK	Density	1	75	48	15	8	20	4		
			2	150	95	30	4	16			
			3	225	143	45	1	16			
	IDW2	S	1	75	50	20	8	20	4		
			2	150	100	40	4	16			
			3	225	150	60	1	16			

Domain	Interpolant	Variable	Pass	Ellipsoid Ranges (m)			Number of Samples			Distance Based Cap	
				Max.	Int.	Min.	Min.	Max.	Max. per Hole	Cap	Distance (% of Ellipsoid)
Upper	OK	Zn	1	75	44	13	8	20	4		
			2	150	87	26	4	16			
			3	225	131	39	1	16			
		Pb	1	75	54	14	8	20	4		
			2	150	107	28	4	16			
			3	225	161	41	1	16			
		Cu	1	75	49	12	8	20	4		
			2	150	99	25	4	16			
			3	225	148	37	1	16			
		Ag	1	75	50	15	8	20	4		
			2	150	100	30	4	16			
			3	225	150	45	1	16			
		Au	1	75	52	13	8	20	4		
			2	150	104	26	4	16			
			3	225	156	39	1	16			
Upper MS and Upper SMS	IDW2	Density & S	1	50	50	25	8	20			
			2	100	100	50	4	16			
			3	200	200	100	1	16			
Minor Lenses and LG	IDW2	All	1	50	50	25	8	20			
			2	100	100	50	4	16			
			3	200	200	100	1	16			

Table 14-14: La Infanta Grade Estimation Parameters

Domain	Interpolant	Variable	Pass	Ellipsoid Ranges (m)			Number of Samples			Distance Based Cap	
				Max.	Int.	Min.	Min.	Max.	Max. per Hole	Cap	Distance (% of Ellipsoid)
North	OK	Zn	1	75	44	15	8	16	4		
			2	150	88	30	4	12		9.2	50
			3	225	132	45	1	12		5.2	25
		Pb	1	75	48	15	8	16	4		
			2	150	97	30	4	12		8.8	50
			3	225	145	45	1	12		4.1	25
		Cu	1	75	43	15	8	16	4		
			2	150	86	30	4	12		2.0	50
			3	225	129	45	1	12		1.3	25
		Ag	1	75	43	15	8	16	4		
			2	150	87	30	4	12			
			3	225	130	45	1	12		238	25
		Au	1	75	69	15	8	16	4		
			2	150	138	30	4	12		1.35	25
			3	225	207	45	1	12		1.35	25
		Density	1	75	53	15	8	16	4		
			2	150	105	30	4	12			
			3	225	158	45	1	12			
	IDW2	S	1	75	50	20	8	16	4		
			2	150	100	40	4	12			
			3	225	150	60	1	12			
South	OK	Zn	1	75	45	15	8	16	4		
			2	150	90	30	4	12		10	50
			3	225	135	45	1	12		5	25
		Pb	1	75	65	13	8	16	4		
			2	150	129	26	4	12		11.7	50
			3	225	194	39	1	12		11.7	25
		Cu	1	75	45	15	8	16	4		
			2	150	90	30	4	12		2.7	25
			3	225	135	45	1	12		2.7	12.5

Domain	Interpolant	Variable	Pass	Ellipsoid Ranges (m)			Number of Samples			Distance Based Cap	
				Max.	Int.	Min.	Min.	Max.	Max. per Hole	Cap	Distance (% of Ellipsoid)
		Ag	1	75	44	15	8	16	4		
			2	150	88	30	4	12		270	50
			3	225	131	45	1	12		270	25
		Au	1	75	45	15	8	16	4		
			2	150	90	30	4	12		1	50
			3	225	135	45	1	12		1	25
		Density	1	75	68	15	8	16	4		
			2	150	135	30	4	12			
			3	225	203	45	1	12			
	IDW2	S	1	75	50	20	8	16			
			2	150	100	40	4	12			
			3	225	150	60	1	12			
South 1	IDW2	Zn	1	50	50	50	6	16	4		
			2	100	100	100	2	12		7.5	25
		Pb	1	50	50	50	6	16	4		
			2	100	100	100	2	12		5.2	25
		Cu	1	50	50	50	6	16	4		
			2	100	100	100	2	12		1.75	50
		Ag	1	50	50	50	6	16	4		
			2	100	100	100	2	12		80	25
		Au	1	50	50	50	6	16	4		
			2	100	100	100	2	12		0.8	50
		Density	1	50	50	50	6	16	4		
			2	100	100	100	2	12			
		S	1	50	50	50	6	16	4		
			2	100	100	100	2	12			
North FW 1 and LG	ID2	All	1	50	50	25	6	16			
			2	100	100	50	2	12			
			3	200	200	100	1	12			

Table 14-15: El Cura Grade Estimation Parameters

Domain	Interpolant	Variable	Pass	Ellipsoid Ranges (m)			Number of Samples			Distance Based Cap	
				Max.	Int.	Min.	Min.	Max.	Max. per Hole	Cap	Distance (% of Ellipsoid)
Top	OK	Zn	1	75	54	15	8	16			
			2	150	108	30	4	12		5.9	25
			3	300	216	60	1	12		3.3	12.5
		Pb	1	75	40	15	8	16			
			2	150	80	30	4	12		3.2	25
			3	300	160	60	1	12		3.2	12.5
		Cu	1	75	59	15	8	16			
			2	150	119	30	4	12		4.3	25
			3	300	238	60	1	12		4.3	12.5
		Ag	1	75	45	15	8	16			
			2	150	90	30	4	12		118	25
			3	300	180	60	1	12		118	12.5
		Au	1	75	40	15	8	16			
			2	150	80	30	4	12		4.2	25
			3	300	160	60	1	12		4.2	12.5
		Density	1	75	43	15	8	16			
			2	150	86	30	4	12			
			3	300	172	60	1	12			
	IDW2	S	1	50	50	25	6	16			
			2	100	100	50	2	12			
			3	200	200	100	2	12			
LG	IDW2	All	1	50	50	25	6	16			
			2	100	100	50	2	12			
			3	200	200	100	2	12			

14.11 Model Validation

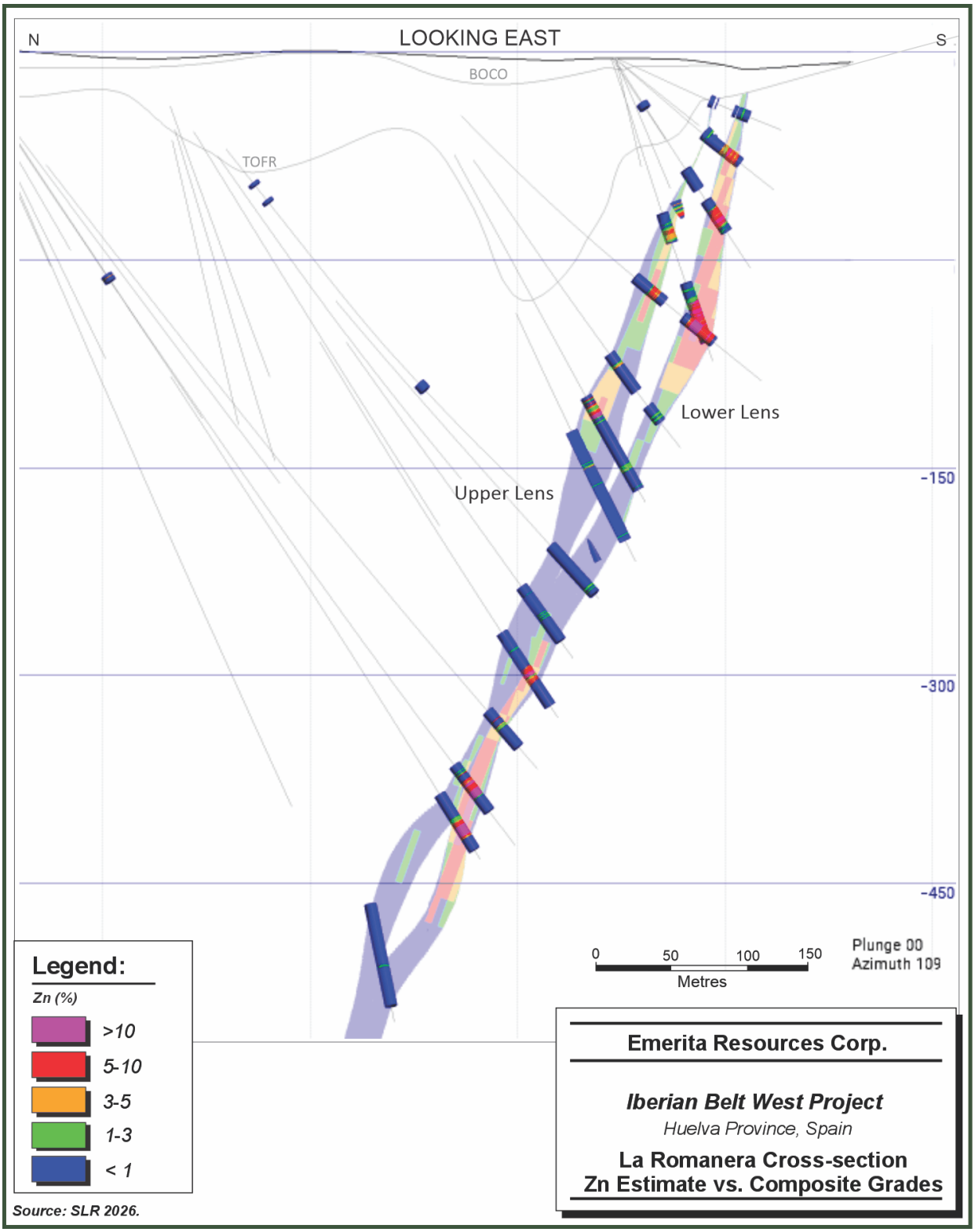
14.11.1 Introduction

Model validation was carried out for all variables and domains. Validation included a visual comparison of composite and estimated block model grades. Nearest neighbour (NN) values were interpolated for validation purposes and used for global statistical and swath plot comparison against estimated block model values.

14.11.2 Visual Comparison

Visual validation was conducted by comparing input drillhole composite and estimated values in cross-section and long-section. The checks showed good agreement between drillhole composite values and block model values. Representative cross- and long-sections are provided for La Romanera (Figure 14-16 and Figure 14-17), La Infanta (Figure 14-18 and Figure 14-19), and El Cura (Figure 14-20 and Figure 14-21).

Figure 14-16: La Romanera Cross Section - Zn Estimate vs. Composite Grades



Source: SLR 2026.

Figure 14-17: La Romanera Long Sections - Zn Estimate vs. Full Domain Width Composite Grades (Excluding LG Envelopes)

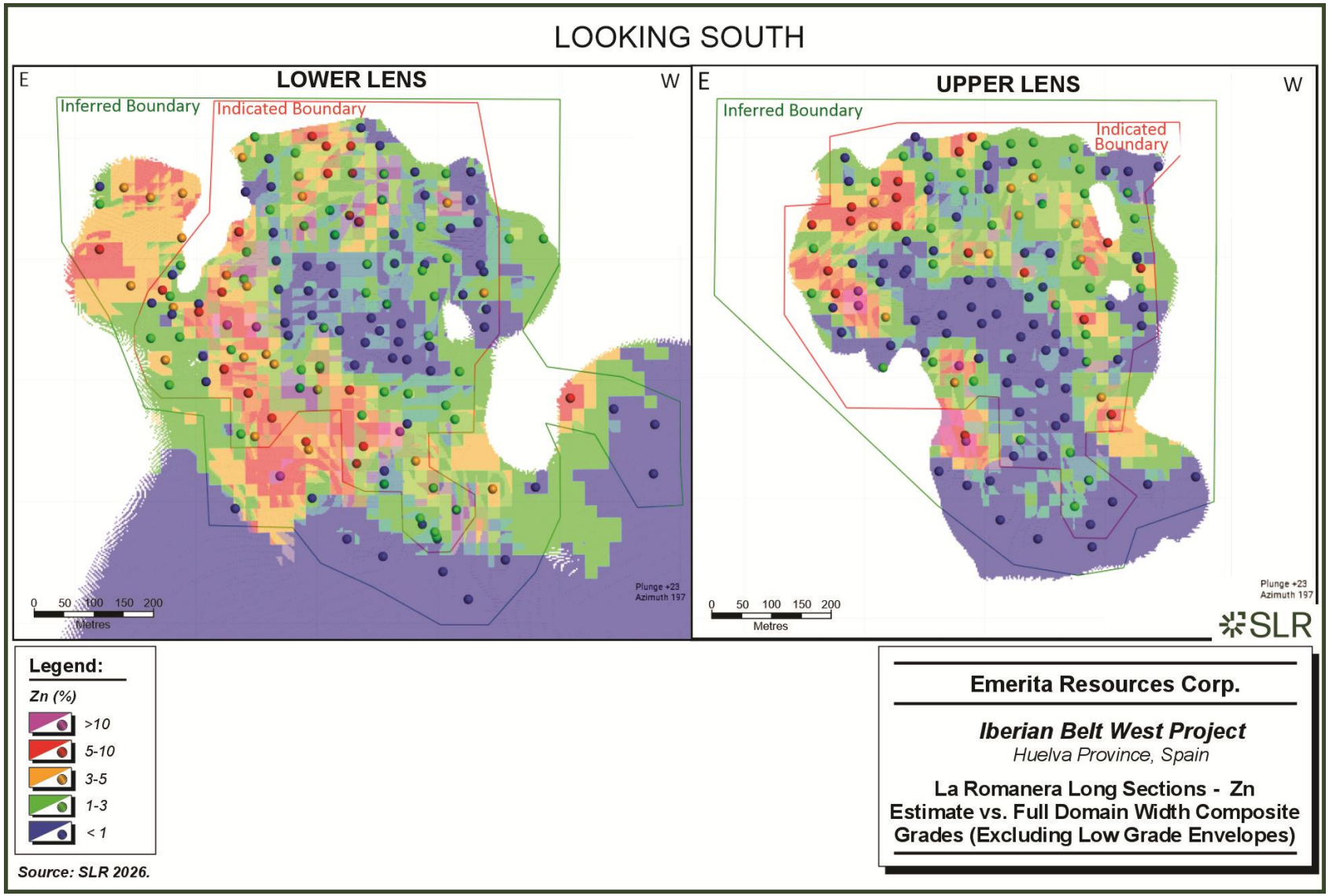


Figure 14-18: La Infanta Cross Section - Zn Estimate vs. Composite Grades

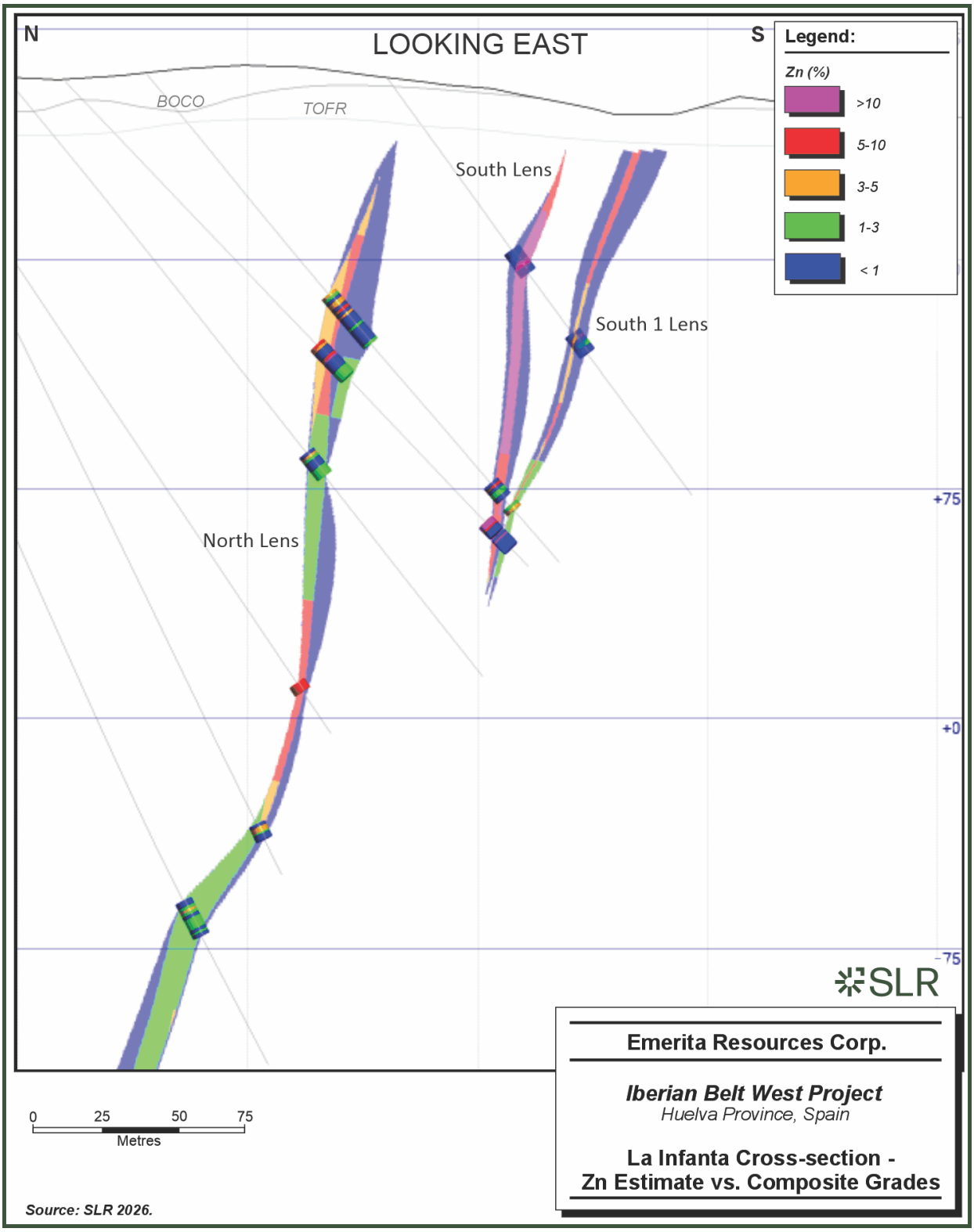


Figure 14-19: La Infanta Long Sections - Zn Estimate vs. Full Domain Width Composite Grades (Excluding LG Envelopes)

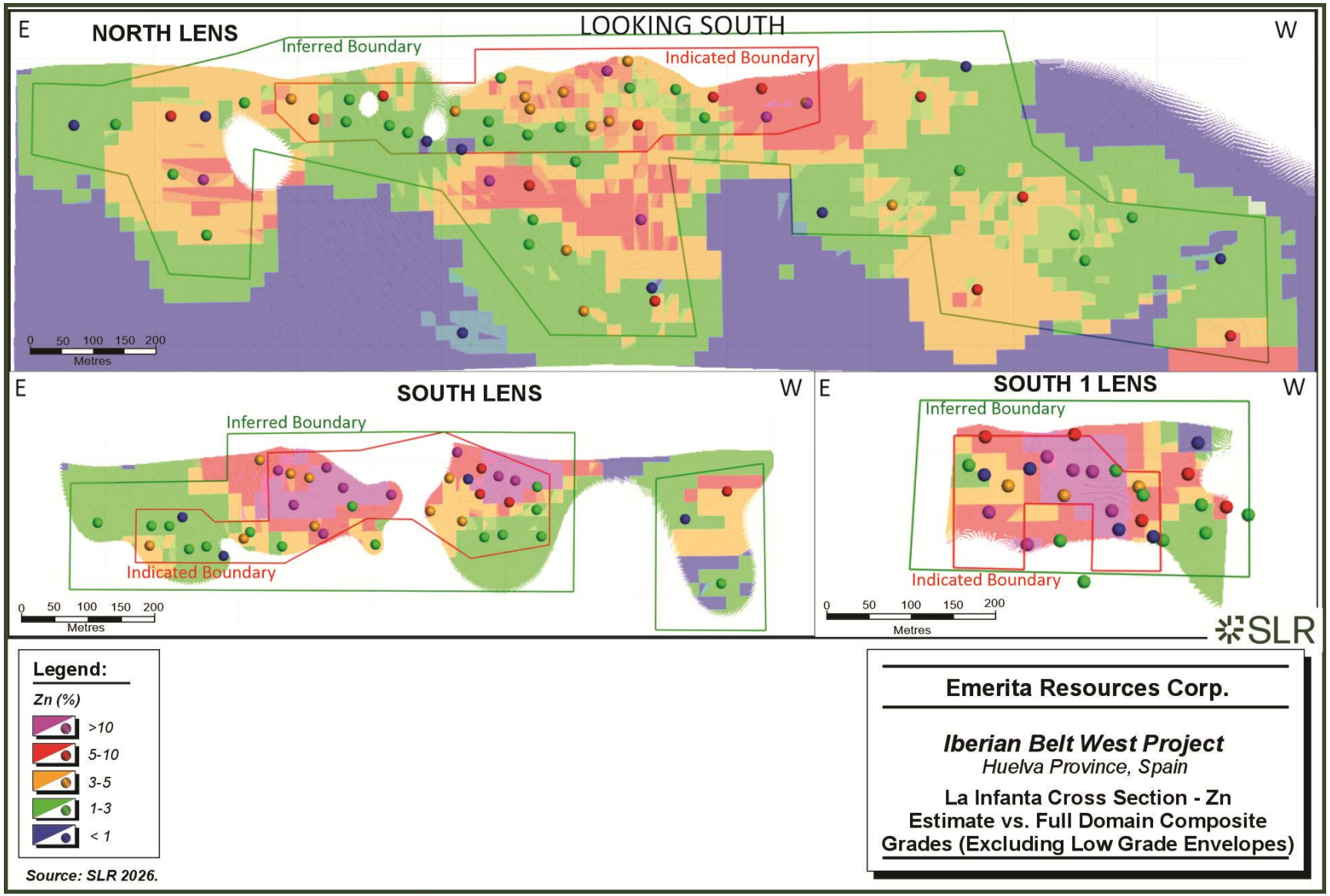


Figure 14-20: El Cura Cross-section - Cu Estimate vs. Composite Grades

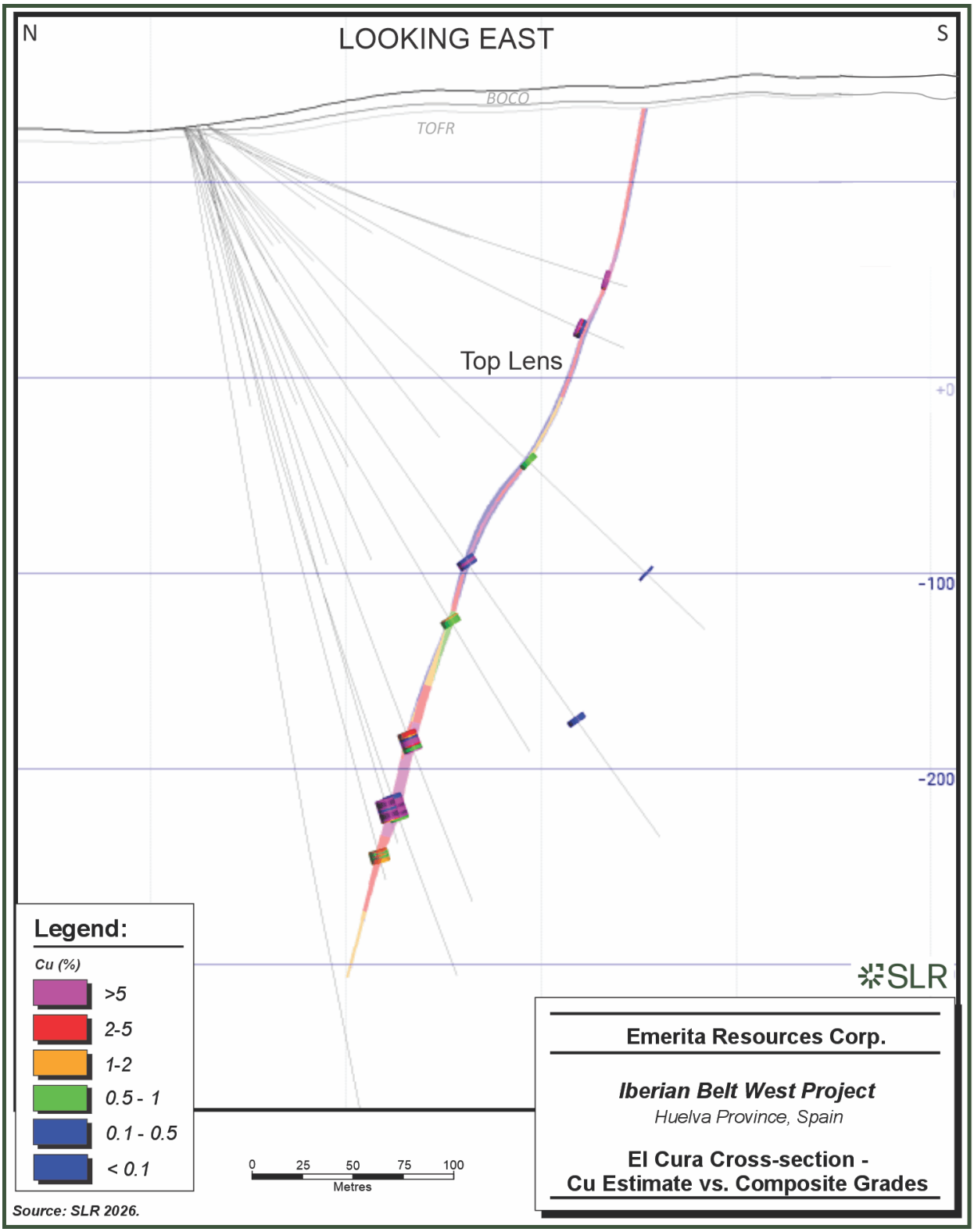
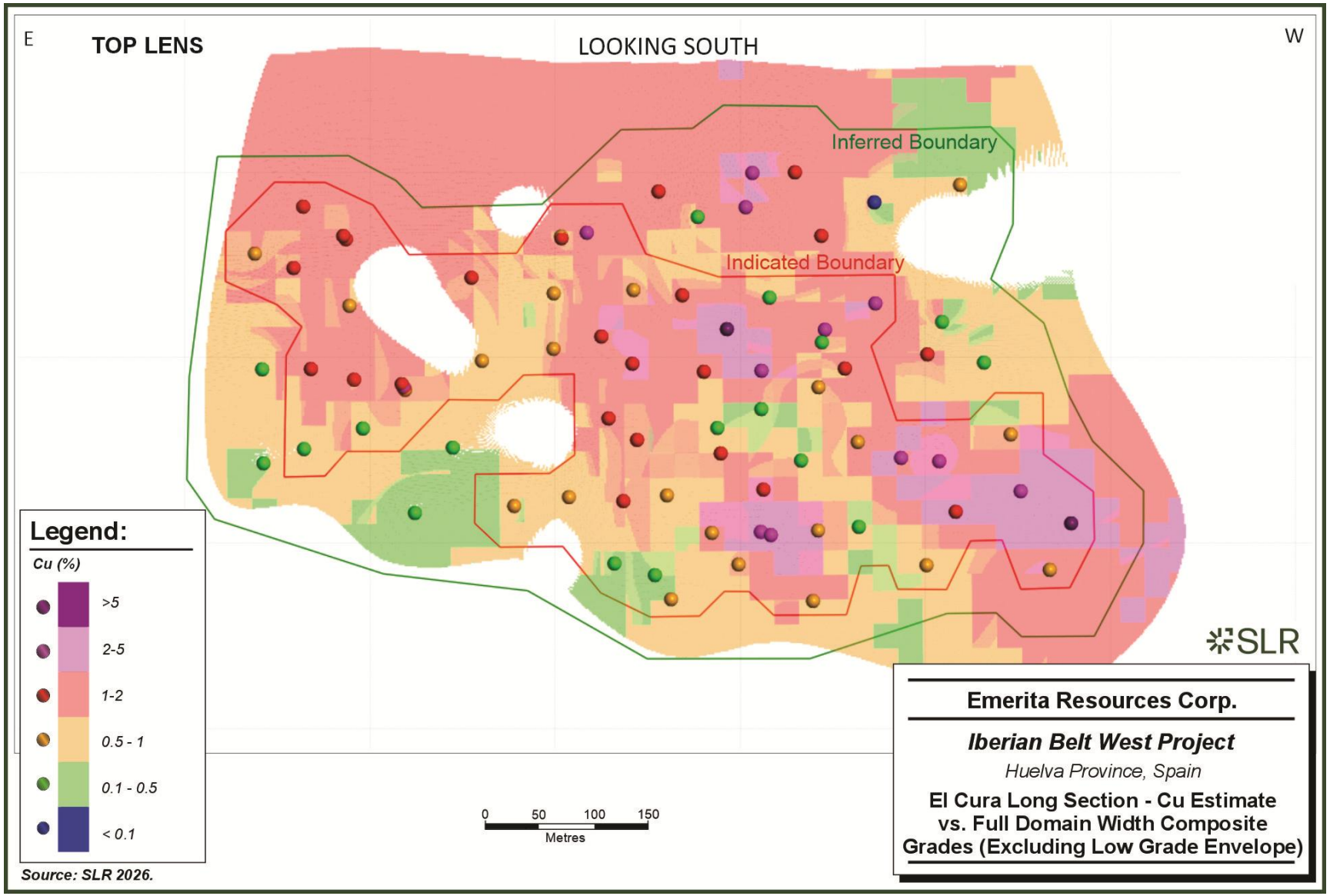


Figure 14-21: El Cura Long Section - Cu Estimate vs. Full Domain Width Composite Grades (Excluding LG Envelope)



14.11.3 Statistical Comparison

The block model estimates were checked for global bias by comparing with the average values from NN estimates. The NN estimator declusters the data and produces a theoretically unbiased estimate of the average value when no cut-off grade is applied. Results for major lenses are summarised in Table 14-16, Table 14-17 and Table 14-18, and show no material global bias.

Table 14-16: La Romanera Mean Grade Comparison by Domain

Statistic	Zn (%)		Pb (%)		Cu (%)		Ag (g/t)		Au (g/t)		S (%)		Bulk Density (g/cm³)	
	MRE	NN	MRE	NN	MRE	NN	MRE	NN	MRE	NN	MRE	NN	MRE	NN
Lower Lens														
Mean	2.77	2.78	1.20	1.22	0.48	0.47	57.1	58.2	1.20	1.21	39.6	39.1	4.29	4.28
% Diff.	-0.3%		-1.3%		2.0%		-2.0%		-0.4%		1.1%		0.0%	
Upper Lens														
Mean	1.88	1.88	1.00	0.97	0.42	0.44	52.7	53.0	0.98	0.96	37.6	36.4	4.21	4.18
% Diff.	0.1%		3.7%		-4.1%		-0.4%		1.3%		3.2%		0.8%	

Table 14-17: La Infanta Mean Grade Comparison by Domain

Statistic	Zn (%)		Pb (%)		Cu (%)		Ag (g/t)		Au (g/t)		S (%)		Bulk Density (g/cm³)	
	MRE	NN	MRE	NN	MRE	NN	MRE	NN	MRE	NN	MRE	NN	MRE	NN
Lower Lens														
Mean	3.90	4.66	2.35	2.64	0.56	0.66	53.7	67.7	0.26	0.24	6.2	6.7	2.96	2.95
% Diff.	-16.4%		-11.0%		-14.0%		-20.7%		7.2%		-6.4%		0.3%	
Upper Lens														
Mean	8.63	9.22	4.83	5.03	1.19	1.21	102.7	98.3	0.36	0.36	7.8	7.3	3.13	3.09
% Diff.	-6.3%		-3.9%		-1.4%		4.5%		-0.1%		6.9%		1.1%	
South 1 Lens														
Mean	11.97	11.61	6.48	6.62	1.55	1.51	123.2	107.5	0.43	0.44	10.3	9.8	3.07	3.24
% Diff.	3.1%		-2.1%		2.7%		14.5%		-2.6%		5.2%		-5.2%	

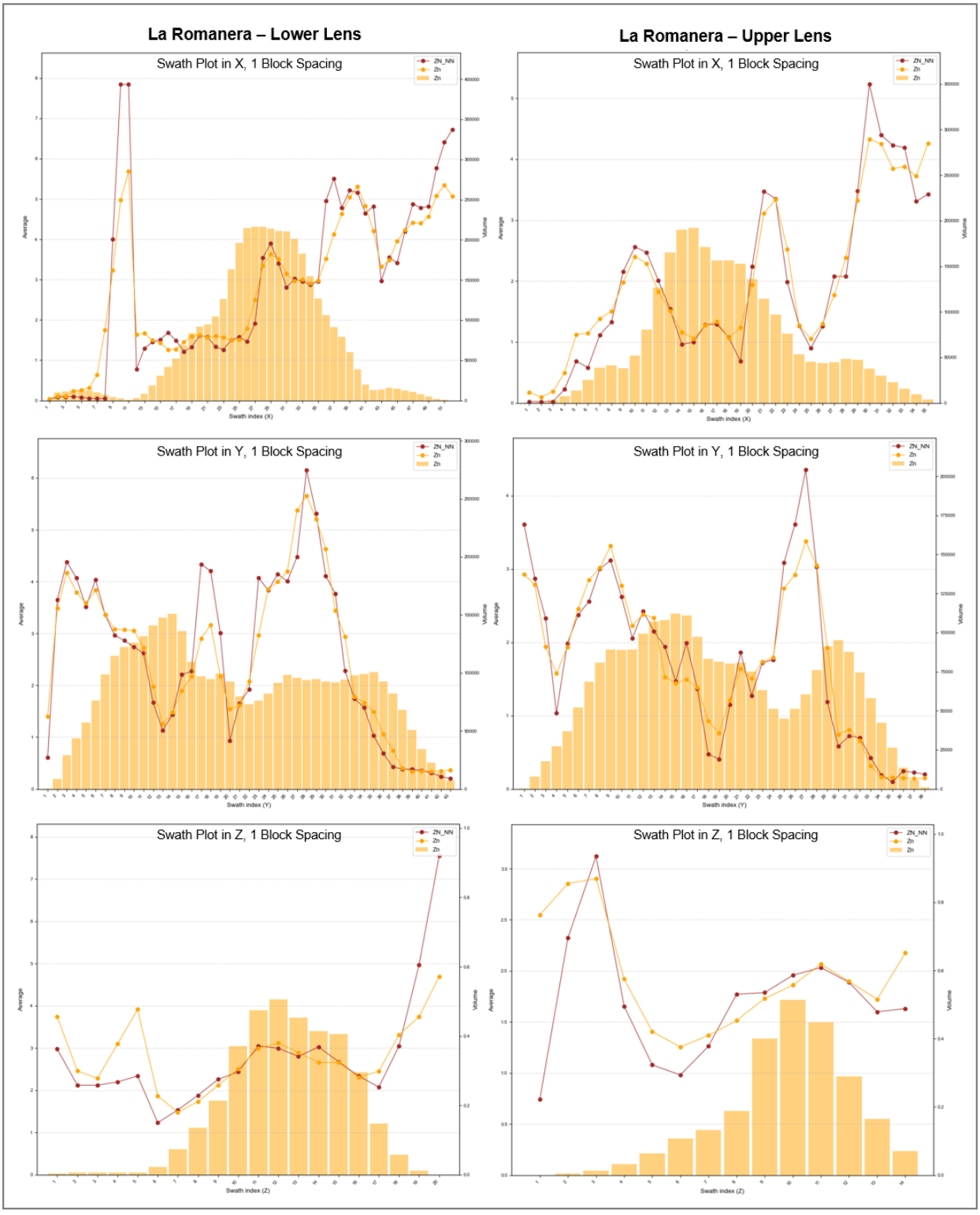
Table 14-18: El Cura Mean Grade Comparison by Domain

Statistic	Zn (%)		Pb (%)		Cu (%)		Ag (g/t)		Au (g/t)		S (%)		Bulk Density (g/cm³)	
	MRE	NN	MRE	NN	MRE	NN	MRE	NN	MRE	NN	MRE	NN	MRE	NN
Top Lens														
Mean	1.64	1.59	0.77	0.75	1.27	1.26	38.6	38.0	1.25	1.26	31.1	29.9	3.75	3.73
% Diff.	3.0%		3.1%		1.0%		1.6%		-1.0%		4.0%		0.4%	

14.11.4 Swath Plots

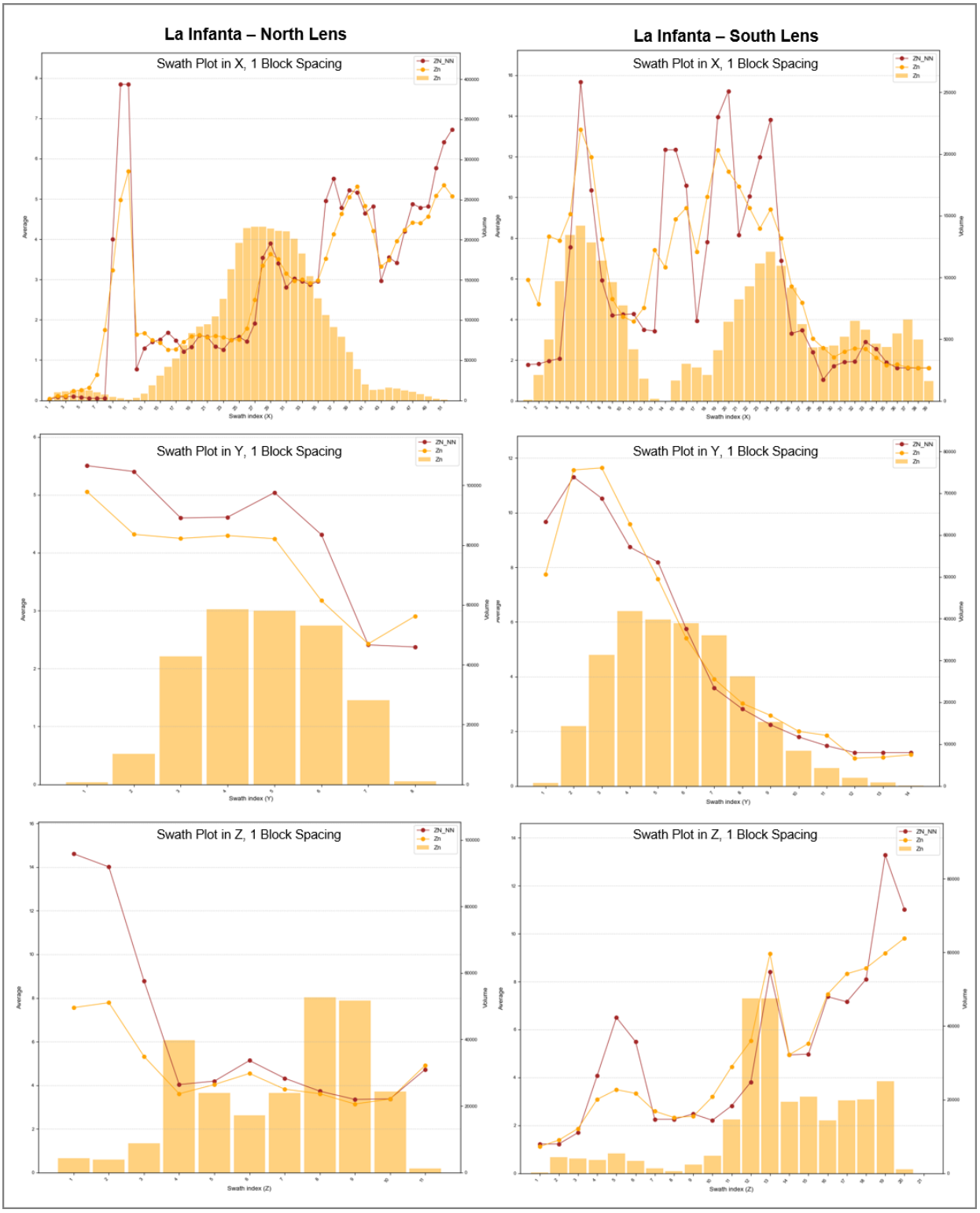
Swath plots provide a spatial comparison of average grades from the block model estimates with average grades from NN estimates (e.g. Figure 14-22 and Figure 14-23). The model estimate should be smoother than the NN estimate. The observed grade profiles behave as expected and show no significant local bias.

Figure 14-22: Swath Plots for the Main La Romanera Domains (OK Grade Profile in Orange and NN Grade Profile in Dark Red)



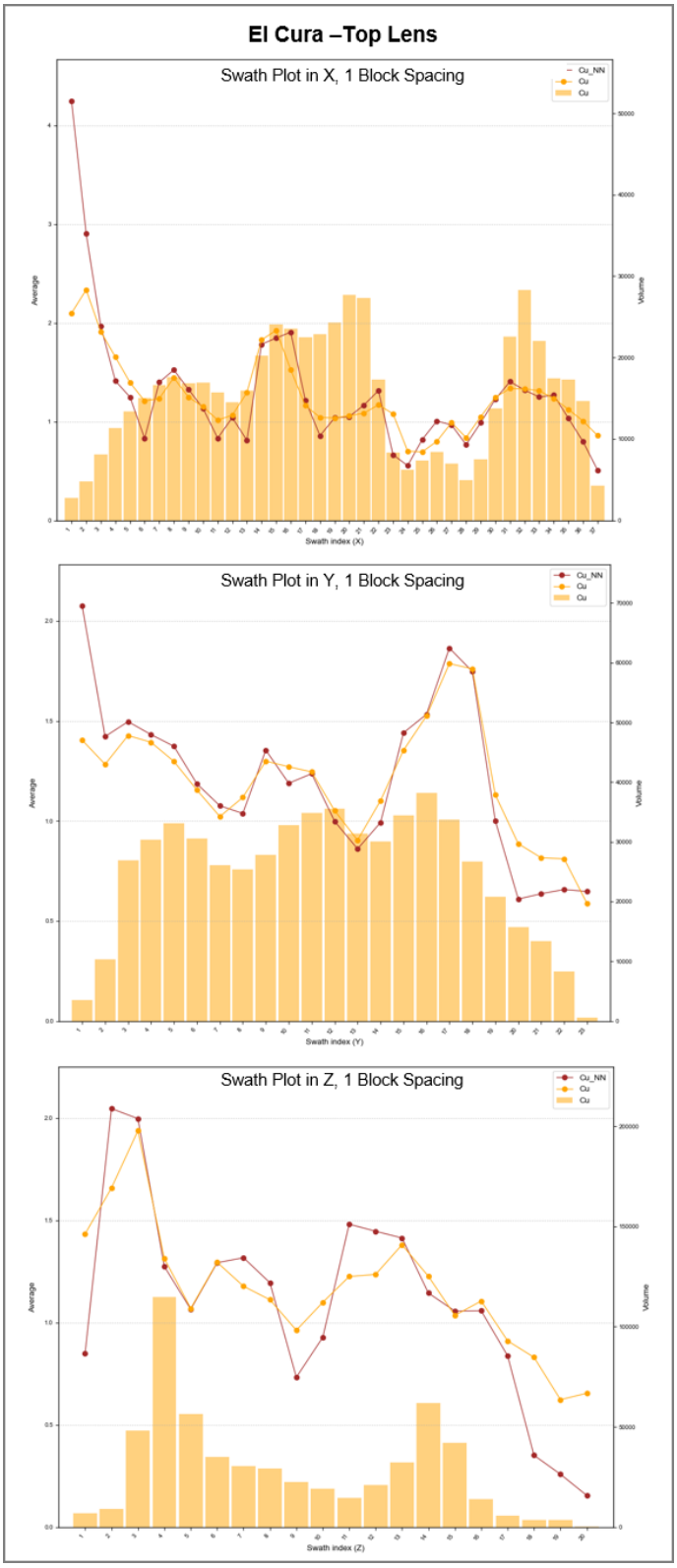
Source: SLR 2026.

Figure 14-23: Swath Plots for Main La Infanta Domains (OK Grade Profile in Orange and NN Grade Profile in Dark Red)



Source: SLR 2026.

Figure 14-24: Swath Plots for El Cura Top Lens (OK Grade Profile in Orange and NN Grade Profile in Dark Red)



Source: SLR 2026.

14.12 Mineral Resource Classification

Definitions for resource categories used in this Technical Report are consistent with those defined by CIM (2014) and adopted by NI 43-101.

At the IBW Project, the approach to Mineral Resource classification is underpinned by confidence in the drillhole data, the geological interpretation, geological continuity, data density and orientation, spatial grade continuity, and confidence in the Mineral Resource estimation.

Classification was set in the block models using wireframes that define contiguous regions that meet specific drill spacing and estimation pass criteria. For Indicated Resources, nominal drill spacing is 50 m or less and blocks are mainly estimated in the first pass. For Inferred Resources, nominal drill spacing is 100m or less. Minor parallel lenses at La Romanera and La Infanta were classified as Inferred.

The Mineral Resource classification relative to input drillhole data is shown for the main lenses at La Romanera (Figure 14-25), La Infanta (Figure 14-26), and El Cura (Figure 14-27).

14.13 Reasonable Prospects for Eventual Economic Extraction

Mineral Resource reporting is based on a conceptual operating scenario comprising underground mining via long-hole open stoping (LHOS), on-site selective flotation of Cu, Pb, Zn, and pyrite concentrates, and off-site third-party treatment and refining of the flotation concentrates. No saleable lead concentrate is produced from El Cura and no saleable pyrite concentrate is produced from La Infanta.

To ensure reasonable prospects for eventual economic extraction (RPEEE), the IBW Project Mineral Resources are reported within underground reporting shapes generated by a mineable stope optimiser (MSO), using an NSR cut-off value of US$69.3/t for La Romanera, US$79.2/t for El Cura, and US$85.3/t for La Infanta. These cut-off values equate to the total operating cost estimates for each deposit.

The technical and economic parameters used to calculate NSR factors for each metal are provided in Table 14-19. These factors were used to calculate the NSR value of each block. Base and precious metal prices reflect consensus, long-term forecasts from banks, financial institutions, and other sources. Pyrite concentrate pricing is based on a market study for 48% sulphur pyrite concentrates (Claight 2026). Metallurgical recoveries reflect available testwork data, whilst market studies for each concentrate were used to estimate payable factors after deductions and penalties, as well as transport, treatment, and refining charges (Cuadri de la Corte 2025; Claight 2026).

The MSO stopes were generated in Deswik using the same parameters as those developed for the IBW Project Mineral Reserve estimate, outlined in Section 15.0 (Table 15-4). Mineralisation domain wireframes were used as control surfaces to guide stope orientation.

Before the MSO process, the NSR value for unclassified blocks was set to zero to ensure that stopes exceeding the NSR cut-off value were supported by classified material only. Stope classification was assigned on a majority tonnage basis. Only primary sulphide mineralisation contained within the MSO stopes was included in reporting. No cut-off value was applied to blocks within the underground reporting shapes, meaning planned dilution (‘must-take material’) is included in the Mineral Resource statement.

The constraining MSO stopes are shown for the main lenses at La Romanera (Figure 14-25), La Infanta (Figure 14-26), and El Cura (Figure 14-27).

Table 14-19: Mineral Resource Estimate Technical and Economic Parameters

Metal Price						
Deposit	**Zn (US$/t)**	**Pb (US$/t)**	**Cu (US$/t)**	**Ag (US$/oz)**	**Au (US$/oz)**	**Pyrite Conc. (US$/t)**
All	3,415	2,425	13,775	65	3,500	265
Net Metallurgical Recovery (%)						
Deposit	**Zn**	**Pb**	**Cu**	**Ag**	**Au**	**S**
La Romanera	78.7	52.2	41.5	93.4	89.8	86.6
El Cura	67.9	0	79.4	79.8	87.4	82.7
La Infanta	78.0	78.3	42.4	88.2	50.9	0
Net Payabilities after Deductions and Penalties (%)						
Deposit	**Zn**	**Pb**	**Cu**	**Ag**	**Au**	**S**
La Romanera	74.6	83.4	79.0	56.9	6.7	95.1
El Cura	78.4	0	93.3	49.5	7.3	95.8
La Infanta	83.1	83.3	52.7	66.6	18.4	0
Operating Costs (US$/t ore)						
Deposit	**Mining**	**Processing**	**G&A**	**Total (NSR Cut-Off Value)**		
La Romanera	36	30.2	3.1	69.3		
El Cura	49	30.2	0	79.2		
La Infanta	52	30.2	3.1	85.3		
Selling Costs and Assumptions						
Product	**Transport (US$/wmt)**	**Treatment Charges / Refining Charges (TC/RC) (US$/dmt or *US$/oz)**	**Moisture (%)**			
Zn Conc.	123	205	8			
Cu Conc.	123	100	8			
Pb Conc.	12.8	180	8			
Pyrite Conc.	9.3	50	8			
Au Doré	-	5.0*	-			
Ag Doré	-	0.5*	-			
Block NSR Factors (US$)						
Deposit	**Zn**	**Pb**	**Cu**	**Ag**	**Au**	**S**
La Romanera	14.72	6.79	40.39	1.10	6.77	3.28
El Cura	13.11	0	93.42	0.85	7.15	3.33
La Infanta	17.54	12.56	25.73	1.22	10.52	0

Figure 14-25: La Romanera Long Sections – Mineral Resource Classification, Underground Reporting Shapes and Mineralisation Domain Intersections

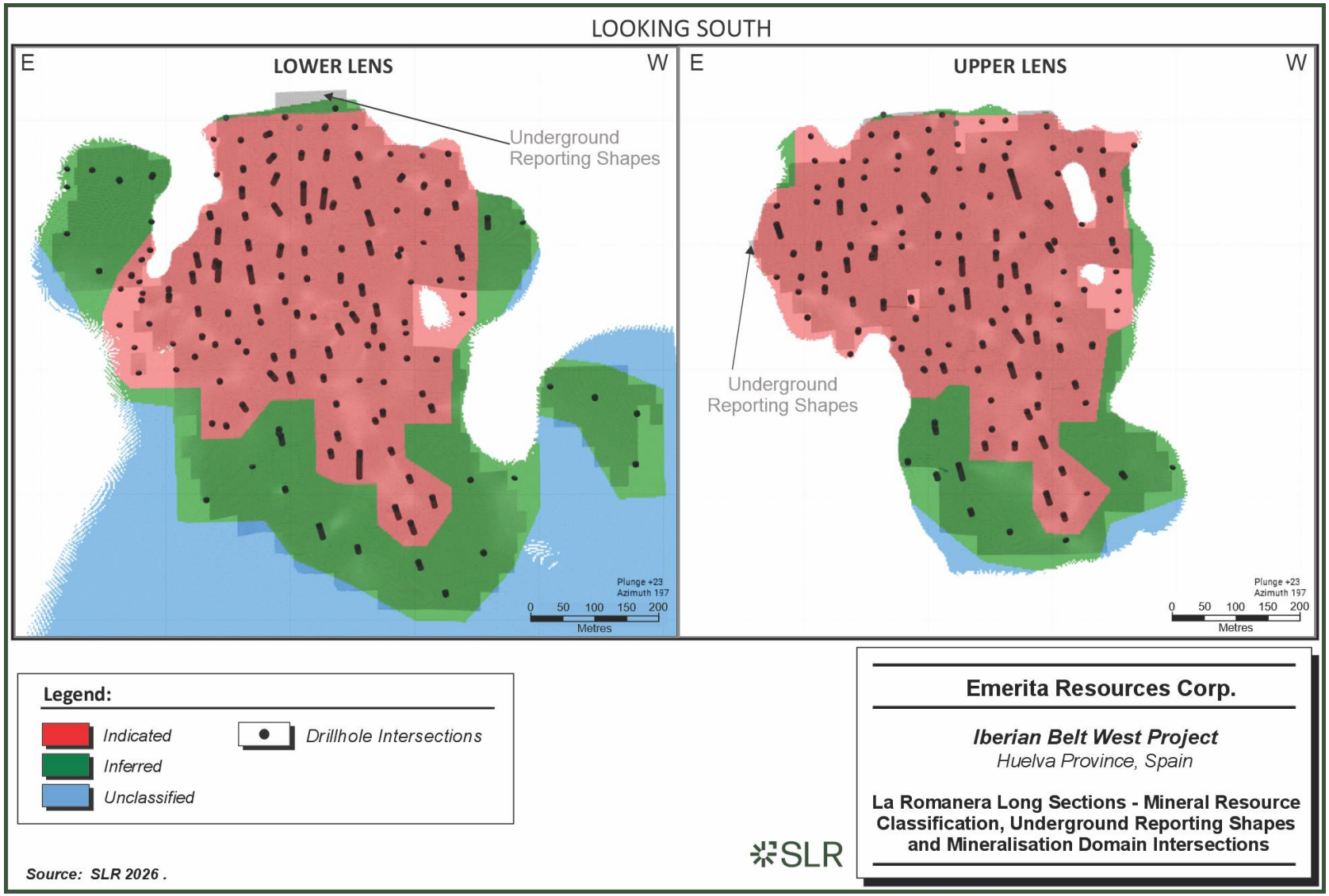
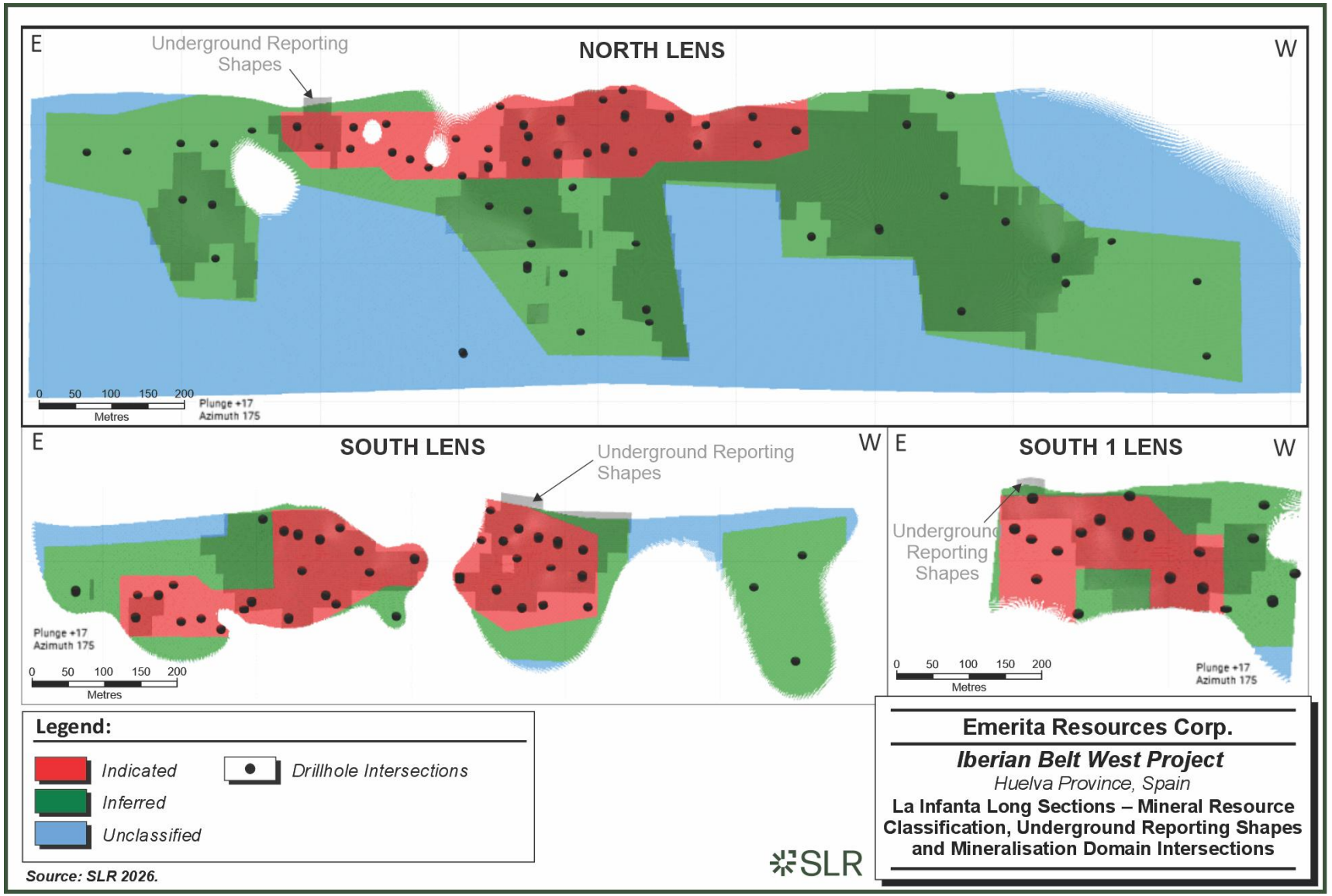
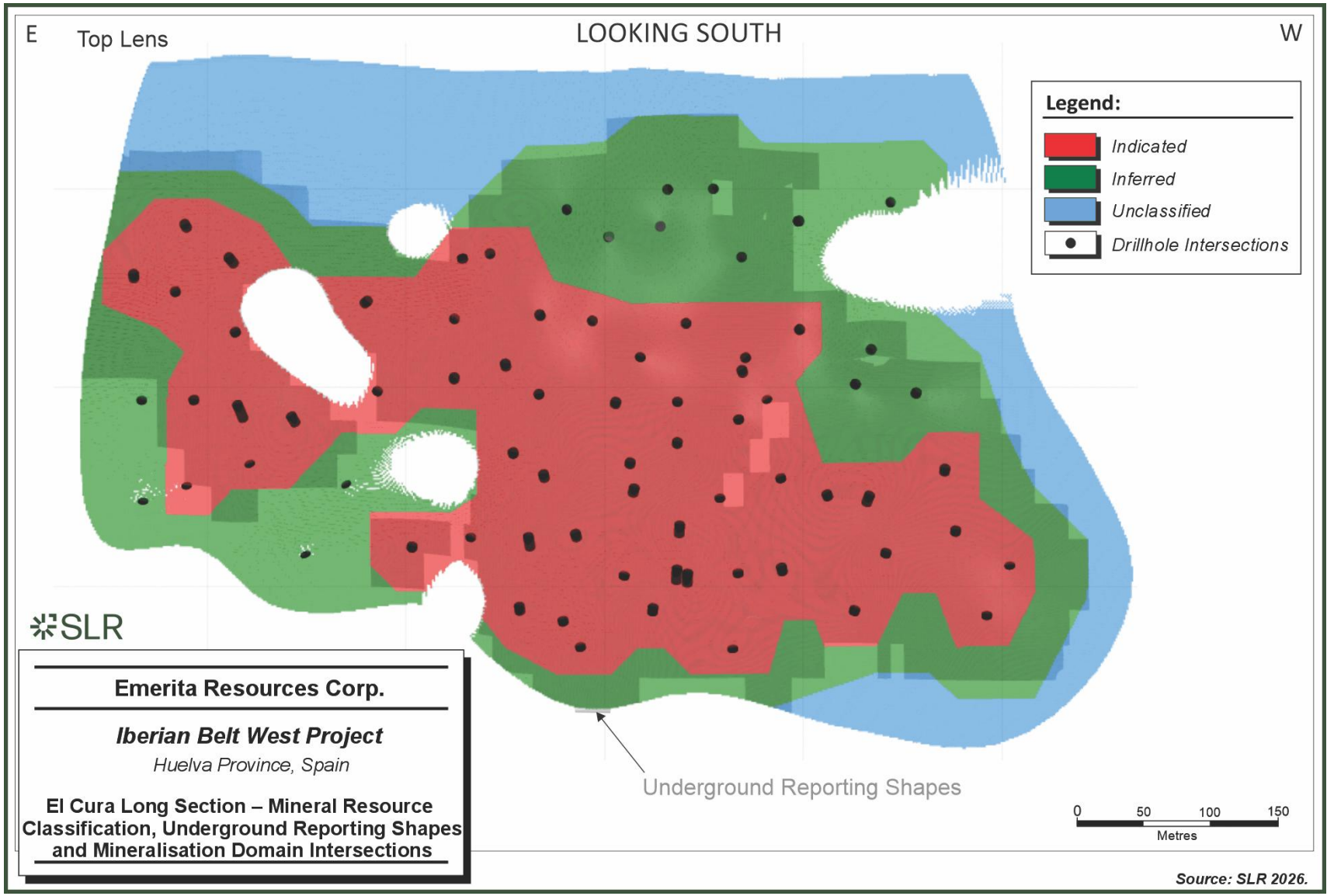


Figure 14-26: La Infanta Long Sections – Mineral Resource Classification, Underground Reporting Shapes and Mineralisation Domain Intersections



Source: SLR 2026.

Figure 14-27: El Cura Long Section – Mineral Resource Classification, Underground Reporting Shapes and Mineralisation Domain Intersections



14.14 Mineral Resource Reporting

The MRE for the IBW Project has an effective date of July 17, 2026 (Table 14-20). Mineral Resources are reported inclusive of Mineral Reserves. Mineral Resources that are not Mineral Reserves do not have demonstrated economic viability. The MRE was prepared in accordance with the Canadian Institute of Mining, Metallurgy and Petroleum (CIM) Definition Standards for Mineral Resources and Mineral Reserves (CIM, 2014 definitions).

Mineral Resources are reported within underground reporting shapes based on NSR cut-off values of US$69.30/t for La Romanera, US$79.20/t for El Cura, and US$85.30/t for La Infanta.

The QP is not aware of any environmental, permitting, legal, title, taxation, socio-economic, marketing, political, or other relevant factors that could materially affect the MRE.

Table 14-20: Summary of Mineral Resources – July 17, 2026

Deposit	Class	Tonnage Mt	Average Grade						NSR $/t	Contained Metal					
			Zn (%)	Pb (%)	Cu (%)	Ag (g/t)	Au (g/t)	S (%)		Zn (kt)	Pb (kt)	Cu (kt)	Ag (koz)	Au (koz)	S (kt)
La Romanera	Indicated	22.4	2.15	1.03	0.38	53	1.10	35.9	236	481	230	84	38,199	792	8,018
	Inferred	6.6	2.02	0.84	0.49	33	0.57	29.6	192	133	55	32	7,090	120	1,952
El Cura	Indicated	2.1	1.20	0.57	0.96	30	0.98	25.8	223	25	12	20	2,010	65	535
	Inferred	0.9	0.98	0.42	0.74	19	0.62	18.7	165	9	4	7	556	18	168
La Infanta	Indicated	1.7	5.25	3.00	0.73	63	0.25	6.7	228	87	50	12	3,316	13	111
	Inferred	2.4	2.87	1.67	0.45	50	0.28	5.6	147	70	41	11	3,901	22	135
IBW Project	**Indicated**	**26.1**	**2.27**	**1.12**	**0.45**	**52**	**1.04**	**33.2**	**235**	**593**	**292**	**116**	**43,525**	**871**	**8,663**
	Inferred	**9.9**	**2.13**	**1.00**	**0.50**	**36**	**0.50**	**22.7**	**178**	**212**	**100**	**50**	**11,547**	**161**	**2,256**

Notes:

1. CIM (2014) definitions were followed for Mineral Resources.
2. The reporting approach is based on underground mining via long-hole open stoping, on-site selective flotation of copper, lead, zinc, and pyrite concentrates, and off-site third-party treatment and refining of the flotation concentrates.
3. Mineral Resources are reported within underground reporting shapes generated using a mineable stope optimiser (MSO) above NSR cut-off values of US$69.30/t for La Romanera, US$79.20/t for El Cura, and US$85.30/t for La Infanta. Only primary sulphide mineralisation is included in the Mineral Resource.
4. The NSR values for each block were calculated using the following formulas:
   - La Romanera – Zn(%)*US$14.72 + Pb(%)*US$6.79 + Cu(%)*US$40.39 + Ag(g/t)*US$1.10 + Au(g/t)*US$6.77 + S(%)*US$3.28
   - El Cura – Zn(%)*US$13.11 + Cu(%)*US$93.42 + Ag(g/t)*US$0.85 + Au(g/t)*US$7.15 + S(%)*US$3.33
   - La Infanta – Zn(%)*US$17.54 + Pb(%)*US$12.56 + Cu(%)*US$25.73 + Ag(g/t)*US$1.22 + Au(g/t)*US$10.52
5. Factors in the NSR formulas are based on consensus long-term metal price forecasts, metallurgical recoveries from available testwork, and market studies, used to estimate payable factors, transport, treatment and refining charges. Inputs to the block NSR calculation are specified in notes 6 through 8.
6. Mineral Resources are estimated using long-term prices of US$3,415/t Zn, US$2,425/t Pb, US$13,775/t Cu, US$65/oz Ag, US$3,500/oz Au and US$265/t pyrite concentrate (>48% sulphur).
7. The following net metallurgical recoveries have been assumed:
   - La Romanera – 78.7% Zn, 52.2% Pb, 41.5% Cu, 93.4% Ag, 89.8% Au, and 86.6% S.
   - El Cura – 67.9% Zn, 0% Pb, 79.4% Cu, 79.8% Ag, 87.4% Au, and 82.7% S.
   - La Infanta – 78.0% Zn, 78.3% Pb, 42.4% Cu, 88.2% Ag, 50.9% Au, and 0% S.
8. The following net payabilities after deductions and penalties have been assumed:
   - La Romanera – 74.6% Zn, 83.4% Pb, 79.0% Cu, 56.9% Ag, 6.7% Au, and 95.1% S.
   - El Cura – 78.4% Zn, 0% Pb, 93.3% Cu, 49.5% Ag, 7.3% Au, and 95.8% S.
   - La Infanta – 83.1% Zn, 83.3% Pb, 52.7% Cu, 66.6% Ag, 18.4% Au, and 0% S.
9. Mineral Resources are inclusive of Mineral Reserves. Mineral Resources that are not Mineral Reserves do not have demonstrated economic viability.
10. Numbers may not add or multiply due to rounding.

14.15 Comparison with Previous Mineral Resource Estimate

Mineral Resources for the IBW Project have been updated from the previous estimate completed by Wardell Armstrong International (WAI) in 2025 (effective date of February 26, 2025). The percentage changes between the WAI 2025 and SLR 2026 MREs are presented in Table 14-21. Sulphur was not reported in the previous estimate and is excluded from the comparison.

Differences with the previous 2025 MRE are mainly due to the following changes at each deposit.

- At La Romanera, additional NSR attributable to pyrite concentrate production has brought sulphide mineralisation with lower base and precious metal grades into the Mineral Resource, resulting in a significant tonnage increase, grade decrease, and more moderate increase in contained metal.
- At El Cura, the impact of pyrite concentrate production on the NSR calculation is combined with a significant expansion of the Indicated classification boundary due to new drilling.
- At La Infanta, no saleable pyrite concentrate is produced, and there has been minimal new drilling. The main driver of change is the use of an MSO reporting constraint, which has resulted in the addition of ‘must-take’ material to the MRE statement. This procedure has also been applied to La Romanera and El Cura, but the impact is less pronounced relative to other, more material changes.

Table 14-21: Percentage Change from the Previous IBW Project Mineral Resources

Deposit	Class	Tonnage (Mt)	Average Grade					Contained Metal				
			Zn (%)	Pb (%)	Cu (%)	Ag (g/t)	Au (g/t)	Zn (kt)	Pb (kt)	Cu (kt)	Ag (koz)	Au (koz)
Previous 2025 MRE												
La Romanera	Indicated	17.3	2.64	1.25	0.43	65	1.34	458	217	75	36,216	747
	Inferred	4.1	3.08	1.27	0.61	50	0.82	127	52	25	6,589	109
El Cura	Indicated	0.5	1.58	0.69	1.45	43	1.41	8	4	8	735	24
	Inferred	0.8	2.08	0.91	1.51	48	1.46	16	7	12	1,180	36
La Infanta	Indicated	1.1	7.38	4.39	1.08	95	0.35	80	48	12	3,311	12
	Inferred	1.9	4.08	2.23	0.66	74	0.38	78	42	13	4,542	23
IBW Project	Indicated	19.0	2.88	1.42	0.50	66	1.28	547	269	94	40,263	783
	Inferred	6.8	3.25	1.50	0.73	56	0.77	221	102	49	12,311	168
2026 MRE Update												
La Romanera	Indicated	22.4	2.15	1.03	0.38	53	1.10	481	230	84	38,199	792
	Inferred	6.6	2.02	0.84	0.49	33	0.57	133	55	32	7,090	120
El Cura	Indicated	2.1	1.20	0.57	0.96	30	0.98	25	12	20	2,010	65
	Inferred	0.9	0.98	0.42	0.74	19	0.62	9	4	7	556	18
La Infanta	Indicated	1.7	5.25	3.00	0.73	63	0.25	87	50	12	3,316	13
	Inferred	2.4	2.87	1.67	0.45	50	0.28	70	41	11	3,901	22
IBW Project	Indicated	26.1	2.27	1.12	0.45	52	1.04	593	292	116	43,525	871
	Inferred	9.9	2.13	1.00	0.50	36	0.50	212	100	50	11,547	161
Percentage Change (%)												
La Romanera	Indicated	29	-19	-18	-12	-18	-18	5	6	12	5	6
	Inferred	61	-34	-34	-20	-34	-30	5	6	28	8	10
El Cura	Indicated	320	-24	-17	-34	-30	-30	213	200	150	173	171
	Inferred	13	-53	-54	-51	-60	-58	-44	-43	-42	-53	-50
La Infanta	Indicated	55	-29	-32	-32	-34	-29	9	4	0	0	8
	Inferred	26	-30	-25	-32	-32	-26	-10	-2	-15	-14	-4
IBW Project	Indicated	37	-21	-21	-10	-21	-19	8	9	23	8	11
	Inferred	46	-34	-33	-32	-36	-35	-4	-2	2	-6	-4

Notes:
1. Percentage change calculated using the equation: ((2026 MRE – 2025 MRE) / 2025 MRE)*100
2. CIM (2014) definitions were followed for Mineral Resources.

2025 MRE Notes:

1. The effective date of the Mineral Resource estimate is February 26, 2025.
2. Mineral Resources are reported at a cut-off grade of 3.0% zinc equivalent (ZnEq) for La Romanera and La Infanta, and 0.9% copper equivalent (CuEq) for El Cura. Cut-off grades are based on metal price, metallurgical recovery, and preliminary operating cost assumptions (total mining, processing, and G&A cost of US$76.6/t, for underground mining and two stage mineral processing using selective copper-lead-zinc flotation and a post-flotation process).
3. Block equivalent grade calculations use factors based upon metal prices and metallurgical recoveries where:
   - La Romanera ZnEq = ((Zn*28.93)+(Pb*12.01)+(Cu*79.80)+(Ag*0.64)+(Au*45.34)/32))/0.904
   - La Infanta ZnEq = ((Zn*28.83)+(Pb*18.01)+(Cu*88.35)+(Ag*0.77)+(Au*56.51)/32))/0.901
   - El Cura CuEq = ((Zn*27.39)+(Pb*0)+(Cu*87.40)+(Ag*0.65)+(Au*45.34)/95))/0.92)
4. Metal price assumptions used in the equivalent grade calculations are US$3,200/t Zn, US$2,300/t Pb, US$9,500/t Cu, US$25/oz Ag and US$2,200/oz Au.
5. Metallurgical recovery assumptions based on available testwork results used in the equivalent grade calculations are:
   - La Romanera – 90.4% Zn, 52.2% Pb, 84% Cu, 80.1% Ag and 64.1% Au.
   - El Cura – 85.6% Zn, 0% Pb, 92% Cu, 80.6% Ag and 64.1% Au.
   - La Infanta – 90.1% Zn, 78.3% Pb, 93% Cu, 95.6% Ag and 79.9% Au.
6. All blocks less than the reporting cut-off grades when diluted over a 3 m minimum mining width were excluded from the Mineral Resources.
7. Only primary sulphide mineralisation is included in the Mineral Resources.
8. Metal grade and content are reported in situ and have not been adjusted for metallurgical recovery or mining dilution.
9. Mineral Resources are not Reserves until they have demonstrated economic viability based on a pre-feasibility study or feasibility study.
10. Numbers may not add due to rounding.

2026 MRE Notes:

1. The effective date of the Mineral Resource estimate is July 17, 2026.
2. The reporting approach is based on underground mining via long-hole open stoping, on-site selective flotation of copper, lead, zinc, and pyrite concentrates, and off-site third-party treatment and refining of the flotation concentrates.
3. Mineral Resources are reported within underground reporting shapes generated using a mineable stope optimiser (MSO) above NSR cut-off values of US$69.3/t for La Romanera, US$79.2/t for El Cura, and US$85.3/t for La Infanta. Only primary sulphide mineralisation is included in the Mineral Resource.
4. The NSR values for each block were calculated using the following formulas:
   - La Romanera – Zn(%)*US$14.72 + Pb(%)*US$6.79 + Cu(%)*US$40.39 + Ag(g/t)*US$1.10 + Au(g/t)*US$6.77 + S(%)*US$3.28
   - El Cura – Zn(%)*US$13.11 + Cu(%)*US$93.42 + Ag(g/t)*US$0.85 + Au(g/t)*US$7.15 + S(%)*US$3.33
   - La Infanta – Zn(%)*US$17.54 + Pb(%)*US$12.56 + Cu(%)*US$25.73 + Ag(g/t)*US$1.22 + Au(g/t)*US$10.52
5. Factors in the NSR formulas are based on consensus long-term metal price forecasts, metallurgical recoveries from available testwork, and market studies, used to estimate payable factors, transport, treatment and refining charges. Inputs to the block NSR calculation are specified in notes 6 through 8.
6. Mineral Resources are estimated using long-term prices of US$3,415/t Zn, US$2,425/t Pb, US$13,775/t Cu, US$65/oz Ag, US$3,500/oz Au and US$265/t pyrite concentrate (>48% sulphur).
7. The following net metallurgical recoveries have been assumed:
   - La Romanera – 78.7% Zn, 52.2% Pb, 41.5% Cu, 93.4% Ag, 89.8% Au, and 86.6% S.
   - El Cura – 67.9% Zn, 0% Pb, 79.4% Cu, 79.8% Ag, 87.4% Au, and 82.7% S.
   - La Infanta – 78.0% Zn, 78.3% Pb, 42.4% Cu, 88.2% Ag, 50.9% Au, and 0% S.
8. The following net payabilities after deductions and penalties have been assumed:
   - La Romanera – 74.6% Zn, 83.4% Pb, 79.0% Cu, 56.9% Ag, 6.7% Au, and 95.1% S.
   - El Cura – 78.4% Zn, 0% Pb, 93.3% Cu, 49.5% Ag, 7.3% Au, and 95.8% S.
   - La Infanta – 83.1% Zn, 83.3% Pb, 52.7% Cu, 66.6% Ag, 18.4% Au, and 0% S.
9. Mineral Resources are inclusive of Mineral Reserves. Mineral Resources that are not Mineral Reserves do not have demonstrated economic viability.
10. Numbers may not add or multiply due to rounding.

15.0 Mineral Reserve Estimates

15.1 Summary

The Mineral Reserve estimate for the IBW Project is prepared in accordance with Canadian Institute of Mining, Metallurgy and Petroleum (CIM) Definition Standards for Mineral Resources and Mineral Reserves (CIM 2014 definitions).

The disclosure of the Mineral Reserve estimate follows the NI 43-101 guidelines and therefore excludes Inferred Mineral Resources. As the Mineral Resource contains Indicated and Inferred material only, with no component in the Measured category, the Mineral Reserve comprises Probable Reserves only.

Mineral Reserves have been estimated for the La Romanera, El Cura, and La Infanta deposits using underground long-hole open stoping (LHOS) mining methods, with cemented paste backfill or dry rockfill. Reporting is based on NSR cut-off values of US$69.30/t for La Romanera, US$79.20/t for El Cura, and US$85.30/t for La Infanta.

The Mineral Reserves are reported and summarised in Table 15-1 and have an effective date of July 17, 2026. The reported Mineral Reserves have been used in the preparation of a mining plan, which is supported by a positive cash flow analysis.

The QP is not aware of any mining, metallurgical, infrastructure, permitting, or other relevant modifying factors that could materially affect the Mineral Reserve estimate.

Table 15-1: Summary of Mineral Reserves – July 17, 2026

Deposit	Class	Tonnage Mt	Average Grade						NSR $/t	Contained Metal					
			Zn (%)	Pb (%)	Cu (%)	Ag (g/t)	Au (g/t)	S (%)		Zn (kt)	Pb (kt)	Cu (kt)	Ag (koz)	Au (koz)	S (kt)
La Romanera	Proven	-	-	-	-	-	-	-	-	-	-	-	-	-	-
	Probable	20.4	2.19	1.05	0.38	54	1.13	36.2	189	447	214	77	35.702	738	7,377
El Cura	Proven	-	-	-	-	-	-	-	-	-	-	-	-	-	-
	Probable	1.8	1.23	0.58	1.01	31	1.01	26.3	187	22	11	18	1,794	59	474
La Infanta	Proven	-	-	-	-	-	-	-	-	-	-	-	-	-	-
	Probable	1.2	5.57	3.15	0.77	65	0.25	6.9	195	70	39	10	2,614	10	87
IBW Project	**Proven**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**
	Probable	**23.4**	**2.30**	**1.13**	**0.45**	**53**	**1.07**	**33.85**	**189**	**539**	**264**	**105**	**40,109**	**807**	**7,938**

Notes:

1. CIM (2014) definitions were followed for Mineral Reserves.
2. The reporting approach is based on underground mining using long-hole open stoping with a minimum mining width of 3.0 m, on-site selective flotation of copper, lead, zinc, and pyrite concentrates, and off-site third-party treatment and refining of the flotation concentrates.
3. Mineral Reserves are reported based on underground stope shapes generated using Deswik Stope Optimiser (DSO) and on 3D mine development shapes, which are scheduled and supported by a positive cashflow analysis. Mineral Reserves are stated above NSR cut-off values of US$69.30/t for La Romanera, US$79.20/t for El Cura, and US$85.30/t for La Infanta.
4. Mineral Reserves are estimated using long-term prices of US$2,975/t Zn, US$2,200/t Pb, US$12,120/t Cu, US$55/oz Ag, US$3,000/oz Au and US$215/t pyrite concentrate (>48% sulphur).
5. The NSR values for each block were calculated using the following formulas, with the factors based on consensus long-term metal price forecasts, metallurgical recoveries from available testwork, and market studies used to estimate payable factors, transport, treatment and refining charges:
   - La Romanera – Zn (%) *US$11.80 + Pb (%) *US$5.70 + Cu (%) *US$33.72 + Ag(g/t) *US$0.92 + Au(g/t) *US$5.68 + S (%) *US$2.43
   - El Cura – Zn (%) *US$10.63 + Cu (%) *US$81.37 + Ag(g/t) *US$0.69 + Au(g/t) *US$6.10 + S (%) *US$2.47
   - La Infanta – Zn (%) *US$14.61 + Pb (%) *US$10.93 + Cu (%) *US$18.66 + Ag(g/t) *US$0.98 + Au(g/t) *US$7.85
6. Mineral Reserves account for the following dilution:
   - La Romanera stopes– 11.2% planned dilution, 6.7% unplanned dilution
   - El Cura stopes – 19.4% planned dilution, 16.0% unplanned dilution
   - La Infanta stopes – 20.9% planned dilution, 26.7% unplanned dilution
   - Ore development – 0% dilution
7. Mining recoveries of 95% were applied in long-hole stopes, 80% in sill pillar stopes, and 100% in ore development.
8. Numbers may not add or multiply due to rounding.

15.2 Resource Model

The IBW Project Mineral Reserve estimate is based on the Indicated Mineral Resource contained in the Resource block model prepared by SLR, effective July 17, 2026. The model includes attributes for economic commodity grades, penalty-element grades, classification, material type, and density, and is described in Section 14.0.

Prior to use for Mineral Reserve estimation, all economic commodity grades for Inferred material were nullified. Penalty element grades for Inferred material were retained.

15.3 Dilution

Dilution refers to the proportion of uneconomic (or waste) material that is mixed with the ore during the process of mining. The discrimination between waste and ore is defined by the break-even cut-off value applied to the blocks.

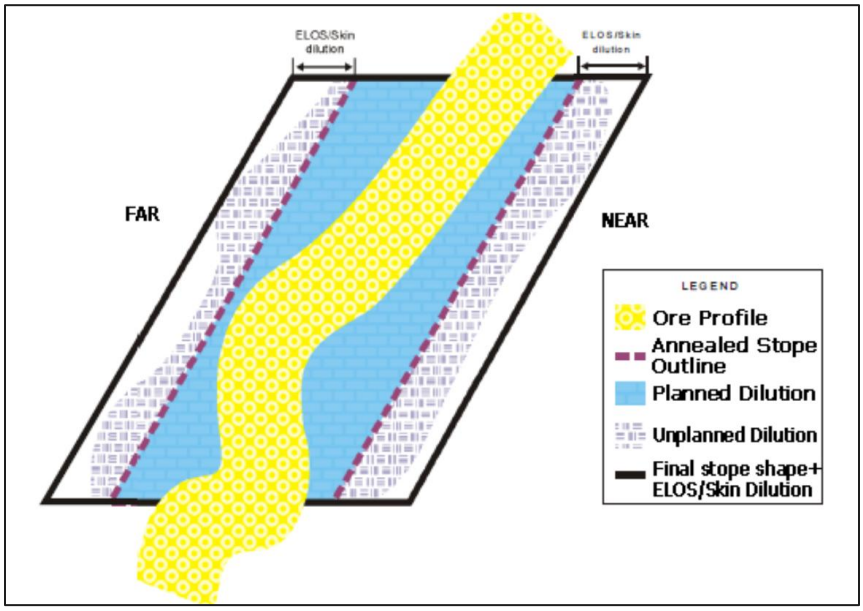
The reported Mineral Reserves are inclusive of two types of dilution:

1. Planned dilution, or internal dilution, is defined as material below the cut-off value within the planned mining shape. Planned dilution will vary for each mining shape, as dilution is a function of the localised grade distributions and mining shape geometries.
2. Unplanned dilution is defined as material originating from outside the planned limits of the defined mining shape. For stopes, an equivalent linear overbreak sloughing (ELOS) estimate was applied, which is based on geotechnical assessments conducted for each deposit (Section 16.2).

The concept of planned and unplanned dilution is illustrated in Figure 15-1, with the stope dilution summary provided in Table 15-2.

No additional dilution has been assumed for lateral development other than what is contained within the defined shape of the development round.

Figure 15-1: Schematic of Planned and Unplanned Dilution



Source: Datamine 2026

Table 15-2: Stope Dilution Summary

	Units	La Romanera	El Cura	La Infanta
ELOS Hanging Wall	m	0.50	0.50	0.75
ELOS Footwall	m	0.50	0.30	0.50
Planned Dilution	%	11.2	19.4	20.9
Unplanned Dilution	%	6.7	16.0	26.7

15.4 Extraction

All stopes generated by the Deswik Stope Optimiser (DSO) process have been evaluated and classified in accordance with the proposed mining plan. Stopes within geotechnically defined crown pillars have been adjusted or removed from the mine design and schedule, as have isolated stopes that meet the minimum NSR criteria but cannot be accessed economically.

A mining recovery factor of 95% has been applied to all production stope tonnage. An 80% mining recovery factor is applied to stopes with no access to the overcut, i.e., stopes at the crown/sill pillars. A 100% mining recovery factor is applied to all lateral ore development.

15.5 Cut-off Value

The break-even cut-off values for the La Romanera, El Cura and La Infanta deposits were evaluated by comparing the mining, processing, and on-site general and administrative (G&A) costs with the calculated NSR value for the individual Resource blocks derived from the technical and economic parameters defined for each deposit.

Table 15-3 provides the unit operating costs used to define the break-even cut-off value for each deposit. The following is noted:

- Mining costs were derived from first principles using deposit-specific engineering cost models as part of a mining study preceding the PFS;
- Process costs were estimated during the PFS work using supplier quotes and first-principles derivation; and
- G&A costs were estimated using comparable projects.

Table 15-3: Operating Costs Used to Define Break-Even Cut-Off Values

Deposit	Operating Costs (US$/t ore)			
	Mining	Processing	G&A	Total (NSR Cut-Off Value)
La Romanera	36.00	30.20	3.10	69.30
El Cura	49.00	30.20	-	79.20
La Infanta	52.00	30.20	3.10	85.30

The technical and economic parameters used to calculate NSR block values are provided in Table 15-4. Base and precious metal prices reflect consensus, long-term forecasts from banks, financial institutions, and other sources. Pyrite concentrate pricing is based on a market study for 48% sulphur pyrite concentrates (Claight 2026). Metallurgical recoveries reflect available testwork data, whilst market studies for each concentrate were used to estimate payable factors

after deductions and penalties, as well as transport, treatment, and refining charges (Cuadri y de la Corte 2025; Claight 2026).

DSO software was used to generate stope shapes, employing industry-standard algorithms to automate and optimise the delineation process. The main input parameters defined within the DSO set-up are provided in Figure 16-3. Mineralisation domain wireframes were also used as control surfaces to guide stope orientation.

Table 15-4: Mineral Reserve Estimate Technical and Economic Parameters Used for NSR Calculation

Metal Price						
Deposit	**Zn (US$/t)**	**Pb (US$/t)**	**Cu (US$/t)**	**Ag (US$/oz)**	**Au (US$/oz)**	**Pyrite Conc. (US$/t)**
All	2,975	2,200	12,120	55	3,000	215
Net Metallurgical Recovery (%)						
Deposit	**Zn**	**Pb**	**Cu**	**Ag**	**Au**	**S**
La Romanera	78.7	52.2	41.5	93.4	89.8	86.6
El Cura	67.9	0	79.4	79.8	87.4	82.7
La Infanta	78.0	78.3	42.4	88.2	50.9	-
Net Payabilities after Deductions and Penalties (%)						
Deposit	**Zn**	**Pb**	**Cu**	**Ag**	**Au**	**S**
La Romanera	74.6	83.4	79.0	56.9	6.7	95.1
El Cura	78.4	-	93.3	49.5	7.3	95.8
La Infanta	83.1	83.3	52.7	66.6	18.4	-
Selling Costs and Assumptions						
Product	**Transport (US$/wmt)**		**Treatment Charges / Refinery Charges (TC/RC) (US$/dmt or *US$/oz)**		**Moisture (%)**	
Zn Conc.	123.00		205.00		8	
Cu Conc.	123.00		100.00		8	
Pb Conc.	12.80		180.00		8	
Pyrite Conc.	9.30		50.00		8	
Au Doré	-		5.00*		-	
Ag Doré	-		0.50*		-	
Block NSR Factors (US$)						
Deposit	**Zn**	**Pb**	**Cu**	**Ag**	**Au**	**S**
La Romanera	11.80	5.70	33.72	0.92	5.68	2.43
El Cura	10.63	-	81.37	0.69	6.10	2.47
La Infanta	14.61	10.93	18.66	0.98	7.85	-

16.0 Mining Methods

16.1 Introduction

The IBW mining plan involves the combined extraction of the La Romanera, El Cura, and La Infanta deposits via long-hole open stoping (LHOS) methods, using cemented paste backfill or dry rockfill to improve mining recoveries. The plan supports a peak production rate of 1.2 Mtpa over a 20-year mine life, with 5 years of pre-development. A total of 74 km of lateral development is scheduled over the mine life, with an annual peak of just over 9 km in the year prior to production ramp-up. Summaries of the life-of-mine designs, schedules, and engineering assumptions are presented below.

16.2 Geotechnical Studies

SLR conducted a geotechnical PFS level assessment of the IBW Project (SLR 2026), covering the La Romanera, La Infanta, and El Cura underground mines. The geotechnical PFS characterised the rock mass and determined the PFS geotechnical design parameters, including:

- Stope stability design
- Stope ground support design
- Unplanned stope dilution
- Pillar widths
    - Standoff distances from stopes and infrastructure.
    - Crown pillar thickness (between underground and surface).

16.2.1 Rock Mass Characterisation

Core logging from photographs was undertaken to collect rock mass classification data using the Barton Q classification system. RQD was provided by Emerita for selected holes based on their positions throughout the orebody. Several data limitations were identified during this stage, namely:

- Photo logging was undertaken rather than physical logging;
- Limited geotechnical tests were undertaken to inform the rock mass classification, with point load tests (converted to unconfined compressive strength [UCS] values) only conducted on limited samples; and
- A detailed structural model showing large- and small-scale structures (such as faults) was not provided.

To complete the geotechnical assessment, SLR used the available data, supported by informed assumptions, to deliver the study to a PFS level of confidence and provide recommendations to improve data confidence in future studies.

Three deposits were assessed as part of the IBW Project:

- La Romanera: 70° inclined orebody extending to nearly 1,000 masl, comprised of Upper and Lower lenses, from 5 m to 35 m thickness.
- El Cura: 70° inclined orebody, typically 5 m wide to 350 m depth.

- La Infanta: three distinct orebodies North, South, and South 1, varying in inclination (average 80°) and thickness (4 m to 8 m), extending to approximately 160 masl.

Preliminary geotechnical sub-domaining was undertaken based on lithology and consolidated into similar lithological units. These lithological units have been assigned to domains representing the hanging wall (HW), orebody (ORE), footwall (FW), and other units. Geotechnical laboratory testing and joint set information were not available for all the lithologies to validate the lithological unit sub-domaining, and the QP recommends that laboratory testing be undertaken to validate or expand upon the geotechnical sub-domains and main domains.

Table 16-1 presents the rock classification values for the lower, median, and upper quartiles for each orebody.

Table 16-1: Q' Values from Geotechnical Logging of Core Photographs

Mine	Orebody	Domain	Q' Value (Lower Quartile)	Q' Value (Median)	Q' Value (Upper Quartile)
La Infanta	N	Hanging wall	2.8	7.3	12
		Orebody	3.3	9.1	27
		Footwall	3.1	7.6	17
	S1	Hanging wall	2.8	6.9	13
		Orebody	2.8	6.3	25
		Footwall	5.2	12	19
	S	Hanging wall	2.8	7.1	13
		Orebody	1.9	6.3	14
		Footwall	3.7	10.5	24
	All	Fault	0.58	1.33	7.8
La Romanera		Hanging wall	17	34	54
		Orebody	1.0	20	37
		Footwall	10.5	18	37
		Fault	0.21	0.83	2.2
El Cura		Hanging wall	11	28	37
		Orebody	5.6	14	35
		Footwall	14	28	39
		Fault	0.28	1.31	6.25

The Geomatec (2023) study included Point Load Testing (PLT) conducted on samples in the dacites, slates, tuffs, granodiorites, and rhyolites. The results of this testing were used to calculate the A Factor (rock stress factors estimated using rock strength and in situ stress) for all deposits. The QP recommends that a more comprehensive testing programme is undertaken to determine appropriate rock strength parameters for all domains. The QP also recommends additional geomechanical property testing to investigate potential variation between the La Romanera, La Infanta, and El Cura deposits.

16.2.2 Geotechnical Analyses

LHOS and cut-and-fill were the two mining methods considered for the Project. LHOS was deemed suitable for all orebodies. Cut-and-fill was also assessed by SLR (2026) as a backup if further investigations identify zones of poor ground.

LHOS stope dimensions, expected dilution, ground support requirements, and crown pillar thickness were assessed.

16.2.2.1 LHOS Stability Assessment

Stope stability was analysed using the rock mass classification data and modifying factors to determine the Stability Number (N') and appropriate hydraulic radii. Stope stability was determined by the Mathews Modified Stability Graph method. A matrix of stope-dimension options with varying hydraulic radii was produced. SLR (2026) details the stability matrices used to guide mine design, optimise level spacings and stope strike lengths to achieve the maximum stable stope dimensions.

Hanging wall dimensions were determined to ensure stable stope shapes and to highlight range(s) of potential stope geometries within the "stable" zone (as well as those requiring additional support). The stope dimensions were designed to maximise the stope size whilst remaining in the stable or transition zones of the stability graph. The DSO parameters (Table 16-2) were determined considering the mine design whilst targeting "stable" or "transitional without-support" stope shapes under lower-quartile expected ground conditions.

Table 16-2: Selected DSO Parameters

	La Infanta	El Cura	La Romanera
Level Height (m)	25	25	30
Strike Length (m)	15	20	15

16.2.2.2 LHOS Dilution

Stable hydraulic radii from the Mathews Stability Graphs were plotted against the calculated N' value on a dilution graph (after Capes 2008), which takes the lower quartile (worst case) and median Q' values, and variation of the A, B, and C factors (according to depth and orientation) across all deposits. The dilution for all mines, considering lower-quartile and median ground conditions, was up to 1 m overbreak for all stope faces. At La Infanta and El Cura, only blast damage of less than 0.5 m is expected. At La Romanera, a potentially higher dilution is expected, with an overbreak of up to 1 m.

To control very poor ground and dilution, it is expected that 25% of stopes will require cable bolt ground support to account for localised poor ground conditions below the lower quartile. SLR (2026) and the QP recommend 6 m twin-strand cable bolts on a 2.5 m x 2.5 m pattern to control localised very poor ground.

16.2.2.3 Ground Support

Ground support design classifications for development were divided into the following categories, based on the rock mass quality:

- Category 1 –Good ground (Q > 10)
- Category 2 – Poor to fair ground (1 < Q < 10)

- Category 3 – Very poor to extremely poor ground (Q < 1)

Development within the fault zone is expected in Category 2 and 3 rock, while development in the footwall and hanging wall is expected in Category 1 and 2. Unravelling failure is expected to be a major driver of instability in fault zones and foliated rock masses, so fibre-reinforced shotcrete (fibrecrete) has been used in the design of ground support for each category.

Based on SLR (2026), the QP recommends the following ground support for each category:

- Category 1 = Q >10:
  - Backs and shoulder wall support using split sets (or encapsulated rebar bolts for long-term infrastructure development) and fibrecrete (or mesh);
  - 50 mm fibrecrete thickness; and,
  - 0.40 minimum bolt density with fibrecrete (bolts/m^2) or 0.55 bolts/m^2 minimum bolt density if welded mesh is used to replace fibrecrete.
- Category 2 = 1 < Q < 10
  - Backs and mid-drift wall support using split sets (or encapsulated rebar bolts for long-term infrastructure development) and fibrecrete;
  - 50 mm fibrecrete thickness; and,
  - 0.50 minimum bolt density with reinforced shotcrete (bolts/m^2).
- Category 3 = Q <1:
  - Backs and wall support to floor using encapsulated rebar bolts and fibrecrete;
  - 100 mm fibrecrete thickness; and,
  - 0.65 minimum bolt density with reinforced shotcrete (bolts/m^2).

The QP notes that the ground support recommendations are preliminary and should be reviewed in more detail during the next study stage with additional ground characterisation, structural information for wedge analyses, and numerical modelling results.

Twin-strand cable bolts have been designed in intersections, with 3-way intersections up to 9 m span requiring 10 cable bolts at 6 m length, and 4-way intersections up to 12 m span requiring 19 cable bolts at 7 m length.

16.2.2.4 Railveyor Ramps

The inter-mine Railveyor twin ramp system was designed to connect La Romanera and El Cura to the mine surface infrastructure at La Infanta through an appropriately sized, twin underground ramp system. The design has assumed conditions similar to the footwall, with Q > 4 expected. Where ground conditions are less than designed, additional support will be required. SLR (2026) and the QP recommend that the ground support for the twin decline ramps includes:

- Backs and wall support using 3 m encapsulated rebar bolts and fibrecrete;
- 55 mm fibrecrete thickness; and
- 2 m x 2 m bolt spacing with reinforced shotcrete.

16.2.2.5 Crown Pillar Stability Assessment

A crown pillar stability assessment was undertaken using the empirical approach developed by Carter (2014) to determine the probability of failure and provide design guidelines. This approach assumes a relatively flat ground surface; however, it is considered suitable at this stage of the study. Using the assumed inputs and orebody geometries, Class E (lower quartile Q values) and Class F (median Q values) probabilities of failure and crown thicknesses are chosen as summarised in Table 16-3.

Table 16-3: Summary of Crown Pillar Thickness and Probability of Failure

Mining Area	Q Value	Crown Pillar Span (m)	Crown Thickness (m)	Probability of Failure (%)	Class
La Romanera	8	15	45	1.4	F
El Cura	2.24	5	15	2.3	E
		7	20	3.4	E
	5.6	5	15	1.1	F
		7	20	1.4	F
La Infanta	1.12	5	25	2.4	E
		7	35	3.3	E
	2.84	5	25	1.1	F
		7	35	1.3	F

16.2.3 Study Level Confidence

Based on QP's review of the available data, the current dataset positions the geotechnical model at the lower end of the data confidence typically required to support a PFS-level study. In particular, the lack of a detailed structural model for major and minor faults, limited rock strength tests, uncertainties associated with photo core logging and potential anisotropy need to be addressed. The detailed geotechnical model reliability is provided in the Geotechnical PFS report by SLR (2026). It is noted that the structural data is below PFS target confidence and additional data should be collected, while all other data sets should be expanded to achieve Feasibility Study and operational confidence levels. Geotechnical recommendations for geotechnical data collection were made to elevate the study level to PFS and FS detail.

16.2.4 Geotechnical Conclusions and Recommendations

Several risks were identified in SLR (2026), with controls designed into the mining method and mine design to mitigate the risks and recommended actions for further investigation.

The QP recommends the following to bring data confidence up to a Feasibility Study level and reduce project risk:

- Additional geotechnical drilling, logging, sampling, and testing to capture data for rock mass and structural characterisation;
- Logging and modelling of major and minor structural features to understand how structures interact with the stopes; and

- Further modelling and re-running of empirical analyses (i.e., ground support) with updated geotechnical characterisation.

16.3 Hydrogeological Considerations

16.3.1 Hydrogeological Overview

The proposed underground mining areas at La Romanera, El Cura, and La Infanta are situated within a geologically and structurally complex sequence of volcanic, volcaniclastic, and metasedimentary rocks of the IPB. No regionally significant groundwater resources have been identified within the Project permitting area. Groundwater encountered to date is associated primarily with private water supply wells and deep mineral exploration boreholes and is interpreted to occur within a series of free-flowing (artesian), confined and semi-confined fractured aquifer systems FRASA (2026).

The preliminary conceptual hydrogeological model identifies four hydrogeological systems comprising a (1) shallow, weathered (Cutaneous) system, (2) an intermediate fractured rock system, (3) a deeper mining system associated with the mineralised sequence, and (4) an underlying low-permeability basement unit. Groundwater flow within the mining horizon is interpreted to be controlled predominantly by secondary permeability associated with fractures, faults, lithological contacts, and other structural discontinuities, rather than by primary porosity. Consequently, groundwater inflows are expected to be spatially variable and concentrated where underground development intersects transmissive structural features, fractured lithological contacts, weathered zones, or historical mine workings. Relatively competent, less fractured rock masses are expected to exhibit lower hydraulic conductivity.

The principal surface water features within the Project area include the Malagón and Cobica rivers, the Albahacar and Tamujosillo watercourses, numerous seasonal drainage features, ponds and the Andévalo Reservoir. Although no direct hydraulic connection between these features and the proposed underground workings has been demonstrated, structurally controlled groundwater flow pathways may provide local hydraulic connectivity where persistent fault zones or fracture networks are present.

The conceptual hydrogeological model remains preliminary and will be refined through additional geological and hydrogeological investigations, groundwater monitoring, hydraulic testing, and numerical groundwater modelling during subsequent project phases. Baseline groundwater quality data have not yet been established and should be collected prior to construction to characterise existing conditions and support mine water management, environmental permitting, and discharge compliance.

16.3.2 Available Hydrogeological Data

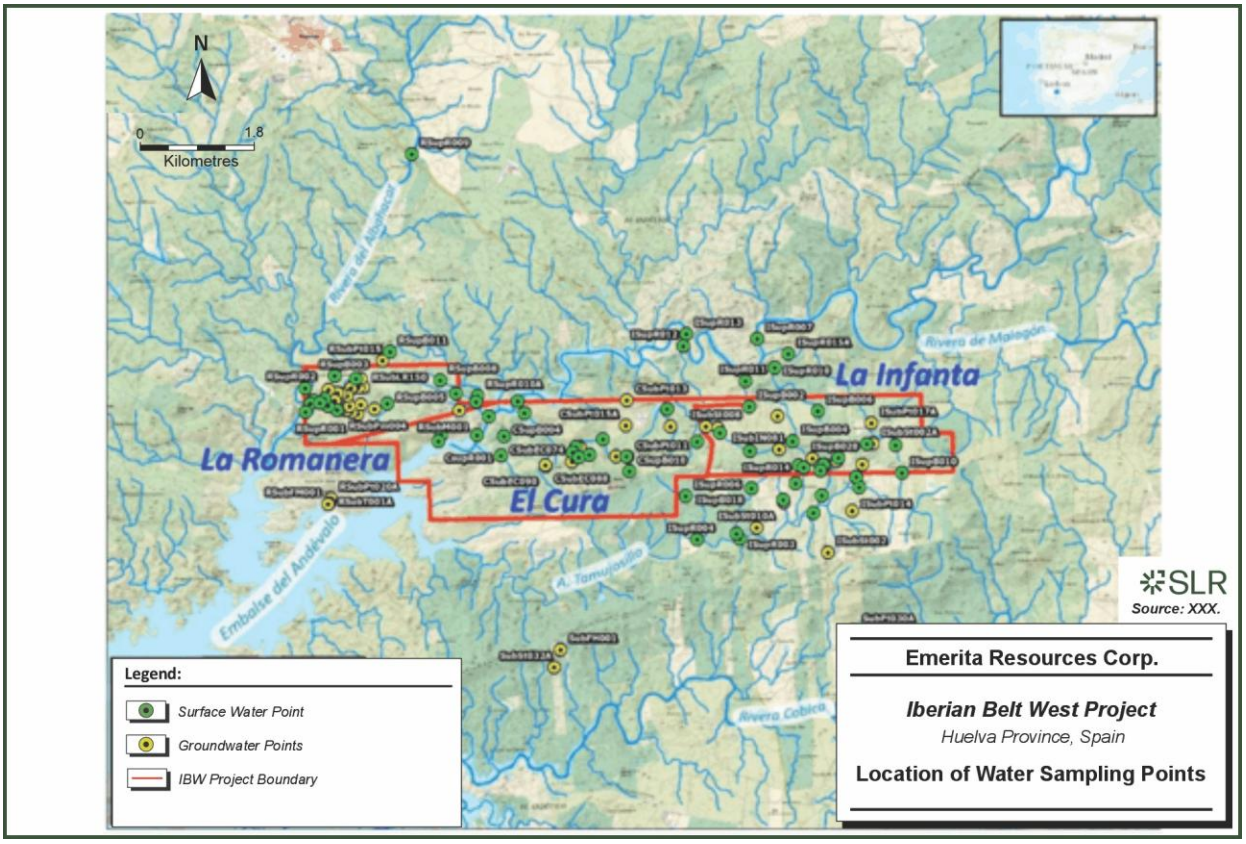
The existing hydrogeological information FRASA (2026) comprises geological and structural mapping, a record of surface water and groundwater monitoring points, one principal baseline sampling campaign undertaken between October and December 2025, and preliminary hydrological and hydrochemical interpretation. The initial monitoring network comprised 120 locations, including 67 surface water and 53 groundwater points. Field measurements were obtained from 98 locations, while samples from 96 locations were submitted for laboratory analysis. A number of monitoring points were dry during the campaign.

The available groundwater monitoring points include third-party abstraction boreholes, historical mine shafts, springs, tunnels, and mineral exploration boreholes. Many of the exploration boreholes are inclined and open across multiple lithological and structural intervals without

hydraulic isolation. Water levels and samples obtained from these boreholes therefore represent an integrated response from the intersected formations and cannot be assigned to individual hydrostratigraphic units or discrete fracture systems.

As of the effective date of this Technical Report, no site-specific hydraulic conductivity, transmissivity, or storage coefficients were available for the key geological and structural units. A representative piezometric surface has not been established, and there is insufficient time-series information to define seasonal groundwater-level variation or vertical hydraulic gradients. Consequently, the available information does not provide a sufficient basis for deterministic prediction of groundwater inflows or drawdown associated with the proposed underground workings.

Figure 16-1: Location of Water Sampling Points



Source: FRASA 2026

16.3.3 Potential Groundwater Inflows

Groundwater inflows to the underground workings are expected to comprise a combination of:

- Release of groundwater initially stored within fractures and weathered materials;
- Longer-term recharge derived from precipitation and infiltration;
- Groundwater flow along transmissive faults, fractures, and lithological contacts;
- Leakage from shallow, weathered materials and locally saturated valley deposits;

- Potential induced recharge from watercourses, ponds, or reservoirs where hydraulically connected structures are present; and
- Localised inflows from historical mine workings or previously disturbed ground.

The magnitude and duration of these components have not yet been established. Initial inflows observed during development may reflect drainage from finite fracture storage and may decline over time. In contrast, inflows associated with laterally extensive structures connected to recharge areas (boundaries) or surface water features may be more persistent. Advance development through faults, fractured zones, or historical workings may also result in localised high-rate inflows.

No numerical groundwater model or analytical life-of-mine (LOM) inflow assessment was available for the PFS. The current hydrogeological information is therefore insufficient to define expected, upper- and lower-bound, or extreme inflow rates for individual mining areas. Pump, sump, pipeline, and water treatment capacities should accordingly incorporate appropriate redundancy and contingency until site-specific hydraulic testing and predictive modelling have been completed.

16.3.4 Mine Drainage and Water Management

The preliminary mine water management strategy should prioritise the interception and controlled management of groundwater before it enters active mining areas. This is particularly important because contact between groundwater and exposed sulphide-bearing rock may result in deterioration of water quality and the generation of acidic or metal-rich mine water.

The conceptual underground water management system should include:

- Probe drilling ahead of advancing development in areas of geological or hydrogeological uncertainty;
- Advance drainage holes where persistent water-bearing structures are identified;
- Provision for local pressure relief drilling where elevated pore water pressures could affect excavation stability;
- Sumps and staged pumping systems located at appropriate underground elevations;
- Duty and standby pumping capacity, together with backup power and emergency storage;
- Separation of relatively clean groundwater, where practicable, from water that has contacted mineralised rock, waste rock, or operational areas;
- Controlled transfer of mine water to surface storage and treatment facilities;
- Monitoring of pumped flow rates, groundwater levels, and water quality; and
- Contingency measures for sealing or grouting discrete high-flow structures where drainage would cause unacceptable environmental effects or operational constraints.

Water collected through mine dewatering, together with wastewater generated by the mine water treatment system, is anticipated to be discharged to watercourses within the ZEC. As the quality and chemical characteristics of these discharges have not yet been fully defined at the PFS stage, the design and operation of the water management system should be based on the

application of the EU Environmental Quality Standards (Directive 2008/105/EC)[1] and the World Health Organisation (WHO) Guidelines for Drinking-water Quality, with the objective of maintaining receiving water quality and preserving the ecological status of downstream watercourses.

The detailed configuration and capacity of the underground mine drainage system will depend on the outcomes of additional geological and hydrogeological investigations, hydraulic testing, groundwater level and water quality monitoring, and geochemical characterisation. Consequently, the PFS design should be regarded as conceptual and should incorporate appropriate allowances for uncertainty in predicted inflows, pumping requirements, equipment redundancy, water treatment capacity, and potential delays to underground development arising from unforeseen groundwater conditions.

16.3.5 Depressurisation and Geotechnical Interaction

Groundwater pressure within faults, fractured rock masses, and lithological contacts may influence the stability and serviceability of underground excavations. The hydrogeological and geotechnical interpretations should therefore be developed concurrently. Areas where ramps, declines, access tunnels, production levels, or other infrastructure intersect major structures should be assessed for potential groundwater inflow, elevated pore-water pressure, erosion of fracture infill, and deterioration of rock mass conditions.

The available hydrogeological information does not currently allow depressurisation requirements to be established. Where elevated groundwater pressures are encountered, local drainage or pressure relief measures may be required. The design of these measures should consider both geotechnical performance and the potential environmental consequences of inducing groundwater flow from surrounding formations or surface water receptors.

Systematic recording of groundwater strikes, drilling losses, fracture conditions, inflow rates, and water quality during mine development will be required to update the hydrogeological conceptual model and refine drainage requirements. Trigger levels should be established for unexpected inflows, changes in groundwater pressure, deterioration in water quality, or responses observed at external monitoring locations.

16.3.6 PFS Limitations and Further Work

The key hydrogeological uncertainty for the proposed mining method is the potential for structurally controlled groundwater inflows and the associated connection between the underground workings and surface water receptors. This uncertainty may affect development rates, ground-support requirements, pumping capacity, water treatment requirements, operating costs, and environmental performance. The recommended investigation programme includes vertical hydrogeological boreholes at the three deposits, additional piezometers along the proposed ramp and connecting tunnel alignments, hydraulic testing of suitable site and third-party boreholes, continued groundwater-level monitoring, and flow monitoring at the La Romanera tunnel. Where practicable, testing should target discrete lithological and structural intervals rather than open boreholes that integrate multiple hydrostratigraphic units.

The resulting data should be used to:

- Define the hydrostratigraphic units and hydraulic significance of the principal structures;

[1] EU Environmental Quality Standards (EU, 2008) eur-lex.europa.eu/legal-content/EN/TXT/PDF/?uri=CELEX:32008L0105

- Establish baseline groundwater heads and seasonal variation;
- Quantify hydraulic conductivity, transmissivity, and storage;
- Assess connectivity with watercourses, ponds, and the Andévalo Reservoir;
- Develop and calibrate a 3D numerical groundwater model;
- Estimate groundwater inflows and depressurisation requirements throughout the mine life;
- Assess potential effects on external receptors; and
- Refine the design and cost of the mine drainage, pumping, storage, and treatment systems.

Until these investigations and analyses are completed, the mine inflow and drainage assumptions adopted for the PFS should be clearly identified as preliminary and supported by appropriate design and cost contingencies.

16.4 Mine Design

16.4.1 Mine Access and Mining Method

16.4.1.1 Mine Access

The IBW Project comprises three distinct deposits, the largest and most significant being the La Romanera deposit, located in the western portion of the concession area. The surface area above the La Romanera deposit is within Andévalo Occidental ZEC, which is identified as a Natura 2000 protected area. Consequently, access to La Romanera is via a 6.3 km decline from the surface industrial area adjacent to the La Infanta deposit (Figure 16-2).

The La Infanta and El Cura deposits are significantly smaller mining operations than La Romanera, but can be accessed with limited additional capital development. La Infanta is located outside the Natura 2000 area and is accessed via a short decline from the surface, approximately 1 km east of the La Romanera decline portal. El Cura is accessed directly from the La Romanera decline, 3 km from the decline portal. Figure 5-2 provides a layout of the respective mining deposits and their associated surface infrastructure.

The La Romanera decline has been designed as a twin ramp system. The southern ramp is the service decline, used to transport mobile equipment, personnel, and supplies to the mine workings. The northern ramp is the Railveyor decline, which has been chosen as the primary bulk material handling system for Emerita.

The twin ramp system was selected following a trade-off study comparing it with a single decline option, with a width sufficient to accommodate the Railveyor and service ramp requirements side by side. Although the costs of both options were comparable, the twin ramp was selected based on the following operational preferences:

- The twin ramp system provides quicker access to production areas, whereas the single ramp has comparatively slow development rates due to its large face profile.
- The twin ramp system enables simpler ventilation during decline development, eliminating the need for intermittent ventilation raises to surface as the ramp advances towards the orebody. This is especially important given the overlap of the Project

property boundary with the Natura 2000 protected area. Refer to Section 16.7.1 for further details on ventilation for the twin ramp development.

- The twin ramp system separates mobile equipment from the Railveyor infrastructure, reducing the risk of damage to the primary material handling system.
- The twin ramp system provides a means of alternate egress in case one decline becomes impassable.

Due to the shallow depth of the La Infanta deposit and the relatively short decline to the base of the deposit, a single ramp decline has been designed for the La Infanta mine with a standard 6.5 m wide profile.

16.4.1.2 Stope Access

The results of the DSO stope optimisation (described in Section 16.4.4.1) formed the basis of the underground mine design, with all mine infrastructure designed to prioritise stope access.

All mine workings stem from central declines that extend the full vertical extent of the DSO stope sets of each individual deposit. The declines are developed at a maximum gradient of 15%, with grade changes at intersections to allow efficient load-haul-dump (LHD) loading during initial development.

The mine workings consist of individual production levels set at sub-level intervals consistent with the stope geometries, which in turn reference the geotechnical design criteria. Accordingly, sub-levels are set at 30 m intervals for La Romanera and at 25 m intervals for El Cura and La Infanta.

Figure 16-2 and Figure 16-3 provide longitudinal and transverse views of the underground workings at La Romanera, respectively. Figure 16-4 provides isometric views of the El Cura and La Infanta workings. Major items of mine infrastructure have been highlighted.

Figure 16-2: Longitudinal View of the La Romanera Mine Workings

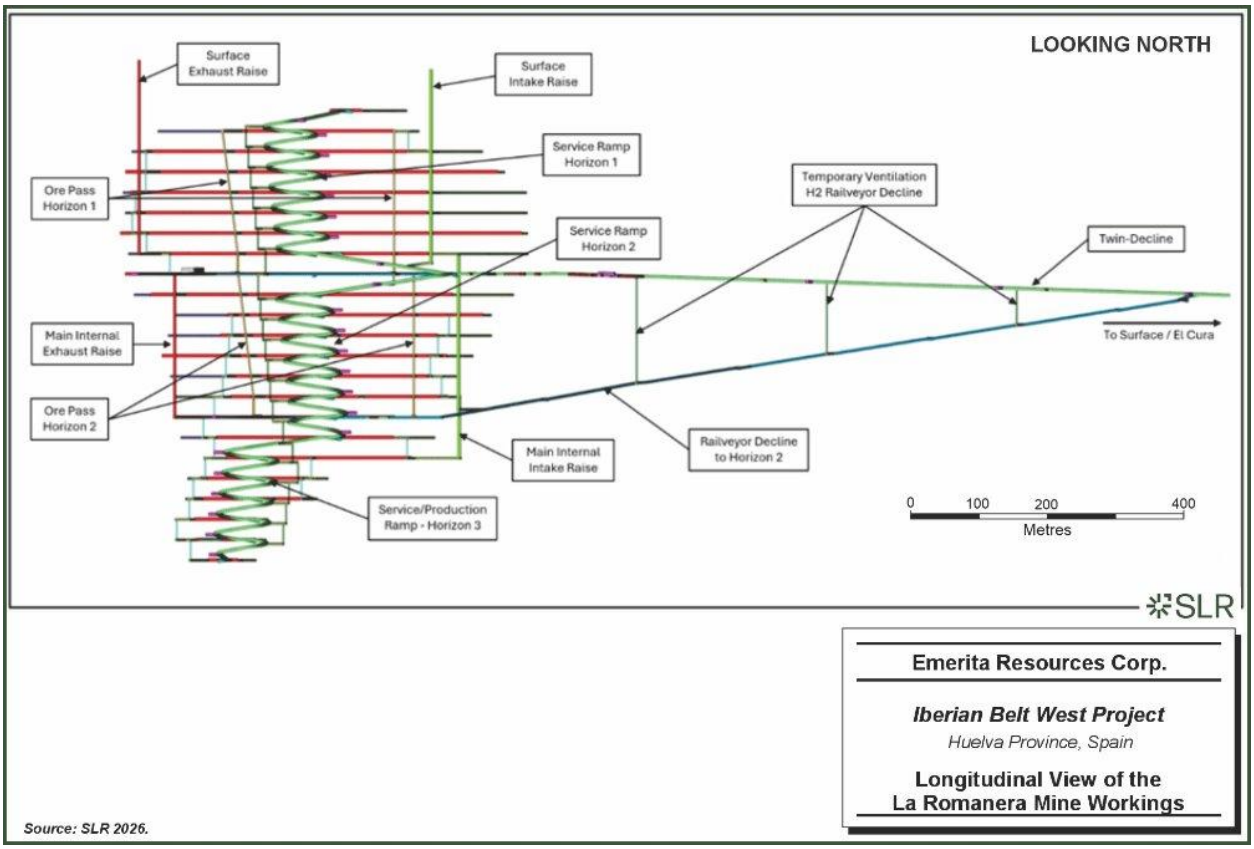


Figure 16-3: View of the La Romanera Mine Workings with DSO Stope Set

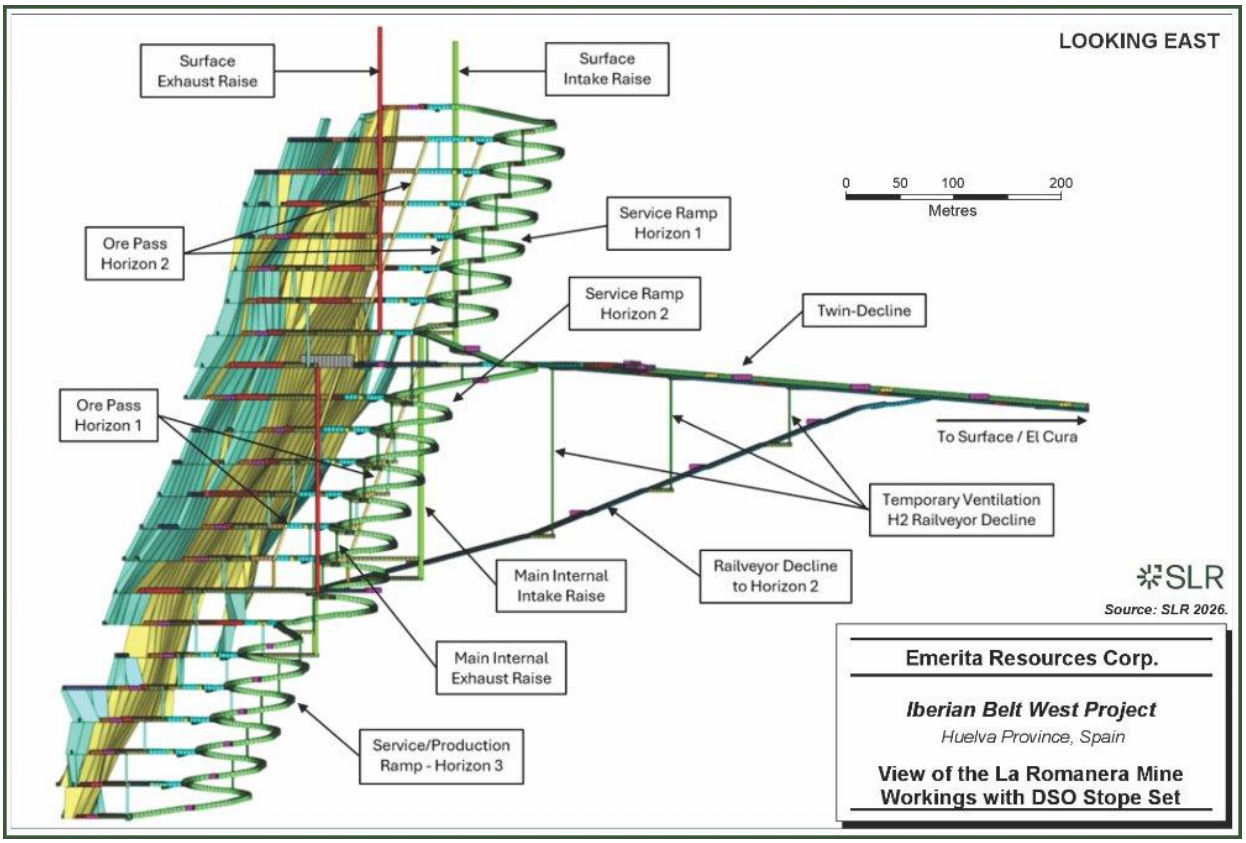
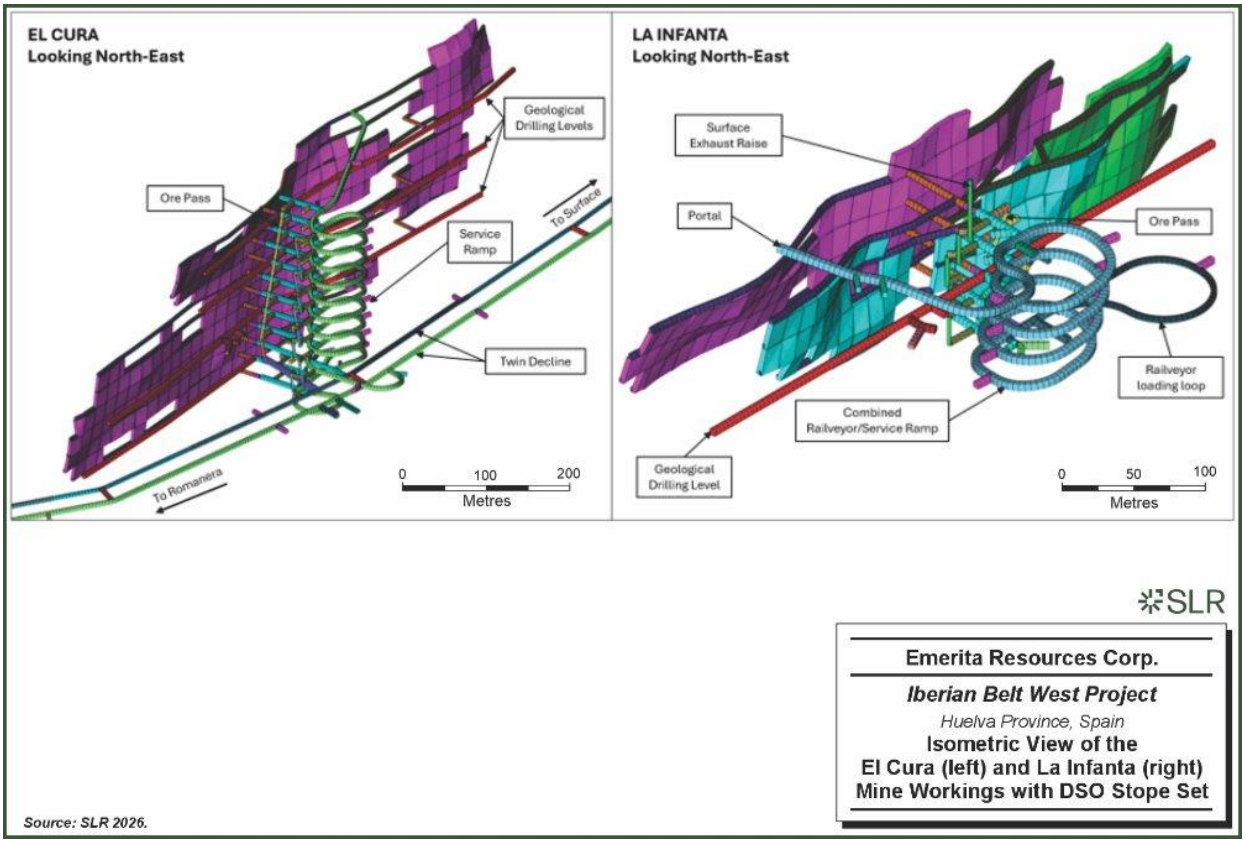


Figure 16-4: Isometric View of the El Cura and La Infanta Mine Workings with DSO Stope Set



At La Romanera, footwall development extends from the level access drives, with footwalls designed to a minimum 25 m offset from the ore zones (as per geotechnical design criteria). This distance further provides a safe and practical distance for remote LHD operation.

Footwalls drives:

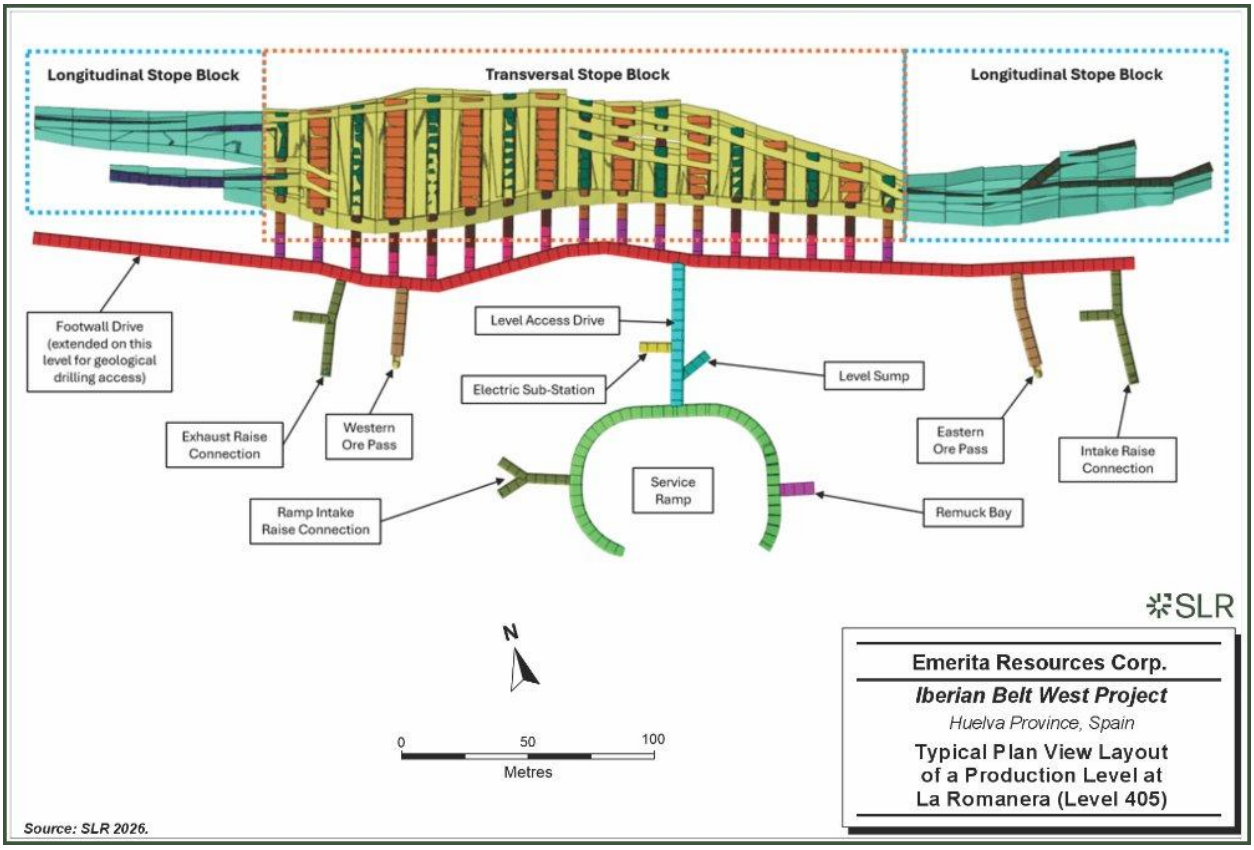
- Provide an initial geological drilling platform to accurately delineate the orebody at close spacing and from close proximity.
- Provide multiple access points to the orebody required for transverse mining.
- Enable the consistent alignment of stope access drives between levels for efficient stope sequencing of longitudinal stoping panels, and to permit flexible access points to stoping panels, thereby facilitating the creation of independent mining blocks to improve mine productivity.
- Allow ventilation and exhaust raise connections to be located at the extremities of the production levels, thus simplifying ventilation control and reducing the number of auxiliary fans required.

Footwall drives are not systematically included in the design for El Cura and La Infanta due to the limited deposit extents and the predominant longitudinal stope access requirements. However, limited footwall development has been included, primarily as a geological drilling platform, at a standoff of 20 m.

All stope access and transverse drawpoint development is driven perpendicular to the footwall drives. Longitudinal ore drives are driven from the stope access development along delineated ore zones.

Figure 16-5 shows a typical layout of a La Romanera (Level 405) production level. All production-level development will be driven at a +3% gradient to encourage water to drain back towards the level access sump.

Figure 16-5: Typical Plan View Layout of a Production Level at Romanera (Level 405)

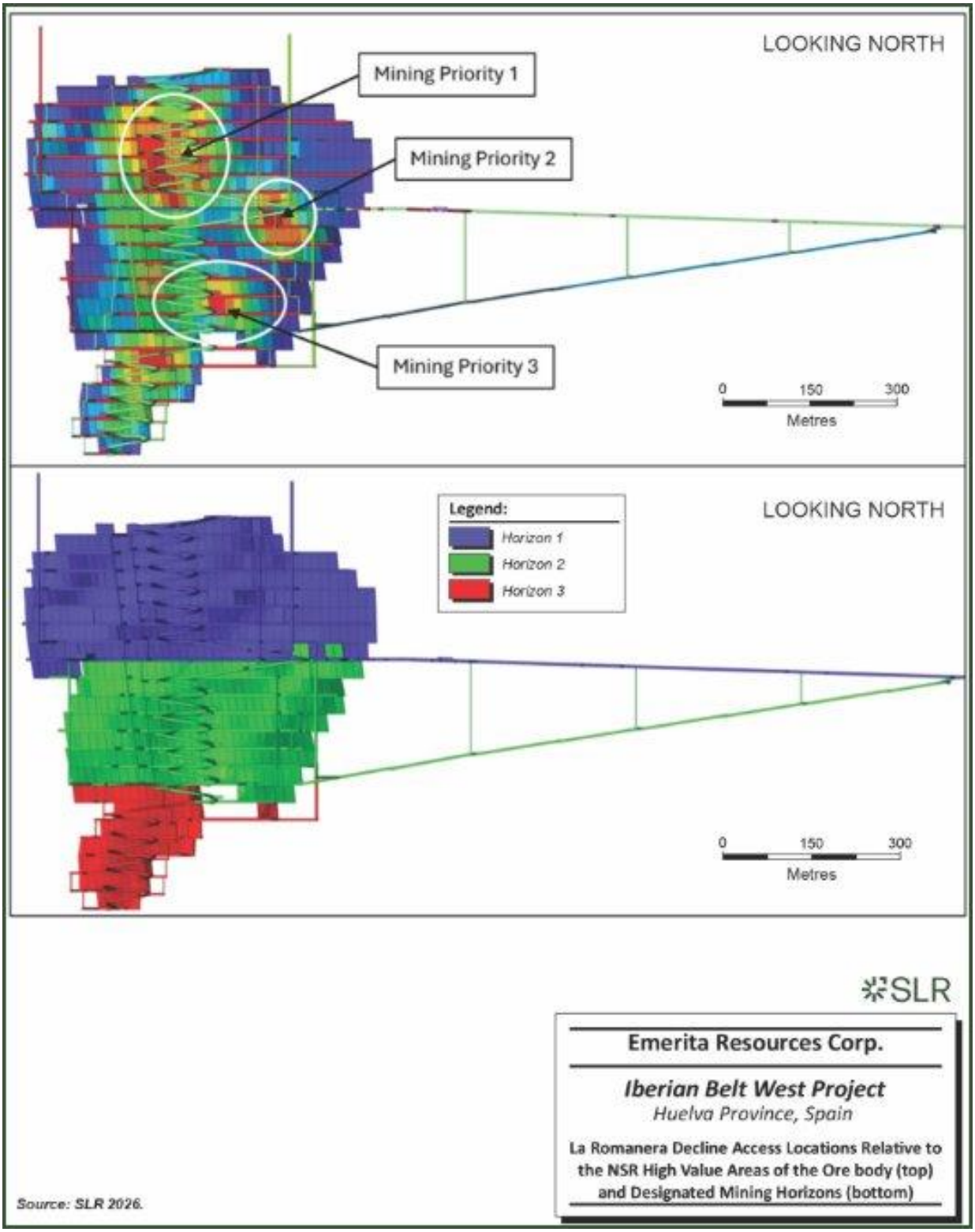


Stope access has been prioritised towards high-productivity, high-value areas of the deposits (discussed in Section 16.4.4.1 and highlighted in Figure 16-6) and has been used to define the individual mining horizons. Accordingly, the La Romanera twin decline targets the 285 level as the base of the first mining horizon, enabling early mining of the large, high-grade transverse stopes above the 285 level (Mining Priority 1) and the smaller high-grade stope block between the 275 and 285 levels (Mining Priority 2).

A second Railveyor “spur” is planned towards the 495 level to form the base of Horizon 2. The Horizon 2 Railveyor decline branches off from the twin decline at 5 km from the portal entrance and is developed as a single standard profile (Figure 16-26), with a service ramp connection to the 285 level via a spiral ramp south of the footwall development (Figure 16-3). The Horizon 2 Railveyor decline allows the prioritisation of stopes within the Mining Priority 3 area (Figure 16-6).

Although pockets of high-grade ore are present in Horizon 3, the comparatively low tonnage was not considered sufficient to warrant priority access, and so it is accessed later in the mine life via the service ramp from the 495 level.

Figure 16-6: La Romanera Decline Access Locations Relative to the NSR High Value Areas of the Orebody (top) and Designated Mining Horizons (bottom)



16.4.1.3 Mining Method

Transverse and longitudinal LHOS mining methods were selected for all Project deposits due to the orebody's shape, thickness, and orientation, as well as the geotechnical competence of the surrounding rock mass.

Cut-and-fill methods were initially considered for the La Infanta South lens due to lower geotechnical integrity; however, it was concluded that the geotechnical data were insufficient to rule out LHOS mining at this stage. The QP recommends that cut-and-fill be re-evaluated for the La Infanta deposit (or a portion thereof) as more data becomes available.

Similarly, an open-pit trade-off study was conducted for the La Infanta deposit due to its proximity to the surface and its exclusion from the Natura 2000 zone; however, high stripping ratios ultimately made underground mining preferable.

Two variations of LHOS will be utilised at the Project: transverse and longitudinal. The selected variant for a particular stope is guided by the thickness of the ore zone, with narrower stopes better suited to longitudinal mining (discussed further in Section 16.4.4.3).

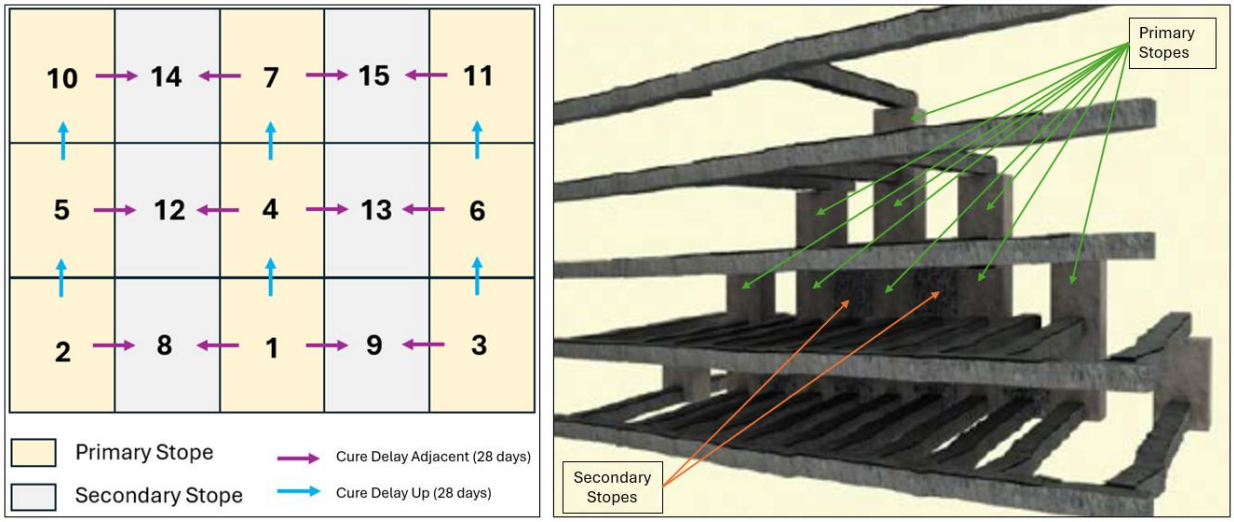
Given the value of the Project orebodies, ore recovery will be maximised by backfilling every mined stope, thereby eliminating the need for systematic geotechnical pillars. Cemented pastefill will be used as backfill in primary transversal and longitudinal stopes for the following purposes:

- Support for the rock mass.
- To provide a consolidated wall of the mining front on the production level.
- To provide a floor for the continuation of the sequence to the next level up.

Dry rockfill will be used in secondary transverse stopes and in longitudinal stopes that do not require consolidated fill.

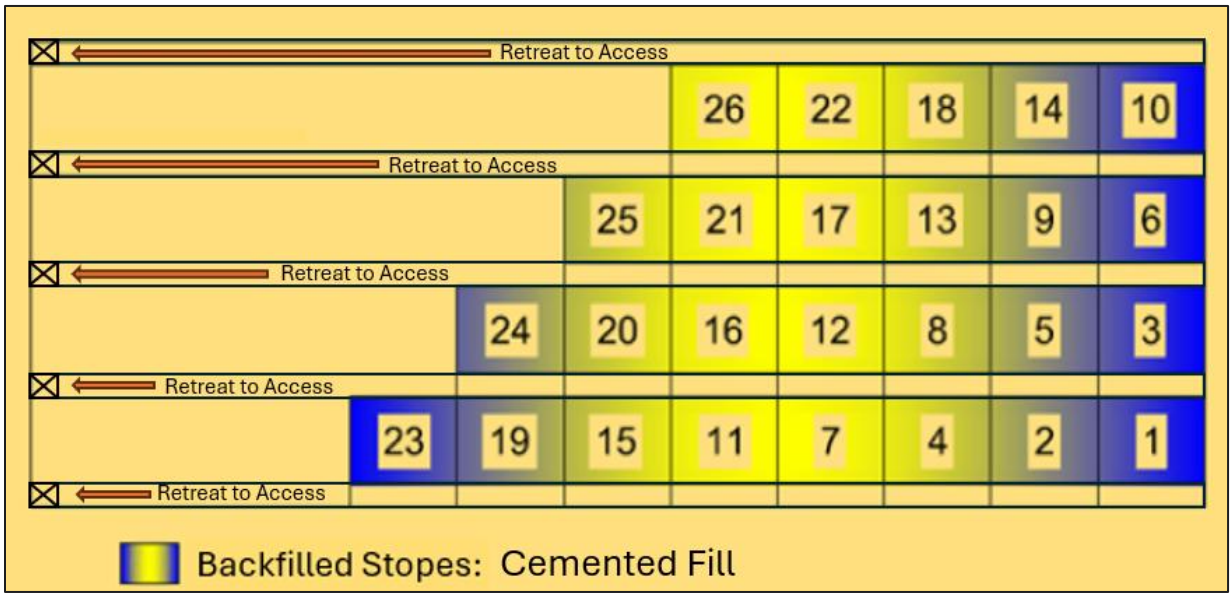
The transverse mining LHOS mining method is illustrated in Figure 16-7, and in Figure 16-8 for longitudinal mining. In both variants, top and bottom (ore drive) access is established from the sub-levels, with the top access used for production drilling (downholes) and the bottom access used for loading with LHDs.

Figure 16-7: Transverse Stope Primary-Secondary Mining Sequence (left) with Isometric Illustration of the Sequence in Progress (right)



Source: SLR 2026

Figure 16-8: Mining Sequence for Longitudinal Long-hole Open Stoping



Source: SLR 2026

A small number of primary transverse stopes are planned to be mined prior to paste plant commissioning, during which cemented rockfill (CRF) will be used as a temporary substitute for pastefill (refer to Section 16.6.4).

16.4.2 Lateral Development Design

16.4.2.1 Design

Lateral development has been sized for the operation of the selected mining feet and summarised in Table 16-4, along with the LOM development metres for each development type (Capital Expenditures [CAPEX] and Operational Expenses [OPEX]). The development has been further split according to its allocated accounting cost centre.

Table 16-4: Underground LOM Lateral Development Summary

Development Type	Profile[1] (height x width)	CAPEX (m)	OPEX (m)	TOTAL (m)
Service Decline	5.0 m x 5.0 m	14,354	-	14,354
Railveyor Decline[2]	4.0 m x 4.5 m	9,983	-	9,983
Decline Crosscut	5.0 m x 5.0 m	554	-	554
Footwall Drive	5.0 m x 5.0 m	10,327	-	10,327
Level Access Drive	5.0 m x 5.0 m	2,559	-	2,559
Remuck	5.0 m x 5.0 m	1,208	-	1,208
Electric Sub-station	4.0 m x 4.0 m	381	-	381
Level Sump	5.0 m x 4.0 m	509	-	509
Refuge Station	4.0 m x 4.0 m	82	-	82
Ore Pass Access	5.0 m x 5.0 m	1,498	-	1,498
Explosive Magazine	4.0 m x 5.0 m	207	-	207
Ventilation Access	4.0 m x 4.0 m	2,679	-	2,679
Longitudinal Ore Drive	4.0 m x 4.0 m	-	11,026	11,026
Transversal Drawpoint[3]	4.0 m x 4.0 m	3,824	3,289	7,112
Transversal Sill - Primary	4.0 m x 9.0 m	-	7,095	7,095
Transversal Sill - Secondary	4.0 m x 5.0 m	-	4,138	4,138
Pump Station	Var.	419	-	419
Maintenance Bay	Var.	243	-	243
Total		**48,825**	**25,547**	**74,372**

Note:

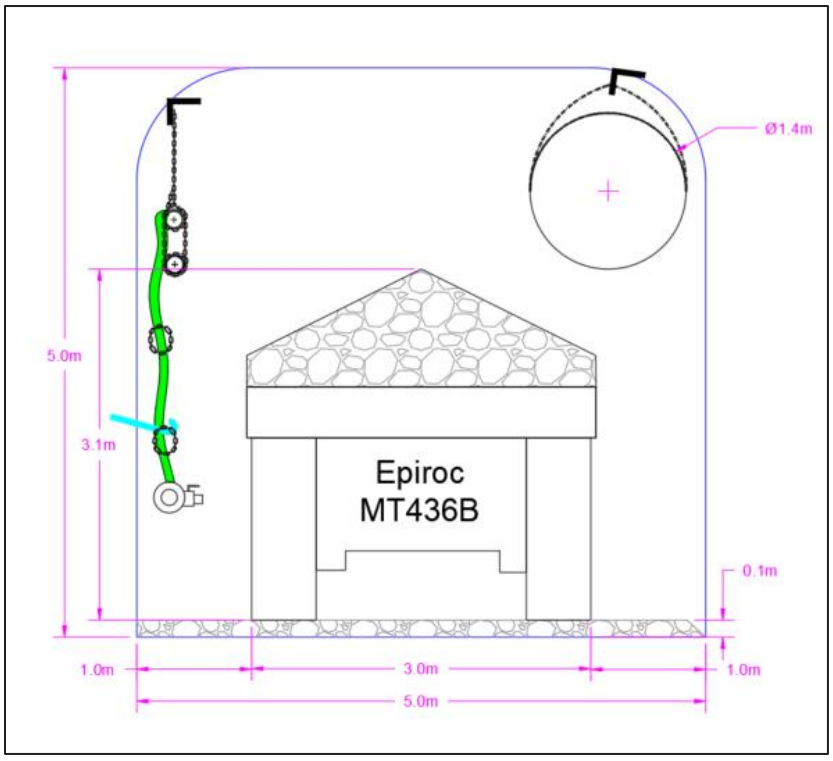
1. All profiles are designed with a flat arched back with shoulders at a 1.0 m radius.
2. The Railveyor decline profile varies along its length from the nominal 4.0 mH x 4.5 mW profile to accommodate drive stations and bypasses. Design variances have been included in the Deswik design model.
3. A Transversal Drawpoint is considered OPEX if it serves two stopes (or less), i.e. it provides drilling access for the stope below, and mucking access for the stope above. If a Transversal Drawpoint serves more than two stopes (due to stacked zoning), it is considered CAPEX due to the comparative longevity of its required use.

All main CAPEX development (declines, level access drives, footwall drives, and crosscuts) must accommodate the largest items in the mining fleet and provide clearance for mine services. All such development is therefore designed according to the schematic shown in Figure 16-9 which includes a loaded haul truck in profile as the largest equipment item to be used at the Project.

Ore drive and transversal drawpoint development has been sized according to indicative drill-and-blast design work (refer to Section 16.4.4.3), and to accommodate the selected production loader. The development profile is shown in Figure 16-10.

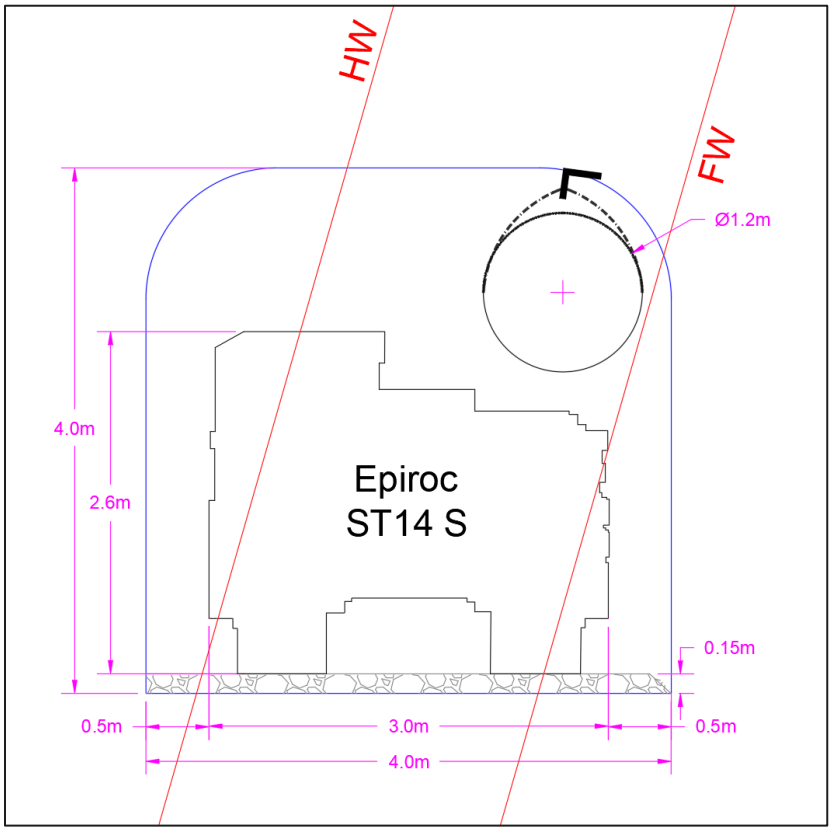
All other drifts are designed to a minimum height of 4 m, dictated by the required operating dimensions of the selected bolting rig for installing a 2.4 m bolt.

Figure 16-9: Schematic Cross-sectional Profile of a CAPEX Heading with a MT436B Haul Truck



Source: SLR 2026

Figure 16-10: Schematic Cross-sectional Profile of an Ore Drive / Drawpoint Heading with an ST14S LHD



Source: SLR 2026

Whilst Horizon 1 and 2 of La Romanera, as well as El Cura and La Infanta, are served by ore/waste pass infrastructure for transporting material to the Railveyor loading points, the Railveyor was not extended to the base of Horizon 3 in the PFS design, as doing so would require significant additional CAPEX for limited tonnages towards the end of the mine life. Ore and waste from Horizon 3 will therefore be transported by haul trucks loaded in the footwall drives at designated intersections, or “charging points”, which are backslashed to accommodate the selected equipment.

16.4.2.2 Reporting

Lateral development metres noted in Table 16-4 have been converted to “equivalent metres” based on a 5.0 mH x 5.0 mW reference tunnel profile, i.e. reported relative to tunnel volume rather than linear extent. CAPEX metres also include a 5% development contingency factor to account for any additional development not included in the Deswik design model. Such items include the backslashes and corner fillets described in this section, as well as safety bays, geological drill bays, service cut-outs, and any supplemental mine infrastructure not considered within the PFS mine design[2].

[2] Lateral development is also scheduled according to the equivalent metre value to account for the impact of tunnel profile on advance rate. Scheduling also considers the 5% CAPEX contingency.

Lateral development has been interrogated using 4.0 m round advance lengths. The round length is derived from the 4.3 m feed length of the selected face drill rig (Epiroc S2 Boomer) with a 0.3 m holdback.

All lateral development tonnages are reported with 0% additional dilution and 100% mining recovery. Any development within mineralised material is directly interrogated against the Resource model without further adjustment. Any waste material within the individual round lengths is treated as internal dilution, and the round is reported as waste if the NSR falls below the cut-off value. The dilution and ore loss assumptions reflect the operational requirement that all tunnels be excavated to the design profile to limit cost overruns (from overbreak) or to avoid compromising equipment clearance tolerances (from underbreak).

16.4.3 Vertical Development Design

Vertical capital development is required to provide and distribute ventilation to the underground workings, to transport material to the Railveyor loading points, and to install ladderways for secondary mine egress. Ventilation raises are sized to accommodate the required volumetric flow rates (Section 16.7.1), ore passes are sized to avoid material hang-ups (Section 16.7.3), and manway raises are sized to accommodate the manway specification (Section 16.7.11).

Table 16-5 provides a LOM summary of the major raise infrastructure required at the Project, with all excavations to be carried out by raise boring. In addition to the infrastructure outlined in Table 16-5, drop raises between adjacent levels are required as local ventilation connections throughout the mine workings and are considered capital development. These drop raises are to be constructed using longhole drill-and-blast techniques.

Table 16-5: Raise Bore Vertical Development Summary

Deposit	From (RL)	To (RL)	Description	Diameter (m)	Length[1] (m)	Construction Year
La Romanera	Surface	255	Intake	5.0	273	-2
	285	495	Intake	5.0	192	-1
	255	285	Intake	5.0	26	1
	Surface	255	Exhaust	4.0	285	-1
	255	495	Exhaust	4.0	206	4
	75	285	Ore Pass H1 East	3.0	213	-1-4
	75	285	Ore Pass H1 West	3.0	213	-1-4
	285	495	Ore Pass H2 East	3.0	213	5-6
	285	495	Ore Pass H2 West	3.0	213	5-6
	285	375	Connection 1 for Railveyor decline advance (temp)	1.8	49	-2
	285	405	Connection 2 for Railveyor decline advance (temp)	1.8	101	-2

Deposit	From (RL)	To (RL)	Description	Diameter (m)	Length[1] (m)	Construction Year
	285	435	Connection 3 for Railveyor decline advance (temp)	1.8	152	-1
	75	285	H1 Intake for Service ramp advance	1.8	203	-1-6
	285	495	H2 Intake for Service ramp advance	1.8	215	-1-5
	495	675	H3 Intake for Service ramp advance	1.8	168	11-16
El Cura	145	370	Ore Pass	3.0	220	-2-5
La Infanta	Surface	150	Intake	3.0	142	9-10
	50	150	Ore Pass	3.0	92	10

Notes:
1. Length depicts total length. In some instances, identified raises will be constructed in multiple sections.

The locations of the raises must be confirmed through additional geotechnical drilling before excavation. Similarly, the requirement for ground support within the larger raises is subject to further geotechnical investigation.

16.4.4 Stope Design

16.4.4.1 Stope Optimisation

DSO software was used to create optimised stope shapes, employing industry-standard algorithms to automate and optimise the stope delineation process.

The main input parameters defined within the DSO set-up are provided in Table 16-6 and ensure that optimisation results respect the Project's economic and technical constraints. Additionally, mineralisation domain wireframes were used as control surfaces to guide stope orientation.

Table 16-6: DSO Inputs for Underground Stope Delineation

MSO Parameter	Units	Value			Source/Comment
		La Romanera	El Cura	La Infanta	
Cut-Off Value	US$	69.3	79.2	85.3	Refer to Section 15.5.
Minimum Mining Width	m	3.0	3.0	3.0	Engineer experience / global benchmarking.
Width Type	m	True	True	True	Permits stope width to be independent of stope dip.
Hanging Wall Dilution	m	0.50	0.50	0.75	Geotechnical design criteria recommendation (Section 16.2.2).

MSO Parameter	Units	Value			Source/Comment
		La Romanera	El Cura	La Infanta	
Footwall Dilution	m	0.50	0.30	0.50	Geotechnical design criteria recommendation (Section 16.2.2).
Stope Height (level spacing)	m	30.0	25.0	25.0	Geotechnical design criteria recommendation (Section 16.2.2).
Stope Length (along strike)	m	15.0	20.0	15.0	Geotechnical design criteria recommendation (Section 16.2.2).
Maximum Mining Width	m	100.0	100.0	100.0	Unconstrained. Reflective of the general stability of the mineralised host rock at the selected stope length.
Minimum Pillar Between Parallel Stopes	m	6.0	6.0	6.0	Geotechnical design criteria recommendation.
Framework Slice Method	Type	Vertical XZ	Vertical XZ	Vertical XZ	Dictated by orebody geometry.
Z Axis Rotation	Deg.	16	342	0	To permit stope shape generation aligned with orebody strike.
Sub-Shapes	Type	None	U2, V1	U2, V1	Half-stopes permitted along strike length (U) for El Cura and La Infanta are easily accommodated with longitudinal mining. Not considered at La Romanera due to the defined transversal interval. No half-stopes permitted on stope height (V).

Metal and sulphur grades for all Inferred Resources were set to zero in the Resource model prior to running the DSO optimisation. All Inferred and non-classified material is thus treated as waste, ensuring that no economic value is considered for subsequent mining plans or attributed to the project economic evaluation.

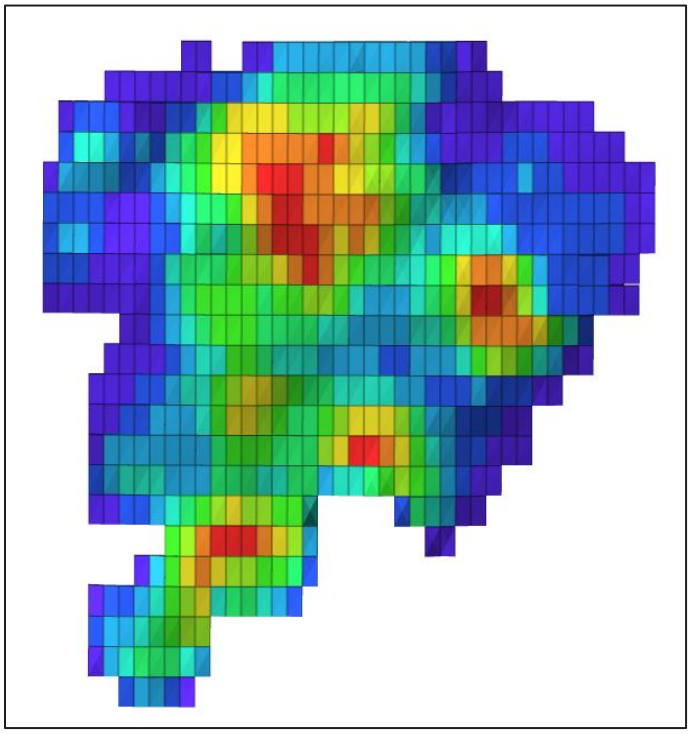
The following summarises the DSO output per deposit:

- **La Romanera:** A total of 800 economic DSO shapes were generated over a strike length of 600 m running east to west, with a vertical extent of 660 m, dipping on average at 70° to the north.
- **El Cura:** A total of 233 economic DSO shapes were generated, including nine half-stopes (along strike) deemed suitable for integration into the global stope set. The stopes were generated on a total strike length of 700 m running east to west, with a total vertical extent of 350 m, dipping at an average of 70° to the north.

- **La Infanta:** A total of 233 economic DSO shapes were generated, including nine half-stopes (along strike) deemed suitable for integration into the global stope set. The stopes were generated over a total strike length of 770 m running east to west, with a total vertical extent of 175 m, dipping at an average of 60° to the north.

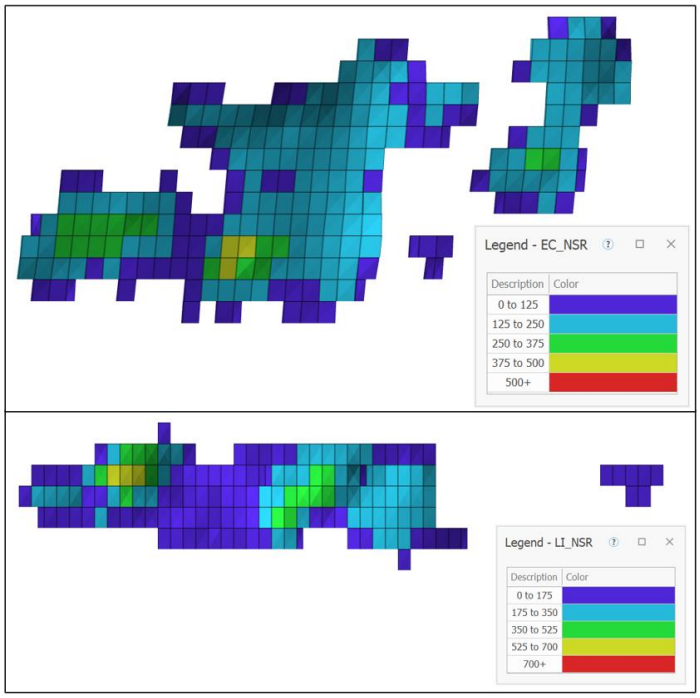
Figure 16-11 shows the global NSR distribution across the entire La Romanera deposit, with areas of high NSR concentration highlighted as “hot spots”. Figure 16-12 presents a similar view for the El Cura and La Infanta deposits; however, both stope sets show a relatively consistent NSR distribution.

Figure 16-11: La Romanera DSO Optimisation Results Global NSR Distribution (looking north)



Note: Red “hot spots” show areas of high concentration of deposit NSR value.

Figure 16-12: El Cura (top) and La Infanta (bottom) DSO Optimisation Results Showing Stope NSR per Tonne (looking north)



The following observations are made from the La Romanera stope optimisations:

- Approximately 29% of the mineable tonnage and 26% of the NSR value are contained within stopes of 12 m width or less, which have been regarded as more suitable for longitudinal retreat mining for the purpose of the PFS.
- The majority of stopes 12 m wide or less lie at the extremities of the orebody, with some correlation between increasing stope width and grade, concentrated around isolated ore pockets.
- Internal dilution percentage is higher in narrower stopes, with a rapid decline as stope width increases.

Figure 16-13 and Figure 16-14 provide the distribution of minable tonnage and global NSR, respectively, for the La Romanera deposit. The respective stope inventories for El Cura and La Infanta exhibit a much-reduced variation in stope width (predominantly less than 8 m), with minimal correlation between stope width and NSR.

Figure 16-13: Romanera DSO Tonnes Distribution by Stope Width

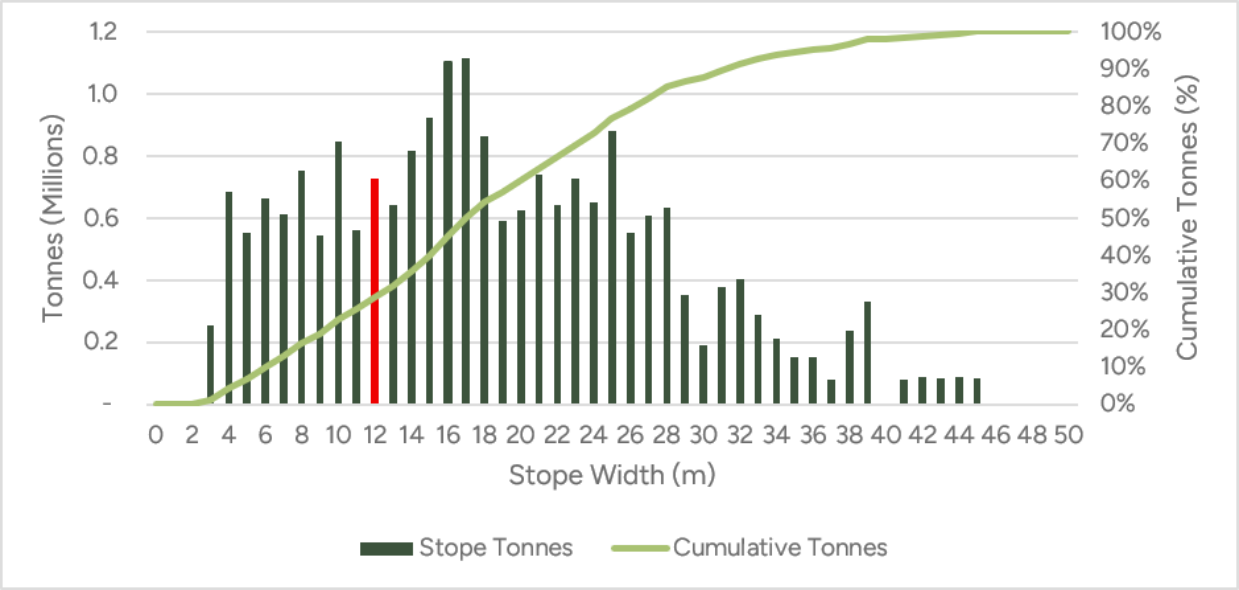
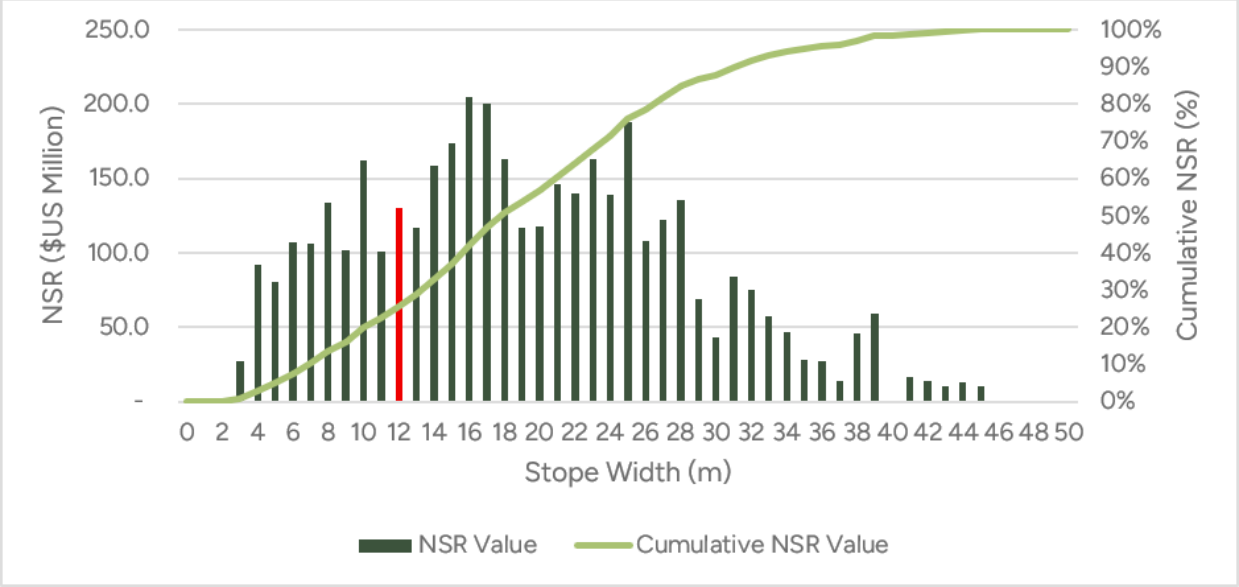


Figure 16-14: Romanera DSO Global NSR Distribution by Stope Width



With most of the production tonnage and NSR value concentrated in the wider, more centralised areas of the orebody, transverse mining will dominate at La Romanera, supplemented by longitudinal retreat at the narrow extremities of the deposit. Early production will focus on stope blocks that show a correlation between high tonnage and value per tonne (i.e., NSR hot spots) to maximise project net present value (NPV) and facilitate operational ramp-up. Lower value and/or narrower longitudinal retreat areas will be blended into the production feed throughout the LOM to limit the impact of dilution tonnes on the process feed.

El Cura and La Infanta will be mined bottom-up in their natural mining sequence. Higher-grade areas will be prioritised as far as practicable.

16.4.4.2 Stope Selection

Upon completion of the DSO optimisation, the resulting stope shapes were individually assessed for inclusion in the final stope set. Stopes were rejected if any of the following conditions were met:

1 Stopes are present within the recommended crown pillar (Section 16.2.2.5).

2 Stopes cannot be accessed economically.

Under condition 1, stopes that partially cross the recommended crown pillar boundary were trimmed to the boundary and re-interrogated for economic value. All such stopes will be mined from the level below, as no top access is possible without entering the crown pillar.

Under condition 2, projected gross revenues and mining costs for isolated stopes were estimated using the criteria in Table 15-3 and Table 15-4. Stopes were ultimately rejected if the capital cost of stope access exceeded net revenues.

A summary of the rejected MSO stopes is provided in Table 16-7.

Table 16-7: DSO Stope Inventory Tonnage Summary

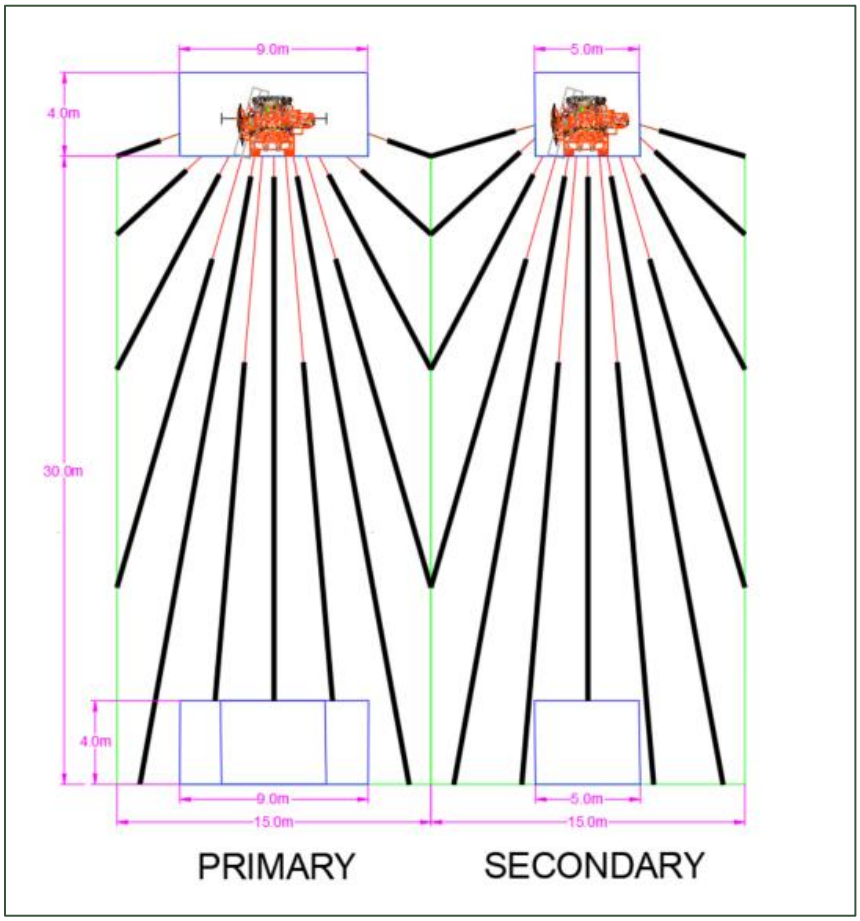
Criteria	Units	La Romanera	El Cura	La Infanta
DSO Output	t	21,495,451	1,889,739	1,445,212
Sub-Stope Addition	t	-	27,863	25,038
Sub-Total: Stope Tonnage Input	**t**	**21,495,451**	**1,917,602**	**1,470,250**
Lost to Crown Pillar	t	32,104	-	95,210
Uneconomical Access	t	-	40,176	50,166
Sub-Total: Stope Tonnage Excluded	**t**	**32,104**	**40,176**	**145,376**
Total: Stope Inventory	**t**	**21,463,347**	**1,877,426**	**1,324,874**

16.4.4.3 Drill-and-Blast

Drill-and-blast designs have been developed in accordance with the defined stope geometries and are used to calculate estimation factors for subsequent mine scheduling and to provide a basis for selecting appropriate production drilling equipment and for cost estimation.

The majority of the La Romanera deposit will be mined using transverse access drives for LHOS, with stopes transitioning to longitudinal access at a nominal true width of less than 12 m. An indicative transverse drill-and-blast design is provided as Figure 16-15 and shows the adjacent primary and secondary stopes.

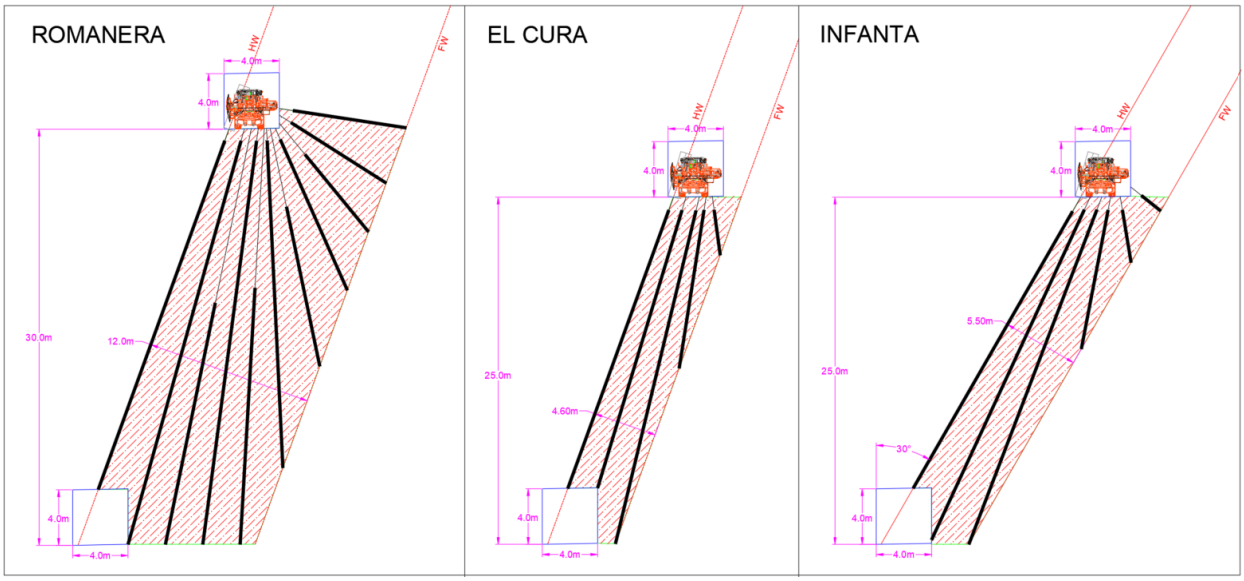
Figure 16-15: Drill-and-Blast Design for an Adjacent Transversal Primary and Secondary Stope at La Romanera



Source: SLR 2026

Figure 16-16 provides the longitudinal stope designs, which assume the average dip of the DSO stope sets per deposit. Stope widths are also taken from the average for the DSO stope sets, except for La Romanera, where a 12 m width was assumed for conservatism in the drill-and-blast assumptions.

Figure 16-16: Drill-and-Blast Designs for Longitudinal Stopes at Each Deposit



Source: SLR 2026

A summary of the drill-and-blast design parameters used is provided in Table 16-8.

Table 16-8: Drill-and-Blast Design Parameters

Parameter	Transversal	Longitudinal La Romanera	Longitudinal El Cura	Longitudinal La Infanta
Explosive Type	Bulk Emulsion			
Explosive Density (g/cm³)	1.20			
Orebody width used for indicative design (m)	N/A	3.25	4.75	6.25
Orebody dip used for indicative design (°)	70	70	70	60
Ore Drive / Transversal Sill Height (m)	4.0	4.0	4.0	4.0
Ore Drive / Transversal Sill Width (m)	9.0	4.0	4.0	4.0
Hole Diameter (mm)	89	89	89	89
Toe Burden (m)	2.7	2.7	2.8	3.0
Ring Spacing (m)	2.2	2.2	2.4	2.5
Design Drill Factor (tonnes per meter drilled)[1]	16.6	14.7	12.2	11.3
Design Powder Factor (kg/tonne blasted)	0.37	0.48	0.58	0.62

Note:
1. Calculated drill factors include a 5% contingency factor for hole cleaning, and a 10% contingency factor for re-drilling.

16.4.4.4 Dilution and Recovery

Stope dilution factors are outlined in Sections 15.3 and 16.4.4.1, with global dilution values from the respective DSO stope sets summarised in Table 16-9.

An ore loss of 5% is assumed as standard across all stope production tonnage, with an additional 15% ore loss assumed for stopes with no access to the overcut, i.e., drilled with uppers. Such stopes are present at the base of the crown pillar or beneath the sill pillar from the preceding mining horizon above. The reduction in recovery reflects the technical challenges of achieving consistent drill-and-blast results without access to the breakthrough location.

Table 16-9: Stope Dilution and Mining Recovery Summary

Types of Dilution and Recovery	La Romanera	El Cura	La Infanta
Planned Dilution	11.2%	19.4%	20.9%
Unplanned Dilution	6.7%	16.0%	26.7%
Stope Recovery	95%	95%	95%
Stope Recovery Beneath Pillars	80%	N/A	80%

As discussed in Section 16.4.2.2 all lateral development is reported with 0% additional dilution and 100% mining recovery.

16.5 Life of Mine Plan

16.5.1 Overview

A production rate of 1.2 Mtpa is required of the IBW Project to meet the design capacity of the process plant. This production rate forms the basis for all mine scheduling work.

The following sections describe the results of the production planning and optimisation process undertaken to ramp up to the required production rate as soon as practicable and to sustain that rate for a prolonged period. It has been considered that the defined production rate is achievable, subject to a reasonable allocation of mining resources appropriate to the type and size of the deposits.

Data tables and charts presented within this section are generally applicable to all deposits combined (La Romanera, El Cura, and La Infanta), unless otherwise stated.

16.5.2 Lateral Development

The lateral development cycle incorporates drilling, blasting, mucking, hauling, scaling, ground support installation, and the advancement of mine services. An advance rate of 4.0 m per cycle is assumed based on the defined specification and set-up of the development drill, with the total development cycle time being a function of the cumulative duration of each element within the cycle.

All mine development is scheduled according to priority. In general, the highest priority development concerns the critical infrastructure necessary to sustain operational activities. Thereafter, priorities follow demand to generate and sustain an optimised mine production profile, with areas of high value accessed as soon as feasible to generate NPV.

The lateral development schedule for the Project uses up to three operable development drills (Jumbos) over the LOM, with each Jumbo allocated to headings within spatially consistent

areas of the mine workings to avoid excessive and unproductive travel between active headings:

- **Jumbo 1:** Allocated to La Romanera service ramp development from the surface down to the 285 level, and to La Romanera Horizon 1 development thereafter.
- **Jumbo 2:** Allocated to the La Romanera Railveyor decline from the surface and to La Romanera Horizon 2 and Horizon 3 development thereafter.
- **Jumbo 3:** Allocated to El Cura, moving to La Infanta once El Cura is fully developed.

Each Jumbo is assigned a maximum capacity of 300 m of lateral advance per month (or 3.6 km per year), which is split across multiple headings; the advance rate of a particular heading is partly defined by its individual urgency. The total development capacity per Jumbo is largely determined by the following assumptions:

- **4 x headings @ 75 m per month advance:** Used to focus development of critical infrastructure during the pre-production years (i.e., advancement of decline, establishing ventilation connections, etc.) and to access the first stopes as soon as possible to enable early production ramp-up.
- **6 x headings @ 50 m per month advance:** Used as the default rate for the remainder of the LOM.
- Longitudinal ore drive development is limited to 25 m per month to allow for grade control activities and directional geological control of the mining front.

In addition to the above, the initial service ramp and Railveyor decline advancement from surface (Phase 1 development) are assigned an advance rate of 100 m to 150 m per month. This rate is applied on the understanding that the advancement of these priority headings is the only consequential activity within the mine during this operational phase and can therefore be immediately resourced at all points in the development cycle, with blasting permitted at any time of day. During Phase 1, total Jumbo capacity is allocated as follows:

- **225 m per month:** Primary face @ 100 m per month, with secondary and tertiary development headings allocated 75 m and 50 m per month, respectively; or
- **150 m per month:** All Jumbo capacity is allocated to the primary face @ 150 m per month.

Figure 16-17 provides the LOM-scheduled development metres for each mining Phase/Horizon at La Romanera, as well as for El Cura and La Infanta (Jumbo 3). Table 16-10 further provides the annual breakdown of development metres by cost centre.

Figure 16-17: LOM Development Metres Distribution

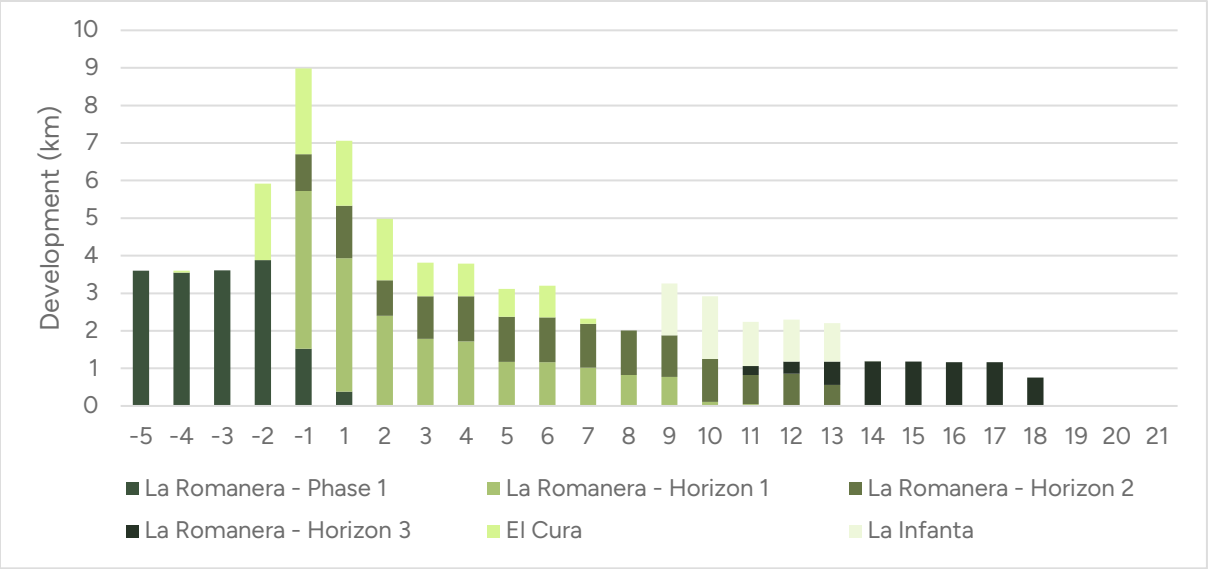


Table 16-10: LOM Development Scheduled Metres Split by Cost Centre

Year	CAPEX (m)	OPEX (m)	TOTAL (m)
-5	3,598	-	3,598
-4	3,598	-	3,598
-3	3,607	-	3,607
-2	5,915	-	5,915
-1	7,214	1,751	8,965
1	4,785	2,275	7,060
2	2,952	2,031	4,983
3	2,465	1,346	3,811
4	2,544	1,248	3,792
5	1,841	1,274	3,116
6	1,314	1,884	3,197
7	231	2,094	2,325
8	322	1,686	2,008
9	1,948	1,316	3,265
10	2,158	762	2,920
11	642	1,594	2,236
12	330	1,970	2,299
13	288	1,920	2,208
14	881	322	1,203
15	917	264	1,180

Year	CAPEX (m)	OPEX (m)	TOTAL (m)
16	752	414	1,166
17	375	793	1,168
18	150	603	753
19	-	-	-
20	-	-	-
21	-	-	-
TOTAL	**48,825**	**25,547**	**74,372**

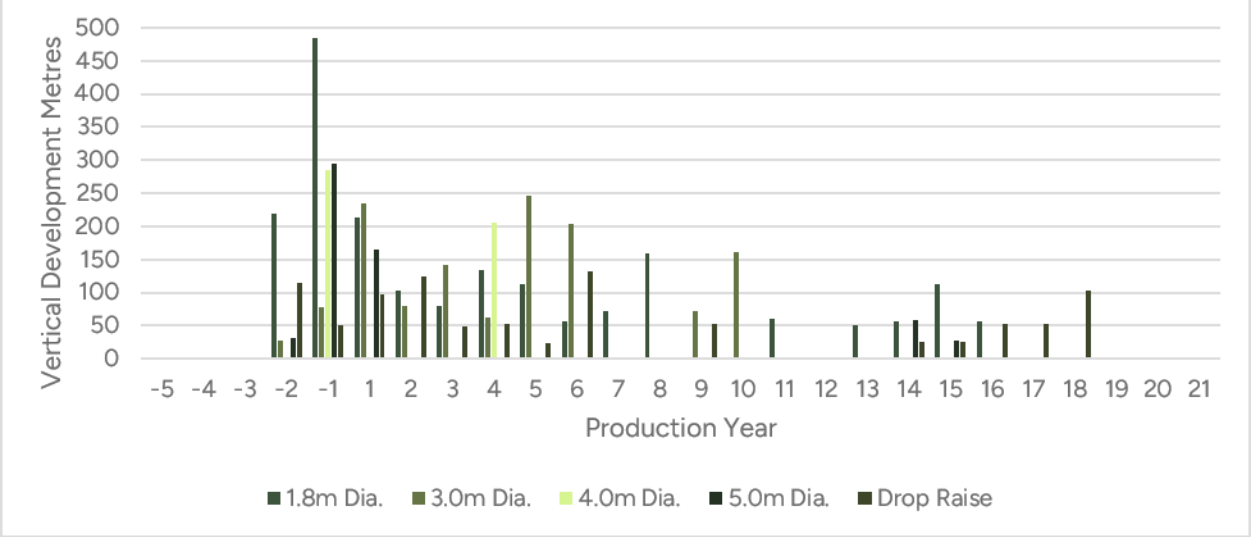
16.5.3 Vertical Development

Vertical development is required at the IBW Project for ventilation, material handling, emergency egress, and slot openings for production stopes. Slot raises for stopes are operational development and are not considered in this section but are included within the stope planning.

Figure 16-18 provides a LOM summary of the required vertical capital development, noting the following design assumptions:

- Primary ventilation infrastructure at La Romanera generally requires 4.0 m or 5.0 m diameter raises, with smaller diameters possible for El Cura and La Infanta.
- Ore pass infrastructure is designed at 3.0 m diameter.
- 1.8 m diameter raises are used for emergency egress installations and temporary/ancillary ventilation.
- Drop raises are used for short ventilation connections between levels.

Figure 16-18: Annual LOM Vertical Development



All raise bore development will be completed by contractor using contractor supplied and operated machinery. All drop raises will be developed by the owner.

16.5.4 Mine Production

16.5.4.1 Stope Productivity

Stope production rates for mine scheduling were derived using the input assumptions provided in Table 16-11. LHD productivity was estimated using cycle time analysis, with reference to a theoretical shift breakdown for an LHD operator. All other factors were assumed based on benchmarked data and/or engineer experience.

Table 16-11: Stope Productivity Analysis Input Assumptions

Assumption	Unit	Quantity	Source / Comment
LHD Productivity	tpd	1,698	Calculated theoretical rate
Production Drill Productivity	m/d	150	Benchmarked
Production Hole Re-drill	% of drill metres	10%	Benchmarked
Production Hole Cleaning	% of drill metres	5%	Benchmarked
Explosive Loading	days	Var.	Up to 3 days dependent on size of blast.
Blast Preparation Time	days	0.5	Assumption for blast evacuation, blasting gas purge and clean-up.
Paste Backfill Preparation Time	days	5.0	Assumption for stope clean-up, rehabilitation, barricade construction, pipe and instrumentation installation.
CRF Backfill Preparation Time	days	3.0	Assumption for stope clean-up, rehabilitation, bund construction, and bumper installation.

16.5.4.2 Mine Production Plan

Under the development schedule described in Section 16.5.2 and the stope productivity assumptions detailed in Section 16.5.4.1, a peak production rate of 1.2 Mtpa is considered achievable for the IPW Project. The production rate is sustainable for 18 complete years of full-scale operation before ramping down over the subsequent two years of resource depletion.

Prior to achieving full production, approximately 5 years of pre-production development are necessary to adequately develop the deposit to a point where production activities can commence, followed by a year of mine production ramp-up.

All ore produced from the underground mine will be fed directly to the process plant without intermittent stockpiling or blending, except for approximately 127 kt of ore produced during pre-development and production ramp-up activities. This material will be stockpiled to supplement the ore feed during a six-month process plant commissioning period.

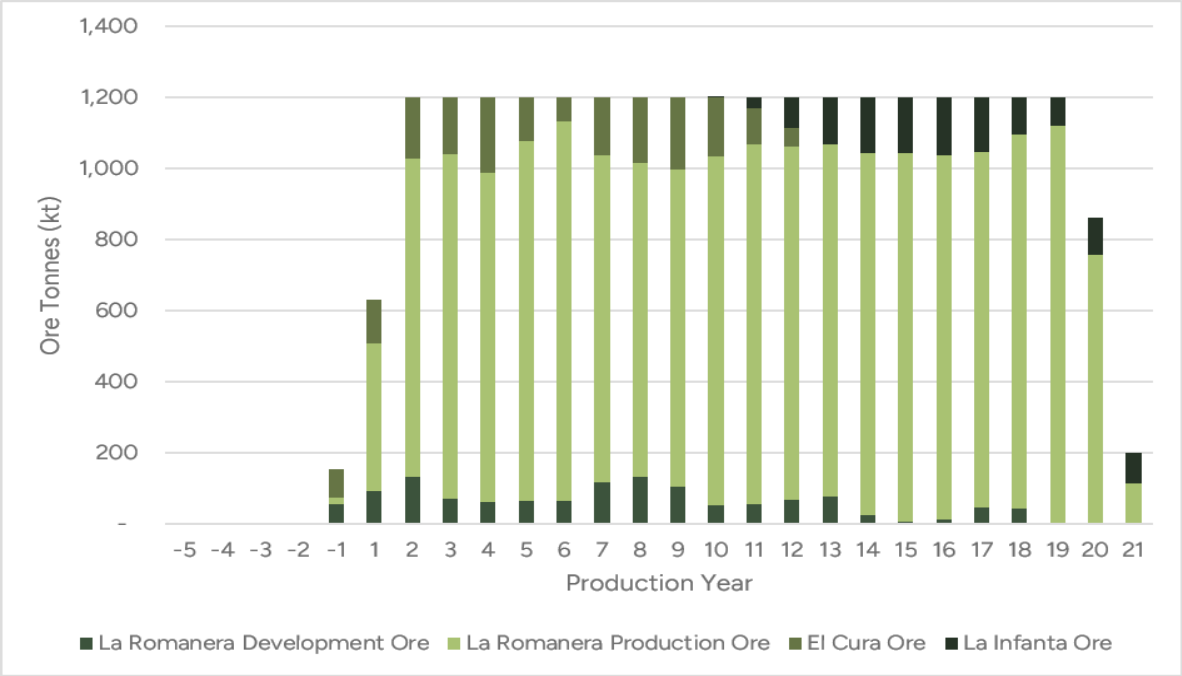
In general, achieving full production at La Romanera is prioritised because it is the largest deposit, containing 87% of the IBW Project Mineral Reserve base, and is therefore capable of achieving and sustaining significantly higher production rates than the El Cura and La Infanta deposits (containing 8% and 5% of the Reserve base, respectively). El Cura and La Infanta are scheduled to supplement the process feed from La Romanera throughout the LOM, with production rates limited by the respective geometries of the deposits. El Cura is scheduled before Infanta for the following reasons:

- Proximity to La Romanera with direct access from the La Romanera decline, enabling the deferment of some CAPEX spend (e.g., Railveyor infrastructure).
- Lower unit costs compared to La Infanta, partly due to a greater ability to share resources with La Romanera; and
- To allow blending of La Infanta ore at higher zinc grades with lower-grade material from La Romanera towards the end of the mine life, thereby ensuring the process grade remains within the design criteria limits of the process plant.

The LOM production plan is provided by Table 16-12 and Table 16-13 for stope production, and global production quantities, respectively.

Ore production from the underground mine is split between ore sourced from lateral development and ore mined from production stopes. The production profile is illustrated by Figure 16-19.

Figure 16-19: Annual LOM Ore Production by Source



As shown in Figure 16-6, the La Romanera deposit is divided into three separate mining horizons to facilitate production ramp-up. Whilst individual horizons were delineated based on accessibility for early development, consideration was also given to targeting the highest-grade areas first to improve project NPV. The application of this strategy is illustrated by Figure 16-20 with a decline in the average NSR of the mined ore as the LOM progresses towards depletion.

Figure 16-20: Annual LOM Production by Mining Horizon with Global Average NSR

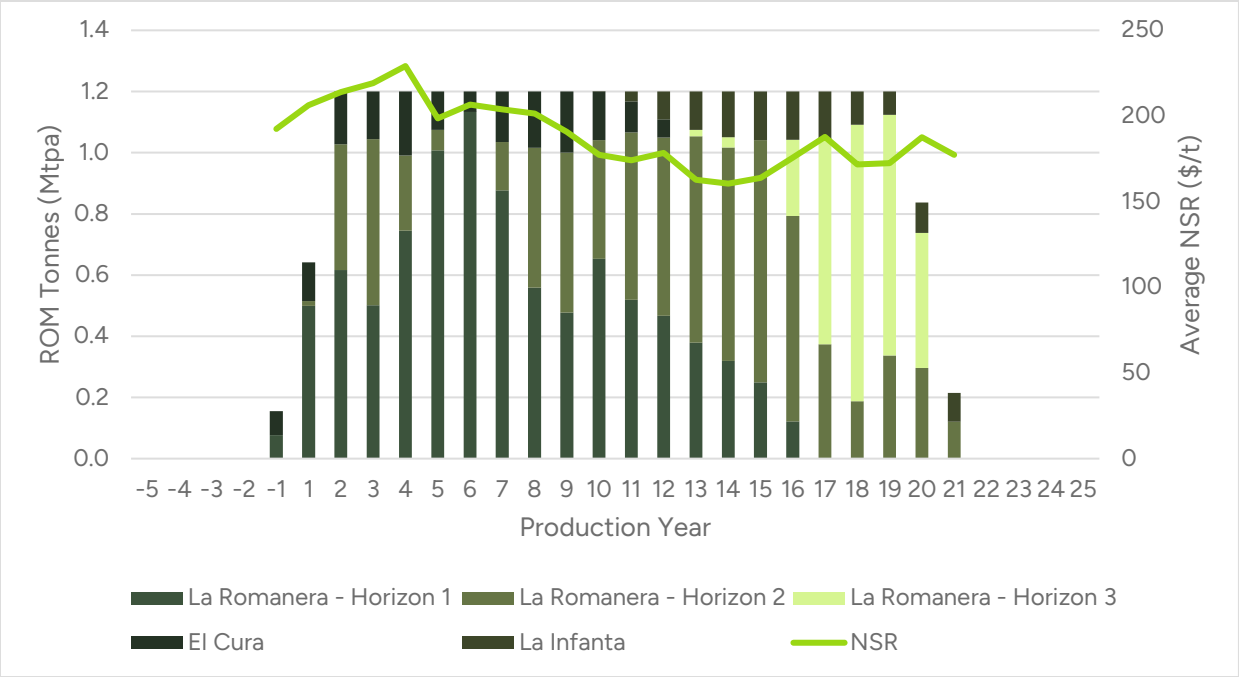


Table 16-12: LOM Stope Production Summary (Diluted and Recovered Tonnes)

Year	Transversal		Longitudinal		Total							
	Tonnage (kt)	No. of Stopes	Tonnage (kt)	No. of Stopes	Tonnage (kt)	No. of Stopes	S (%)	Zn (%)	Cu (%)	Pb (%)	Au (g/t)	Ag (g/t)
-5	-	-	-	-	-	-	0.0%	0.00%	0.00%	0.00%	-	-
-4	-	-	-	-	-	-	0.0%	0.00%	0.00%	0.00%	-	-
-3	-	-	-	-	-	-	0.0%	0.00%	0.00%	0.00%	-	-
-2	-	-	-	-	-	-	0.0%	0.00%	0.00%	0.00%	-	-
-1	19	0	16	3	35	3	32.1%	0.98%	0.61%	0.94%	0.99	58.43
1	395	12	87	15	482	27	34.9%	1.78%	0.52%	1.28%	1.24	66.74
2	710	19	336	39	1,046	59	34.6%	2.82%	0.50%	1.43%	1.19	66.06
3	731	17	376	38	1,106	54	37.1%	2.93%	0.47%	1.19%	1.16	59.58
4	759	21	360	41	1,119	62	37.4%	3.42%	0.53%	1.36%	1.46	59.67
5	828	27	298	32	1,125	59	37.3%	2.41%	0.45%	1.15%	1.50	55.02
6	941	27	156	16	1,097	44	38.3%	2.69%	0.32%	1.23%	1.88	53.35
7	824	31	246	28	1,071	59	36.2%	2.94%	0.33%	1.28%	1.57	56.39
8	717	25	348	39	1,065	64	33.8%	2.45%	0.40%	1.09%	1.17	71.01
9	695	24	399	44	1,094	68	33.9%	1.94%	0.41%	0.98%	1.00	63.93
10	653	21	493	52	1,146	73	33.4%	1.81%	0.42%	0.90%	0.93	52.17
11	698	23	414	45	1,113	68	32.6%	1.62%	0.39%	0.86%	0.92	51.26
12	663	21	408	44	1,071	65	33.5%	1.76%	0.37%	0.91%	1.07	58.63
13	688	22	392	41	1,080	63	31.5%	1.48%	0.38%	0.84%	0.78	43.34
14	820	27	355	47	1,175	74	30.0%	1.51%	0.46%	0.90%	0.70	41.33
15	780	27	410	51	1,191	78	30.2%	1.76%	0.54%	1.01%	0.71	43.39
16	733	23	453	53	1,186	76	30.5%	2.58%	0.45%	1.27%	0.73	44.45
17	752	21	399	51	1,151	72	32.9%	2.91%	0.46%	1.35%	0.76	52.10
18	859	23	295	34	1,154	57	33.9%	2.58%	0.51%	1.28%	0.83	43.15

Year	Transversal		Longitudinal		Total							
	Tonnage (kt)	No. of Stopes	Tonnage (kt)	No. of Stopes	Tonnage (kt)	No. of Stopes	S (%)	Zn (%)	Cu (%)	Pb (%)	Au (g/t)	Ag (g/t)
19	890	21	310	31	1,200	52	34.4%	1.77%	0.42%	0.91%	1.02	41.36
20	595	13	265	27	861	40	35.0%	2.30%	0.48%	1.18%	1.08	52.47
21	86	3	115	21	201	24	24.0%	2.75%	0.90%	1.62%	0.57	43.97
TOTAL	**14,837**	**449**	**6,932**	**791**	**21,769**	**1,240**	**34.1%**	**2.3%**	**0.4%**	**1.1%**	**1.09**	**53.09**

Table 16-13: LOM Global Production Summary (Diluted and Recovered Tonnes)

Year	Ore (kt)	S (%)	S (kt)	Zn (%)	Zn (t)	Cu (%)	Cu (t)	Pb (%)	Pb (t)	Au (g/t)	Au (koz)	Ag (g/t)	Ag (koz)	Waste (kt)	Total (kt)
-5	-	0.00%	-	0.00%	-	0.00%	-	0.00%	-	-	-	-	-	228	228
-4	-	0.00%	-	0.00%	-	0.00%	-	0.00%	-	-	-	-	-	231	231
-3	-	0.00%	-	0.00%	-	0.00%	-	0.00%	-	-	-	-	-	247	247
-2	-	0.00%	-	0.00%	-	0.00%	-	0.00%	-	-	-	-	-	386	386
-1	155	19.04%	30	1.22%	2	0.71%	1	0.88%	1	1.07	5	55.45	277	557	712
1	632	30.25%	191	1.96%	12	0.56%	4	1.27%	8	1.26	26	63.42	1,289	382	1,014
2	1,200	31.66%	380	2.83%	34	0.50%	6	1.40%	17	1.19	46	65.19	2,515	230	1,430
3	1,200	33.59%	403	2.95%	35	0.47%	6	1.20%	14	1.23	48	59.36	2,290	196	1,396
4	1,200	32.56%	391	3.35%	40	0.53%	6	1.35%	16	1.45	56	59.70	2,303	204	1,404
5	1,200	33.99%	408	2.39%	29	0.45%	5	1.14%	14	1.48	57	54.23	2,092	161	1,361
6	1,200	36.55%	439	2.65%	32	0.33%	4	1.21%	15	1.82	70	53.76	2,074	151	1,351
7	1,200	32.00%	384	2.89%	35	0.33%	4	1.27%	15	1.52	59	58.19	2,245	71	1,271
8	1,200	29.55%	355	2.40%	29	0.39%	5	1.08%	13	1.16	45	69.82	2,694	46	1,246
9	1,200	29.66%	356	1.87%	22	0.40%	5	0.96%	12	0.99	38	62.43	2,409	148	1,348
10	1,200	30.29%	363	1.78%	21	0.42%	5	0.89%	11	0.92	35	51.58	1,990	159	1,359
11	1,200	30.09%	361	1.68%	20	0.40%	5	0.89%	11	0.88	34	51.04	1,969	83	1,283
12	1,200	31.39%	377	2.05%	25	0.41%	5	1.08%	13	1.02	39	58.34	2,251	51	1,251

Year	Ore (kt)	S (%)	S (kt)	Zn (%)	Zn (t)	Cu (%)	Cu (t)	Pb (%)	Pb (t)	Au (g/t)	Au (koz)	Ag (g/t)	Ag (koz)	Waste (kt)	Total (kt)
13	1,200	31.05%	373	1.70%	20	0.40%	5	0.96%	11	0.78	30	45.20	1,744	59	1,259
14	1,200	30.24%	363	1.54%	18	0.46%	6	0.90%	11	0.70	27	41.65	1,607	70	1,270
15	1,200	30.32%	364	1.76%	21	0.54%	6	1.00%	12	0.71	27	43.42	1,675	80	1,280
16	1,200	30.62%	367	2.58%	31	0.45%	5	1.26%	15	0.73	28	44.49	1,716	74	1,274
17	1,200	33.24%	399	2.84%	34	0.46%	6	1.33%	16	0.77	30	51.03	1,969	52	1,252
18	1,200	34.20%	410	2.56%	31	0.51%	6	1.27%	15	0.86	33	43.33	1,672	27	1,227
19	1,200	34.40%	413	1.77%	21	0.42%	5	0.91%	11	1.02	39	41.36	1,596	-	1,200
20	861	34.97%	301	2.30%	20	0.48%	4	1.18%	10	1.08	30	52.47	1,452	-	861
21	201	24.01%	48	2.75%	6	0.90%	2	1.62%	3	0.57	4	43.97	284	-	201
TOTAL	**23,448**	**31.88%**	**7,474**	**2.30%**	**539**	**0.45%**	**105**	**1.13%**	**264**	**1.07**	**807**	**53.21**	**40,110**	**3,893**	**27,341**

16.6 Mine Backfill

16.6.1 Overview

Backfill is an integral component of the proposed underground mining method and is required to support geotechnical stability, ore recovery, dilution control, and the planned extraction sequence. The selected PFS mine fill strategy uses a combination of cemented pastefill, rockfill, and cemented rockfill (CRF), with the allocation of fill type controlled by the mine schedule and stope requirements.

- **Cemented Pastefill:** Involves mixing process tailings with a cement binder to produce a consolidated fill that can be pumped and placed underground by hydraulic means. It is used as the default option for backfilling primary transversal stopes and longitudinal retreating stopes due to operational and cost efficiencies; however, it relies on the availability of suitable tailings.
- **Dry Rockfill:** Consists of backfilling with unconsolidated waste rock and is the default option for backfilling secondary transverse stopes, as well as any additional stopes where consolidated fill is not required.
- **Cemented rockfill (CRF):** Involves mixing or coating the rockfill with a cement slurry for backfill consolidation. Used as a back-up option where consolidated fill is required and paste backfill is unavailable.

The current LOM schedule includes approximately 4.36 Mm³ of pastefill, 3.62 Mt of rockfill, and 0.22 Mt of CRF. CRF is required for the initial La Romanera and El Cura stopes before paste becomes available. The current mining schedule controls the annual timing and allocation of these materials.

16.6.2 Cemented Pastefill

The Project will employ cemented pastefill as the principal underground backfilling method for the La Romanera, El Cura, and La Infanta underground mines. The selected backfill strategy has been developed to provide stable fill support for the planned mining sequence while maximising the reuse of process tailings and reducing long-term surface tailings storage requirements.

The cemented pastefill system will utilise filtered flotation tailings from the process plant combined with cement binder to produce paste backfill for underground stope filling. Flotation tailings will be thickened and pressure filtered at a centralised surface filtration facility to produce filter cake for pastefill production. Tailings not immediately required will be temporarily stored in the IPS and reclaimed as needed.

For the La Romanera and El Cura operations, filtered tailings will be transported underground in an uncemented form and combined with cement binder at a dedicated underground pastefill plant at La Romanera before distribution to active stopes via a reticulation network. This arrangement reduces the operational and hydraulic risks associated with transporting cemented paste from surface. A separate pastefill mixing facility at La Infanta will provide backfill for that operation.

The La Romanera underground installation has been incorporated into mine planning on the basis of approximately 15 months from development-access release to operational readiness, inclusive of cavern excavation and support, civils, mechanical and electrical installation, and

commissioning. Backfill availability and curing therefore remain important interfaces with the mine development and production schedule.

Key design parameters mine backfill design include:

- LOM flotation tailings production: approximately 8.3 Mt dry solids
- LOM pastefill requirement: approximately 4.36 Mm³
- Nominal paste production rate: 150 t/h dry solids
- Design capacity sensitivity case: 180 t/h dry solids
- Filter cake solids concentration: 85 wt% solids (design basis)
- Final paste solids concentration: 80 wt% to 82 wt% solids
- Uncemented slurry transfer slump: 250 mm
- Final paste slump: 175 mm
- Nominal binder addition rate: 5% of dry solids
- Binder sensitivity range: 3% to 6%
- Operating stockpile capacity: approximately 5 days
- Underground reticulation allowance: approximately 5 km
- Mine and process operating basis: 8,000 operating hours per year

The process balance, based on the confirmed 35.40% final tailings yield, indicates approximately 8.30 Mt of dry final flotation tailings over the LOM compared with an estimated 7.47 Mt to 7.88 Mt of dry solids required by the scheduled paste volume. Supplementary granular solids are therefore not required to close the aggregate LOM paste mass balance, although they remain a potential recipe, grading, strength, or scheduling sensitivity.

The cemented pastefill system provides a technically appropriate backfilling solution for the underground mining operations while supporting the Project's tailings management strategy through the reuse of process tailings as underground fill. The available tailings inventory is sufficient to satisfy the LOM paste backfill requirements, and the proposed configuration of surface filtration with underground paste preparation at La Romanera reduces operational complexity and transportation risks. The cemented pastefill system forms a key component of the mining method and is expected to provide the ground support necessary to achieve the planned extraction sequence and stope recovery assumptions.

Further work at Feasibility Study level should include paste and filtration testwork, confirmation of rheology and hydraulic performance, binder and strength optimisation, detailed integration of the La Romanera underground station, confirmation of the La Infanta local distribution arrangement, and vendor sizing of the principal backfill equipment. These activities are intended to refine the selected PFS configuration rather than re-open the selected backfill strategy.

16.6.3 Dry Rockfill

Dry rockfill will be tipped into the open stope via LHD. A dry rockfill operation typically involves the following steps:

- Install a steel bumper once the stope is emptied of ore.

- Backfill manually (i.e. LHD operated directly from the machine) until the natural slope of the fill reaches the steel bumper.
- Remove the steel bumper and replace it with a rock berm (at a minimum height of half the LHD tyre diameter).
- Resume backfilling remotely (i.e. LHD operated from the remote stand). Maintain the rock berm at the edge of the natural fill slope by continually pushing material forward to advance the fill horizon.

Waste material is unlikely to be consistently available within the tramming distance of an LHD, so provisions for backfill storage must be considered near active backfill horizons. Underground backfill reserve silos are likely required to enable waste-carrying haul trucks to tip their load for re-handling into a stope. The silos can generally be created by utilising off-cycle transverse stopes, or by adapting exhausted development headings and/or established infrastructure not currently in use. Silos can alternatively be developed specifically for this purpose, although this would represent additional cost to the operation and should be considered a last resort[3].

16.6.4 Cemented Rockfill

Due to the limited CRF requirements at the Project, a simple CRF mixing set-up will be utilised with waste rock and cement slurry mixed in a designated sump, or mixing pit, located adjacent to the CRF stope. Slurry will be added directly to the mixing pit from an agitator truck (or Transmixer) that has been filled at surface and parked nearby. Waste is then dumped into the mixing pit, mixed with the slurry, and rehandled into the stope, one bucket load at a time.

16.7 Mine Infrastructure

16.7.1 Ventilation

16.7.1.1 Overview

The mine ventilation strategy has been developed for all IBW Project deposits based on the mine designs and schedules. The ventilation assessment was undertaken through desktop engineering analysis and supported by LOM ventilation network modelling using Ventsim design software.

The ventilation system has been designed to provide sufficient fresh air to support the planned underground workforce and mobile equipment fleet, dilute and remove airborne contaminants, and maintain acceptable working conditions underground throughout the mine life.

Ventilation requirements have been assessed against the Spanish mining regulations, supplemented by industry best-practice design criteria where appropriate.

16.7.1.2 Ventilation Design Basis

The ventilation design for the IBW Project has been developed with consideration of diesel equipment emissions and the applicable Spanish regulatory requirements set out in *Real Decreto 863/1985, Reglamento General de Normas Básicas de Seguridad Minera,* together with the associated supplementary Technical Instructions (ITCs).

[3] It is noted that no specific consideration has been given to backfill reserve silos in the mine design; however, a 5% CAPEX metre contingency has been included to account for any such detailed design requirements (see Section 16.4.2.2).

The applicable Spanish mining regulations and associated ITCs specify the following ventilation requirements:

- A minimum airflow of 40 L/s (0.040 m³/s) per person, based on the maximum number of personnel on the largest shift.
- Sufficient additional ventilation must be provided where diesel/internal-combustion vehicles or stationary engines are operated (a ventilation design criterion of 0.06 m³/s per kW of diesel engine power has been assumed, in line with industry best practice).
- Ventilation must be sufficient to dilute and remove gases, dust, and other harmful substances, and to maintain concentrations within the applicable exposure limits.
- A general maximum air velocity of 8 m/s applies, except in specified shafts, crosscuts and main return airways, where higher velocities may be permitted.
- Ventilation must account for temperature and humidity to maintain acceptable working conditions underground.

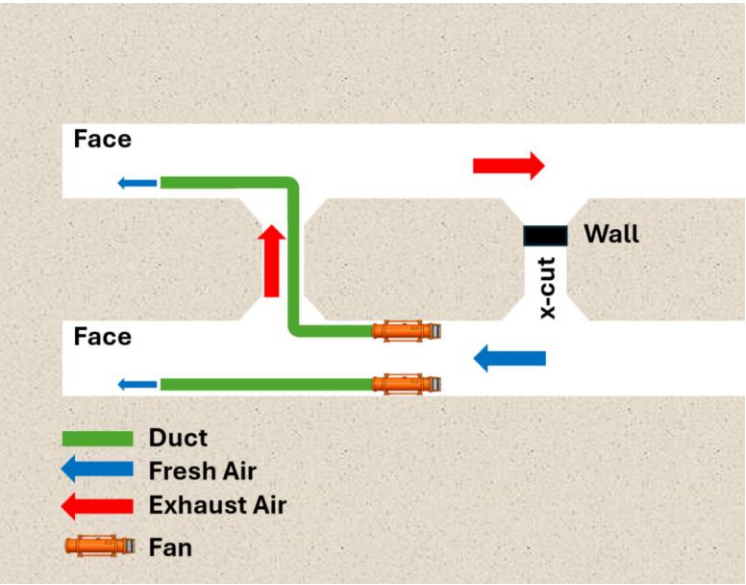
In addition to the ITCs, the maximum air velocity in working drifts is limited to < 4 m/s to minimise worker discomfort. This is in line with industry best practice.

16.7.1.3 La Romanera Decline Development

Initial development of the twin-decline access to La Romanera (Section 16.4.1.1) will require auxiliary ventilation until sufficient connections (crosscuts) between the declines are in place to establish a through-flow ventilation circuit.

Once a decline crosscut is in place, a primary exhaust installation will be established at the Railveyor tunnel portal, comprising two single-stage 1,600 mm impeller axial fans positioned within a sealed ventilation double-door across the portal. The exhaust fans will create negative pressure within the tunnel decline, drawing air from the surface through the service tunnel access. Air will travel down the service tunnel to the open crosscut, then return along the exhausting tunnel to the surface through the portal fan arrangement (Figure 16-21).

Figure 16-21: Twin Decline Ventilation Strategy



Source: SLR 2026

Auxiliary fans will be positioned underground, upstream of the crosscut, to force fresh air towards the advancing tunnel headings. The auxiliary fans (and connecting duct) will be progressively relocated as additional crosscuts are established along the decline.

The portal exhaust fan system will remain in place as part of the LOM tunnel ventilation infrastructure, controlling and supplementing the primary mine ventilation network as additional underground development and ventilation infrastructure are established. A curtain/brattice arrangement will be installed around the Railveyor to provide sufficient resistance for the exhaust fans to operate whilst allowing the free flow of the Railveyor to the surface.

16.7.1.4 Primary Ventilation Circuit

The LOM ventilation system has been developed to provide defined pathways for fresh air intake and return air to the La Romanera, El Cura and La Infanta mining areas.

La Romanera and El Cura will form part of the principal mine ventilation network serving the main access and Railveyor tunnel infrastructure. La Infanta will operate as a separate ventilation district with an independent connection to the surface.

The primary ventilation system will operate primarily as an exhaust system. The exhaust fans will create negative pressure within the return air system, drawing fresh air from the surface through the designated intake openings and distributing it through the underground workings before contaminated return air is exhausted to the surface.

La Romanera

The Romanera mining area will be ventilated using an exhaust ventilation system incorporating dedicated fresh-air and return-air infrastructure.

During the initial stages of underground development, fresh air will be supplied predominantly through the main access tunnel. Once the dedicated fresh air raise (FAR) is established, it will become the principal fresh air supply route to the La Romanera mining levels, with airflow delivered through the tunnel infrastructure as required.

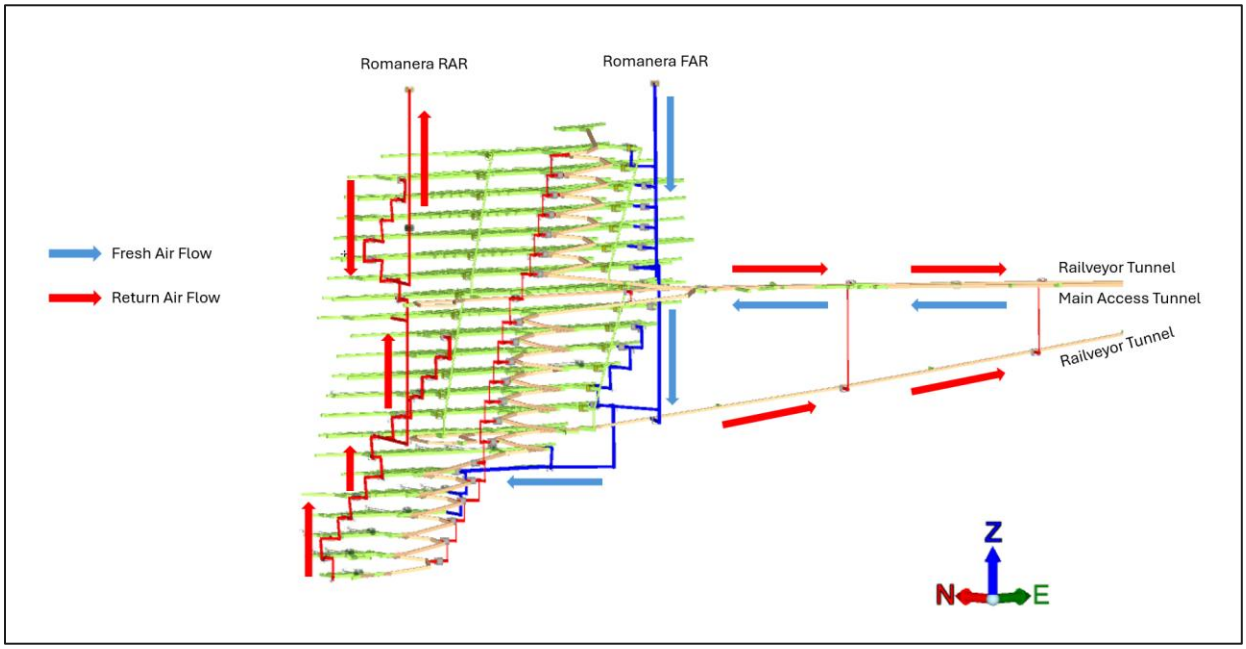
Fresh air will be supplied from the FAR and the main access infrastructure to the active mining levels. Return air from the operating areas will be directed via internal ventilation connections to the dedicated La Romanera return air raise (RAR) system.

Connections between the individual mining levels and the primary ventilation raises will comprise a combination of direct connections and dog-legged jump-up raises. This arrangement allows fresh air to be distributed to active working areas while isolating contaminated return air and directing it towards the primary return-air system.

Return air will ultimately be exhausted to the surface through the La Romanera RAR by the dedicated La Romanera primary exhaust fan.

The Romanera LOM ventilation strategy is illustrated in Figure 16-22.

Figure 16-22: Romanera Ventilation Network



Source: SLR 2026

El Cura

The El Cura mining area will be integrated into the main tunnel ventilation system.

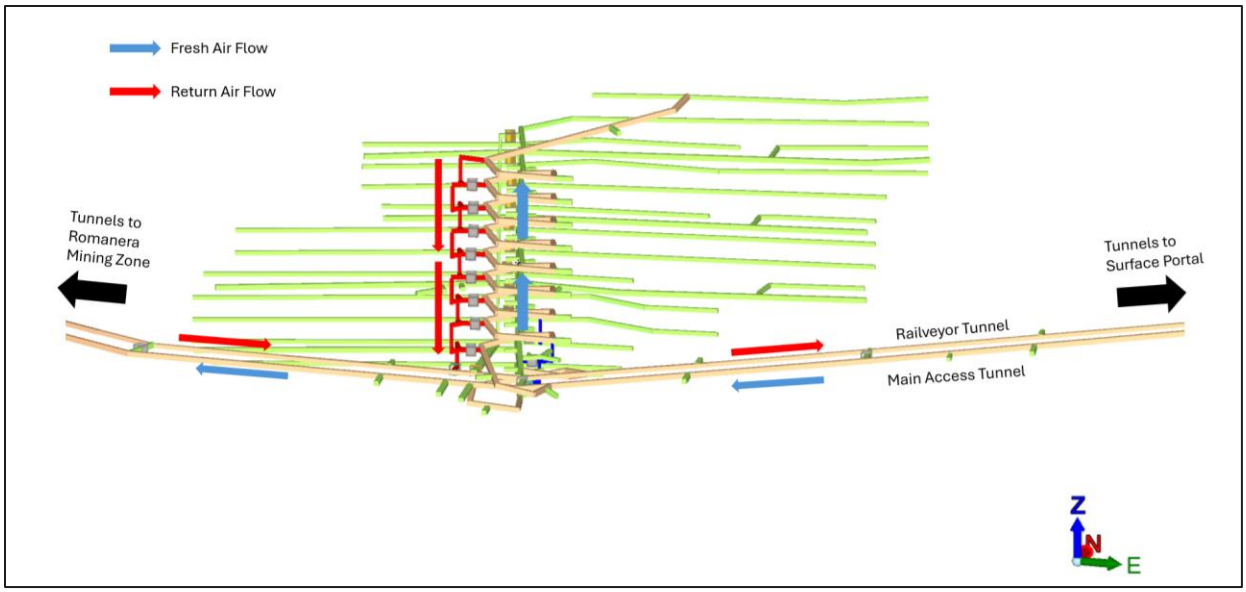
Fresh air will be supplied from the surface via the main access tunnel and distributed to the operating levels via the internal ramp and level development.

Return air from the El Cura workings will be directed through the internal RAR network, including dog-legged jump-up raises that connect the individual mining levels to the main return-air pathway. Return air will then be directed to the Railveyor tunnel and exhausted to the surface via the tunnel's primary exhaust fan system.

The tunnel system therefore provides the primary intake and return air connections between the El Cura underground workings and the surface.

The El Cura LOM ventilation strategy is illustrated in Figure 16-23.

Figure 16-23: El Cura Ventilation Network



Source: SLR 2026

La Infanta

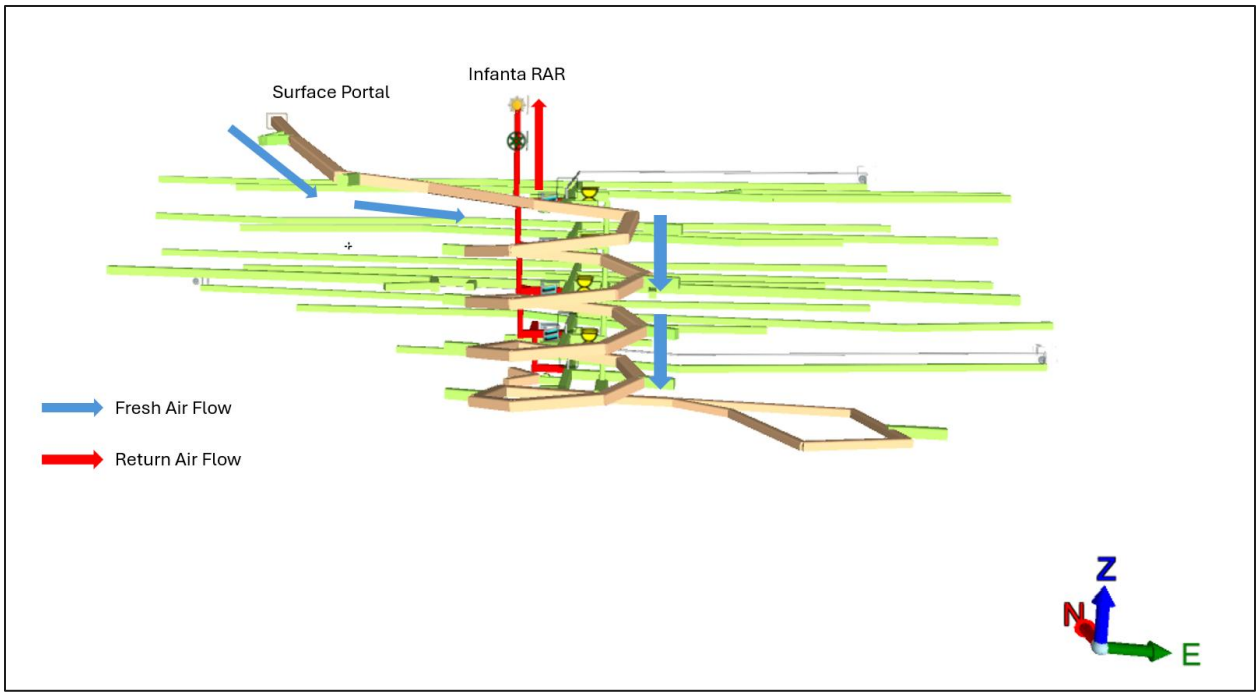
La Infanta will be ventilated independently from the La Romanera and El Cura ventilation network and will operate as a separate ventilation district.

Fresh air will be supplied directly from the surface via the La Infanta decline and distributed through the internal development to the active mining levels.

Return air will be directed through the dedicated La Infanta RAR and exhausted to the surface by the La Infanta primary exhaust fan. This arrangement establishes a defined intake-to-return ventilation circuit between the decline and the dedicated surface-connected RAR.

The Infanta LOM ventilation strategy is illustrated in Figure 16-24.

Figure 16-24: La Infanta Ventilation Network



Source: SLR 2026

16.7.1.5 Primary Fan Requirements

Primary fan duties were derived from the ventilation network model to provide the required airflow within each ventilation district while overcoming the resistance of the associated underground ventilation network.

The PFS primary fan duties are summarised in Table 16-14.

Table 16-14: Primary Fan Duties

Ventilation District	Fan Arrangement	Fan Type	Design Duty
Infanta	Single 1,400 mm fan	Howden AXN 1400	68 m^3/sec, FTP =2452 Pa, 1490 rpm
El Cura	Twin 1,600 mm fans	Howden AXN 1600	139 m^3/sec, FTP =3455 Pa, 1490 rpm
Romanera	Single 3,000 mm fan	Zitron ZVN 1-30-1100/6	225 m^3/sec, FTP = 3500 Pa, 1000 rpm

The primary fan selections at PFS level are based on the modelled airflow and pressure requirements. Final fan selection, configuration, and installation requirements will be confirmed during subsequent stages of engineering, in consultation with the selected fan supplier.

Variable frequency drives (VFDs) are recommended for the primary fan installations to provide operational flexibility and allow fan duties to be adjusted in response to changes in airflow demand throughout the mine life. This will enable the ventilation system to respond to the

changing location and intensity of underground mining activities rather than operating continuously at the maximum design duty.

16.7.1.6 Auxiliary Ventilation

Auxiliary ventilation will be provided to development headings and other working areas that cannot be adequately ventilated directly by the primary ventilation circuit.

Under normal development and production conditions, secondary ventilation will be provided by 1,200 mm auxiliary fans (or 1,400 mm fans for longer sections) connected to flexible ducting. Fans will be positioned at fresh air locations and will deliver forced ventilation through the ducting to the active development headings and working faces.

Airflow distribution across individual mining levels will be regulated to meet short-term mining and development requirements by utilising drop-board regulators (DBRs) installed within ventilation walls. The DBRs will enable control of the amount of fresh air entering a production level in line with local operational demands.

16.7.2 Mine Dewatering

16.7.2.1 Overview

As discussed in Section 16.3, limited hydrogeological data and analysis has been undertaken at the Project, meaning the available hydrogeological data are currently insufficient to define a preferred mine water management strategy or support detailed dewatering system design. The following represents a conceptual design for a mine dewatering system to collect and convey contact water within the mine to surface for treatment, re-use, or discharge. This section is intended to complement what is summarised in 16.3.4, with the remaining elements of the strategy (including the required system capacity) to be further defined as hydrogeological investigations progress and operational service-water requirements are refined.

16.7.2.2 Mine Dewatering Strategy

The purpose of the underground mine dewatering system is to collect the used service water (water used in drilling operations and for wetting the muck piles) and groundwater inflow (collectively referred to as mine water) and transfer this water to surface from the mine workings. The system at the IBW Project will be a “dirty” water system, with limited underground treatment of suspended solids prior to pumping to surface, other than settlement within designated sumps and pumping stations.

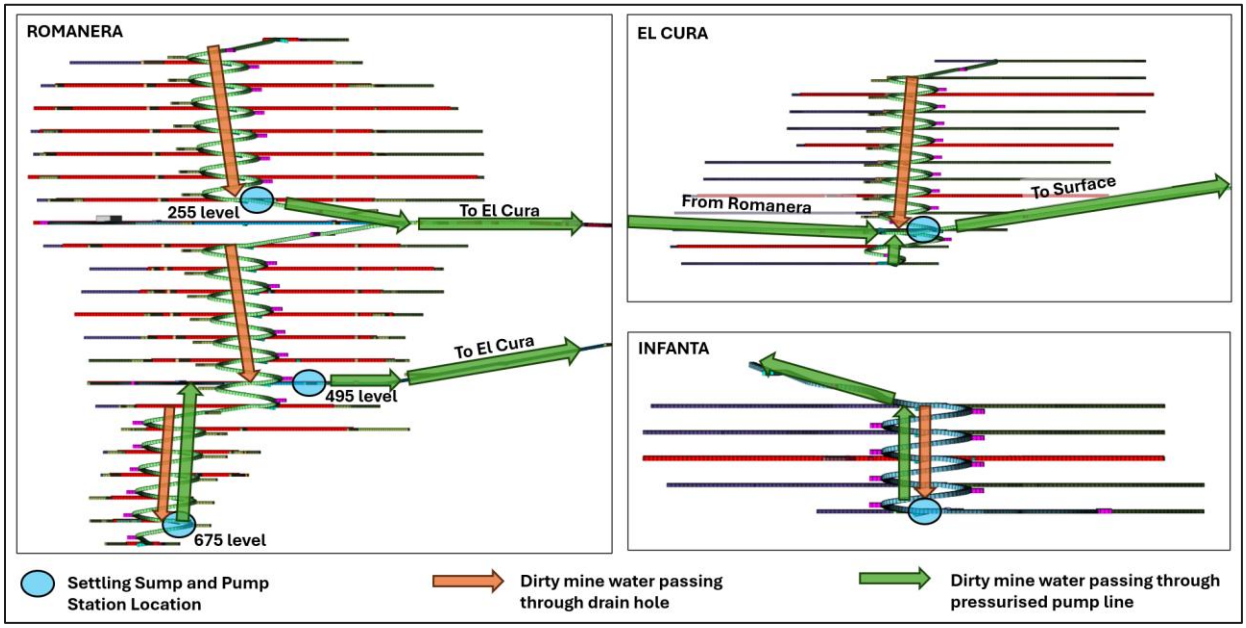
During the initial decline development (i.e., before the primary dewatering facilities have been constructed and commissioned), mine water will be pumped to surface using a positive cascade system through the drain line reticulation installed in the decline. Four-kilowatt face pumps will be used to remove water at the advancing face, with 15 kW submersible pumps lifting water from established level sumps (at the level access drive or a temporary location on the Railveyor decline) and depositing it into the adjacent level sump on the level above, or further up the decline. This process will continue until the mine water reaches the surface.

With this type of system, maintenance of the level sumps should be carried out regularly, with sumps mucked out to remove dewatered grit, fines and fibres, if fibres are used in the shotcrete. The pumps also require regular maintenance to ensure their expected operating life and efficiency.

Primary pumping stations with integrated settling arrangements will be constructed at strategic locations within the mine workings. At La Romanera, they have been placed at the base of each production horizon, i.e., on the 255-level serving Horizon 1, on the 495-level serving Horizon 2, and on the 675-level serving Horizon 3. A primary pumping station is also located at the base of the El Cura and La Infanta mine workings.

Figure 16-25 presents an overview of the conceptual mine dewatering strategy for the three deposits, which uses drain holes drilled between level sumps to direct mine water towards the primary pumping infrastructure, and footwall drives developed on a positive gradient from the level accesses (+3%) to enable water to gravitate towards the level sumps. It is noted that all La Romanera mine water will pass through the El Cura pump station on its way to surface, meaning the El Cura pump station will be of higher design capacity. Similarly, all mine water from Horizon 3 will pass through the 495-level pump station at La Romanera as an intermediary.

Figure 16-25: Overview of Mine Dewatering Strategy at the Project (looking north)



Source: SLR 2026

16.7.3 Material Handling

16.7.3.1 Railveyor

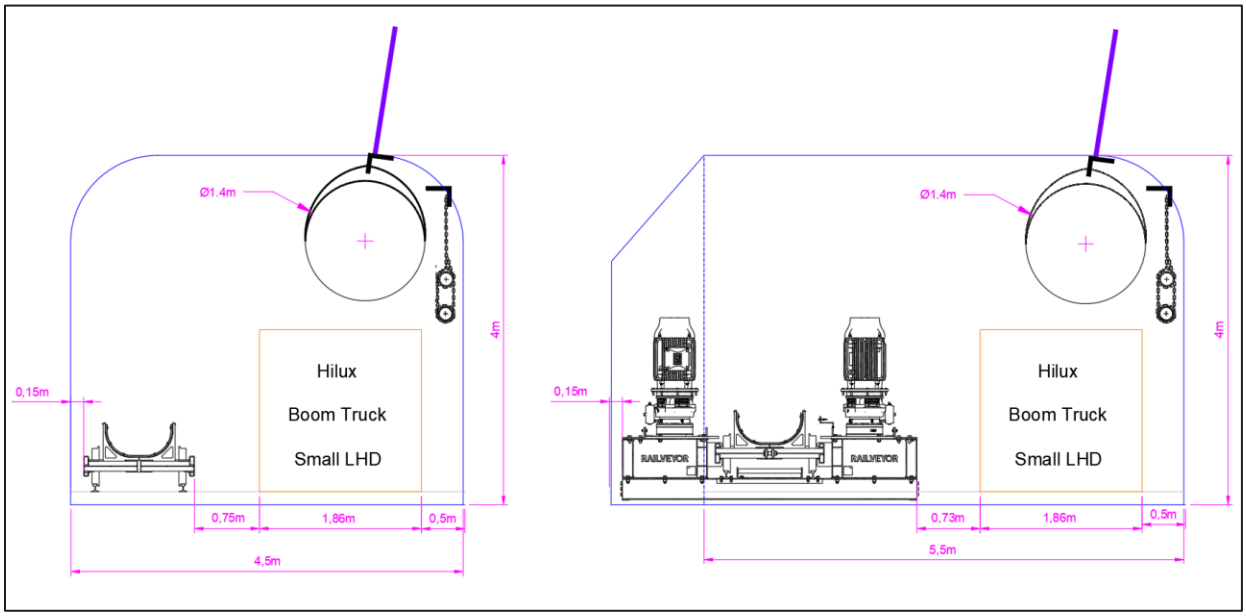
A Railveyor system has been selected by Emerita as the primary bulk material handling system. A summary of the system design is included below. Refer to the full design report for further detail (Railveyor Technologies Global Inc., 2026).

The system configuration for the IBW Project will be a shuttle with bypass spurs. Loaded trains will travel up the ramp from the load levels in the forward direction, passing the returning empty trains in the bypasses, and on to the discharge locations. At the discharge locations, the Railveyor trains will dump material into stockpiles.

The mine ramp design has horizontal turn radii of 30 m, allowing the use of Railveyor's standard 2.44 m cars. Drive stations will be placed along the route based on power requirements to control the movement of all trains and ensure sufficient power to start and stop trains anywhere in the system.

The Railveyor decline tunnel profile has been sized to accommodate the Railveyor track and any service equipment required for maintenance. Decline profile widths must increase to accommodate drive stations and designated bypass locations. Figure 16-26 provides the design schematic for the Railveyor decline defined for the IBW Project.

Figure 16-26: Railveyor Decline Profile Showing Standard Section (left) and Drive Station and Bypass Section (right)



Source: SLR 2026

The Railveyor system will be used to transport material during decline construction. A temporary load location will be moved as the declines are extended, keeping the scoop tramming distance to a minimum. During this period, a Hag Loader will be used to load material onto the Railveyor cars. Once the declines reach the main load point, permanent loading equipment will be installed. There will be one permanent loading location at La Infanta and El Cura, and four locations at La Romanera, at the base of each material pass (see Section 16.7.3.2).

There will be two discharge loops on the surface. The ore discharge loop will deposit ore into a stockpile, where wheel loaders will transfer it to the crusher circuit. Waste will be stockpiled via the second discharge loop and then moved to the larger waste stockpiles. Also on the surface is the Railveyor maintenance loop and shop, where the trains will be serviced separately from the production.

16.7.3.2 Material Pass

The Railveyor system will be used alongside the ore/waste pass system serving Horizon 1 and Horizon 2 of La Romanera, as well as El Cura and La Infanta. As the Railveyor does not extend to Horizon 3 of La Romanera, material from these lower levels will be loaded onto trucks at designated footwall loading points and hauled to the Horizon 2 material pass (level 465). As the Railveyor does not extend to Horizon 3 of La Romanera, material from these lower levels will be loaded onto trucks at designated footwall loading points and hauled to the Horizon 2 material pass (level 465).

With the exception of La Romanera Horizon 3, ore and waste will be loaded directly at the production face and hauled to the material pass tipping point on the level. Due to the greater strike length at La Romanera and the higher throughputs, two separate material pass systems have been designed for each Horizon, one towards the east and one towards the west of the orebody. The two-pass system reduces haulage time to the tipping points and provides opportunities to segregate material types for batch transportation to surface, e.g. campaigning the haulage of ore/waste, or mineral type for ore blending, etc.

All tipping points will have a grizzly to prevent oversize from migrating into the material pass. Grizzlies will have a 0.6 m aperture, with the material pass sized at 3.0 m diameter to give a 5:1 orepass diameter to rock size. This ratio is often used as the industry-standard for avoiding hang-ups.

16.7.3.3 Railveyor Loading

A loading chute with a vibrating feeder will be installed at the base of each material pass at La Romanera. The feeder will feed a short conveyor, which will in turn load the Railveyor cars. A magnet will be installed to remove any tramp metal before Railveyor loading.

Due to the intended low productivities at El Cura and La Infanta, no chute/screen arrangement will be installed. Instead, the material will exit the pass directly onto the floor, where it will be rehandled by an LHD and loaded onto the Railveyor cars with the assistance of a Hag Loader.

16.7.4 Mine Service Water

Mine service water will be sourced from the surface and distributed around the mine via a high-density polyethylene (HDPE) piping network that enters at the surface portals. Pressure in the reticulation network will be controlled by pressure reduction valves (PRVs) installed in the decline. Ancillary pumps will be required to lift service water to the production areas of La Romanera Horizon 1 and throughout El Cura. All other areas are expected to be served by gravity flow.

16.7.5 Electrical Distribution

Electrical power will be supplied throughout the mine for operational and miscellaneous loads. The power will be distributed at 12.5 kV through a primary feeder entering at the mine portal.

A 1000 kVA, 12.5/0.6 kV underground substation will be located on each level (at the level access location) and along every 500 m of development. Boreholes will be used to connect substations between levels; minimising cable runs in active development headings and reducing cable distances to limit substation requirements.

The peak installed power for the IBW mining operations is estimated at 8.1 MW. The mining power demand is calculated using the underground mining models for the three orebodies, together with their corresponding equipment duty and utilisation profiles.

16.7.6 Compressed Air

Compressed air at the Project is used to power equipment without built-in compressors, for ancillary tasks such as bootleg/bench blowing and hole cleaning, and to provide an emergency air supply to areas of refuge. The compressed air supply will be provided by compressed air units located at the surface and reticulated underground via a network of steel pipes installed along the ramp, main drifts, and escapeways throughout the mine. Standby compressor capacity is maintained at the surface for system redundancy.

With modern mining equipment now largely using built-in onboard compressors, opportunities exist to replace the surface compressors with portable underground compressors transported directly to the work location, where required. This would negate the need for a compressed air reticulation system, thereby providing operational cost savings. However, such a decision would need to consider specific operational demands, equipment needs, and any pertinent local regulatory requirements.

16.7.7 Mine Communications

Mine communications will be provided by a leaky feeder network covering the entire mine. All mine personnel will carry leaky feeder radios, and vehicles will be equipped with base units.

Although not considered or costed as part of the PFS, the QP recommends that a fibre optic backbone also be considered for the Project to enable the following mine optimisation opportunities:

- Equipment automation potential;
- Personnel and asset tracking;
- Ventilation on Demand (VOD), including remote control of ventilation regulators and VFDs on auxiliary and surface fans;
- Air quality monitoring stations for fresh and return air systems;
- Pump station automation;
- Automated stench gas injection; and
- Underground Wi-Fi connectivity.

16.7.8 Refuge Stations

Underground refuge stations will be installed and maintained throughout the mine for use in case of emergency. Sufficient refuge station capacity will be provided to accommodate all underground workers, with a refuge station located within the closer of 1 km or 15 minutes' walking distance of every active workplace, as per industry best practice. Permanent refuge stations have been placed at strategic, centralised locations within the mine workings of each deposit to meet best practice criteria. An additional refuge station will likely need to remain portable and follow the advancing development. This refuge station can be installed in any unused development heading.

Each refuge station is a prefabricated, fully self-contained unit that requires only an electrical connection at its installation location. Based on a peak underground workforce estimate, a total of five refuge stations with a capacity of 16 people will be required at La Romanera, and one each at El Cura and La Infanta.

16.7.9 Maintenance Bay

The main maintenance workshop will be located on surface, supplemented by a maintenance bay located off the La Romanera service ramp at the base of the surface decline (285 level). The 285 Maintenance Bay will be equipped to perform general servicing of critical equipment.

16.7.10 Explosive Magazines

Explosive and detonator magazines will be strategically located underground to improve operational efficiency. Magazines have been located at the 285 and 485 levels of La Romanera to ensure each mining horizon is adequately served. A magazine is also placed at central locations within El Cura and La Infanta.

Magazines will be constructed in accordance with local mining regulations, including mandated stand-off distances from critical infrastructure.

16.7.11 Emergency Egress

Secondary egress will be provided via escapeway raises connected to and passing between each level, allowing personnel to travel between levels via integrated ladderways in an emergency, if required.

It is assumed that a prefabricated manway system with an in-built ladder and platforms, such as the Safescape Laddertube, will be adopted at the Project. Such a system can be fitted within a small 1.8 m diameter raise-bored hole and is ideally positioned adjacent to a ventilation raise for quick and safe installation.

Emergency egress design and routing will likely need prior approval from the appropriate in-country authorities.

16.8 Mine Equipment

The underground mobile equipment requirements are summarised by Figure 16-27 and are based on the production schedule presented in Section 16.5.4.

Fleet numbers for critical equipment have been derived from first-principles calculations and based on machine operating hours with consideration for:

- 2 x 11 hours shifts per day, operating on a 365 workdays per annum calendar;
- Mechanical Availabilities of 85% for all equipment;
- Equipment Utilisation Factors derived for each equipment item; and
- Equipment Operating Efficiencies derived for each equipment item.

The individual shift plans are included in the underground mining cost model, but in general are inclusive of:

- Operator travel time from surface to the machine at the start of shift (assumed 15 minutes)
- Equipment inspection before start-up (assumed 6 minutes)
- Lunch breaks (assumed 1 hour)
- Supervisor visit and safety inspection (assumed 15 minutes)
- Operators travel time to surface at the end of shift (assumed 15 minutes)

- Any additional ancillary work dependent on the work activity.

Table 16-15 provides a summary of the derived operating metrics for all major equipment. Fleet number estimates for production and development machinery are generated in Deswik Scheduler, and the metrics shown here are used as direct Deswik inputs for the calculation.

Table 16-15: Operating Metrics for Major Equipment Used in Fleet Estimation

Equipment Item	Equipment Mechanical Availability	Equipment Utilisation Factor	Annual Equipment Operating Hours	Equipment Operating Efficiency	Annual Effective Operating Hours
LHD[1]	85%	69.5%	4,312	79.7%	3,437
Haul Truck	85%	81.1%	5,032	73.5%	3,699
Jumbo Drill	85%	76.5%	4,747	77.1%	3,660
Production Drill	85%	79.0%	4,902	90.5%	4,436
Bolter	85%	76.5%	4,747	83.7%	3,973
Scaler	85%	69.0%	4,281	39.9%	1,078
Emulsion Loader	85%	56.5%	3,506	66.4%	2,328

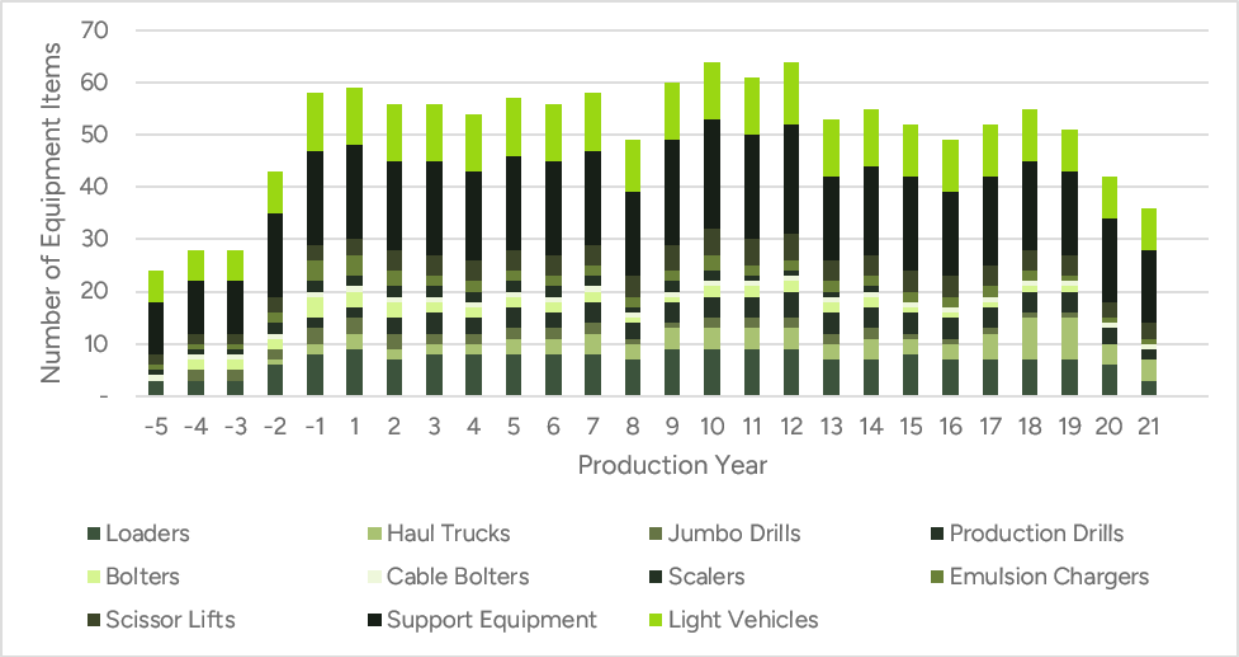
Notes:
1. Refers to fleet calculation for development LHDs. Production LHD felt requirements are derived from productivity calculations described in Section 16.5.4.1.

Haul truck numbers were estimated from haulage simulation and summarised annually (Figure 16-27). The simulation accounted for the internal haulage of development waste for backfill, and for the loading and hauling of reclaimed waste from the surface dump during years of underground waste deficit for backfill. Truck numbers are seen to increase notably in the later years of production at La Romanera during the mining of Horizon 3, i.e. for the truck conveyance of all mined material to the 465-level material pass.

Additionally, fleet estimations considered the following:

- The Cable Bolter fleet (and its operating hours) has been calculated using an assumed productivity of 30 m of installed cable per 11-hour shift and is consistent with benchmarked data for a comparable operation.
- The Transmixer fleet (and its operating hours) is derived from cycle time analysis and reflects the number required to optimise the productivity of the backfill LHD.
- The Scissor Lift fleet estimate comprises service installation requirements, ground rehabilitation requirements, and underground construction requirements. Fleet numbers for each operational demand have been estimated based on engineers' experience from comparable operations.
- All remaining service fleet items are estimated based on engineers' experience from comparable operations.

Figure 16-27: Mobile Mining Fleet by Production Year



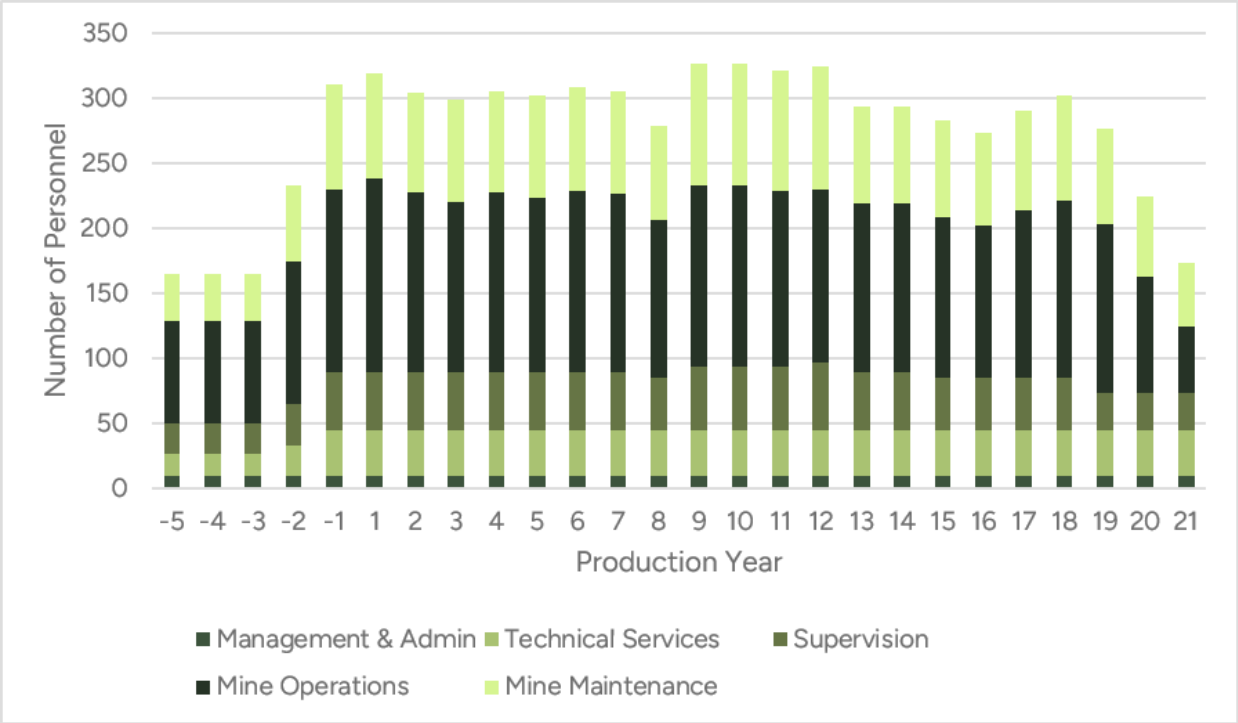
16.9 Mine Personnel

Mine personnel requirements for the Project are estimated based on the mining schedule and the operating requirements of the associated equipment (refer to Section 16.8). The estimate assumes owner mining, with a mine operating schedule of 11 hours per shift, two shifts per day, for seven days per week. Each 11-hour shift includes 0.5 hours for shift change and 0.5 hours for briefings and safety meetings, resulting in an effective shift length of 10 hours.

Each 11-hour shift is supported by a four-crew rotation on a 14-on-14-off roster (i.e., 14 days on-shift followed by 14 days of paid leave). After allowances for working days lost to annual leave, sick leave, absenteeism, and training, each worker is assigned 1,255 effective annual working hours, which forms the basis for workforce estimation. Senior management will work five 8-hour days per week.

Figure 16-28 summarises the LOM workforce estimate for the underground mine.

Figure 16-28: Mining Personnel by Production Year



17.0 Recovery Methods

17.1 Process Description

Three orebodies will be treated using the same process plant. La Romanera will be the main ore source, with ore from La Infanta and El Cura blended with it to even out the head grades and process requirements. Three orebodies will be treated using the same process plant. La Romanera will be the main ore source, with ore from La Infanta and El Cura blended with it to even out the head grades and process requirements as the process design criteria is based on La Romanera average head grades and testwork. La Romanera ore constitutes approximately 85% of the total tonnage for the three orebodies.

The process plant design is based on a flowsheet that comprises of a single stage crushing followed by SAG milling with pebble crushing in closed circuit, ball milling with classification cyclones in closed circuit, tower milling fine grinding with classification cyclones in closed circuit, four flotation circuits in the sequence of copper -> lead -> zinc -> pyrite, concentrate thickening and tails thickening. The final tailings are dewatered to a filter cake for paste backfill requirements and dry stacking.

The key project design features or criteria for the plant were:

- Nominal throughput of 1.2 Mtpa.
- A primary crusher and coarse ore stockpile with a 75% availability.
- Milling and flotation circuits with all downstream processing units with an availability of 92%.

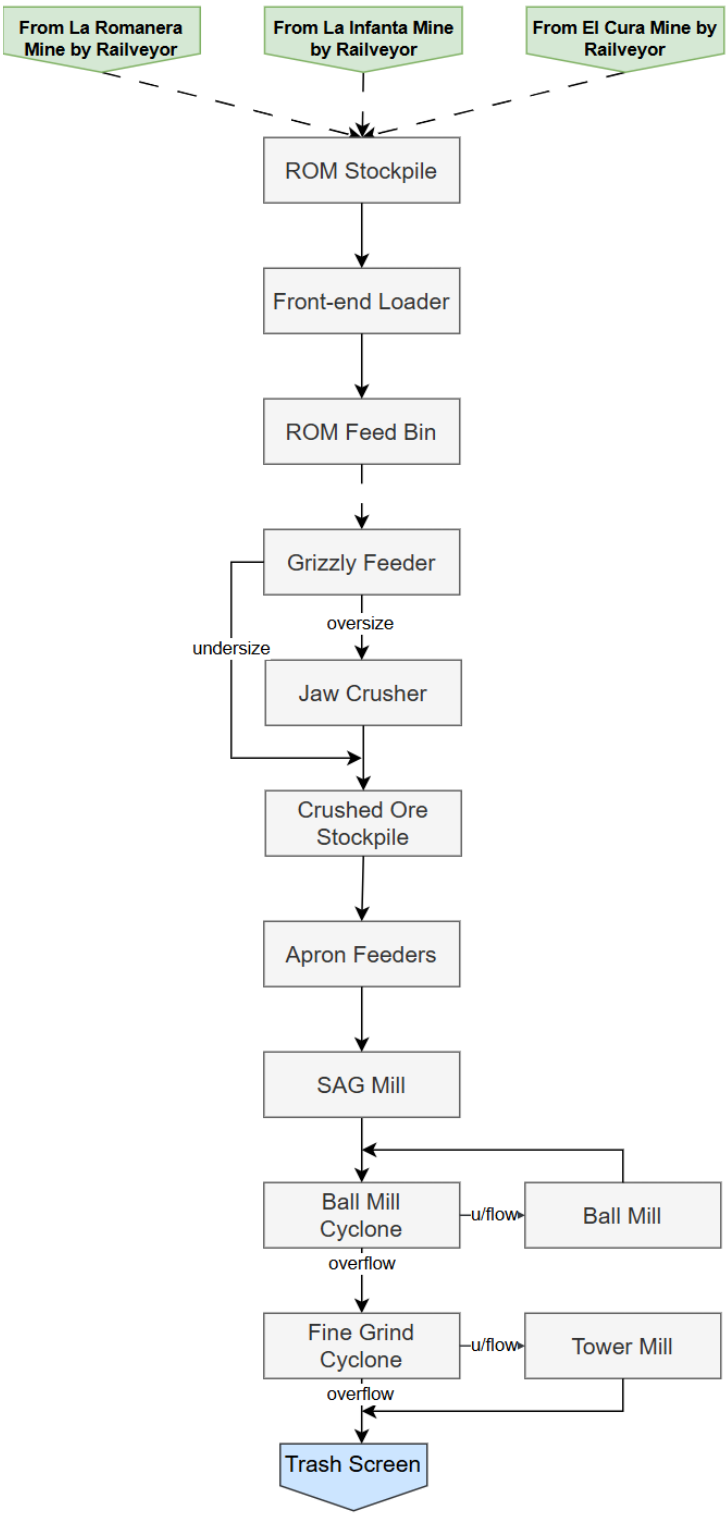
17.2 Process Flowsheet

The selected process flowsheet includes the following steps:

- ROM stockpile
- Primary crushing
- Crushed ore stockpile
- SAG mill in open circuit, secondary ball mill in closed circuit, and tertiary tower mill in closed circuit
- Copper flotation
- Copper concentrate thickening and filtration
- Lead flotation
- Lead concentrate thickening and filtration
- Zinc flotation
- Zinc concentrate thickening and filtration
- Pyrite flotation
- Pyrite concentrate thickening and filtration
- Tailings thickening and filtration for paste backfill and dry stacking on the IPS

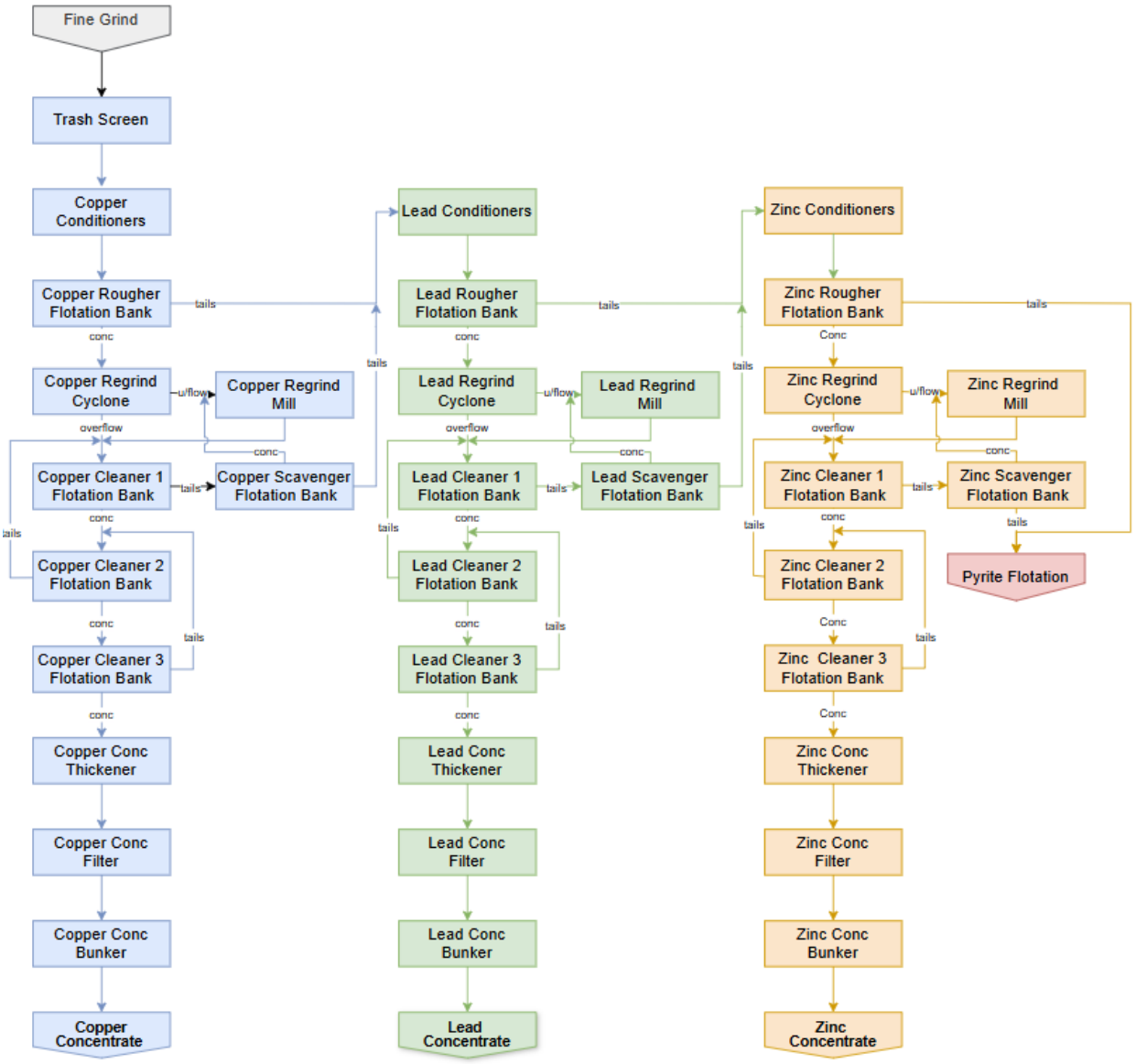
Figure 17-1 to Figure 17-3 illustrate the block flow diagrams for the process.

Figure 17-1: Comminution Block Flow Diagram



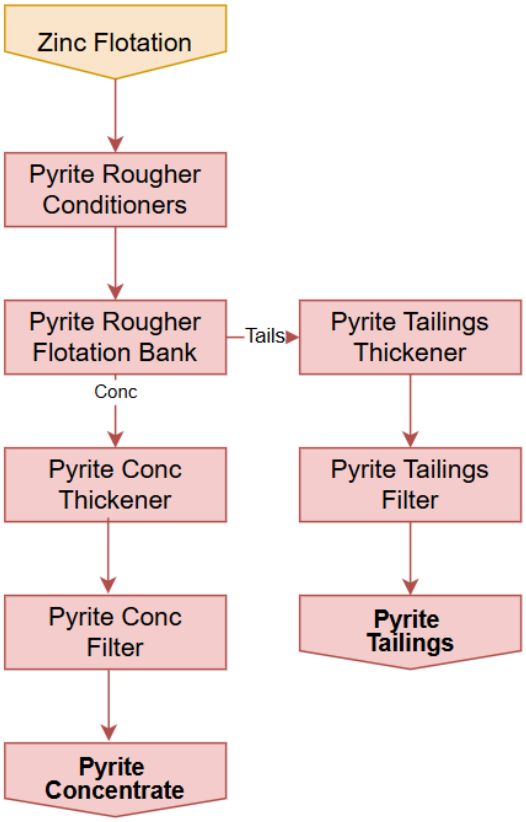
Source: Zenito, 2026

Figure 17-2: Base Metals Flotation Block Flow Diagram



Source: Zenito, 2026

Figure 17-3: Pyrite Flotation Block Flow Diagram



Source: Zenito, 2026

17.3 Key Process Design Criteria

The key process design criteria are listed in Table 17-1 and form the basis for the process flowsheet design and equipment specification). The process design calculations are based on the average head grades and testwork for La Romanera ore.

Table 17-1: Key Process Design Criteria

Parameter	Unit	Value
Plant throughput	tpa	1,200,000
Mill and flotation plant operating time	h/a	8,000
Crushing throughput	t/h	400
Milling and flotation throughput	t/h	150
Copper concentrate production	tpa	11,320
Lead concentrate production	tpa	29,346
Zinc concentrate production	tpa	51,330
Pyrite concentrate production	tpa	782,720
Tailings production	tpa	321,200

Parameter	Unit	Value
SAG milling configuration	-	Closed circuit with pebble crusher
Ball milling configuration	-	Closed circuit with cyclones
Tertiary circuit configuration	-	Cyclone underflow to mill
Tower mill product P_{80}	µm	45
Flotation circuits	-	Copper, lead, zinc, pyrite
Dewatering circuits	-	Copper, lead, zinc, pyrite concentrates, tailings

The average head grades used for the process design are presented in Table 17-2.

Table 17-2: Average Head Grades for La Romanera, La Infanta, and El Cura

Ore Source	% Copper	% Lead	% Zinc	% Sulphur
La Romanera	0.38	1.10	2.31	37.94
La Infanta	0.87	3.52	5.95	7.28
El Cura	0.98	0.58	1.22	32.57

The recoveries for each concentrate are as shown in Table 17-3 based on the LOM average ROM grades.

Table 17-3: Concentrate Recoveries and Grades

Concentrate, by deposit	Grade	Recovery
La Romanera		
Copper concentrate	20.4 % Cu	41.5 %
Lead concentrate	26.8 % Pb	52.2 %
Zinc concentrate	50.1 % Zn	78.7 %
Pyrite concentrate	1.49 g/t Au 49.6 g/t Ag	75.7 % 40.5 %
La Infanta		
Copper concentrate	20.2 %	42.4 %
Lead concentrate	47.9 %	78.3 %
Zinc concentrate	57.5 %	78.00 %
Pyrite concentrate	0.84 g/t Au 50.7 g/t Ag	32.1 % 7.2 %
El Cura		
Copper concentrate	22.9 %	79.4 %
Lead concentrate	4.2 %	2.7 %
Zinc concentrate	45.2 %	67.9 %
Pyrite concentrate	1.89 g/t Au 24.5 g/t Ag	75.1 % 32.0 %

17.4 Plant Description

17.4.1 Introduction

The process description is based on the process flow diagrams generated by Zenito. The flowsheet (Figure 17-4). The process plant will be located northwest of the portals of the three mines (see Figure 18-1 for infrastructure layout). A high-level overview of the process plant layout is shown in Figure 17-5.

Figure 17-4: PFD Colour Flow Sheet

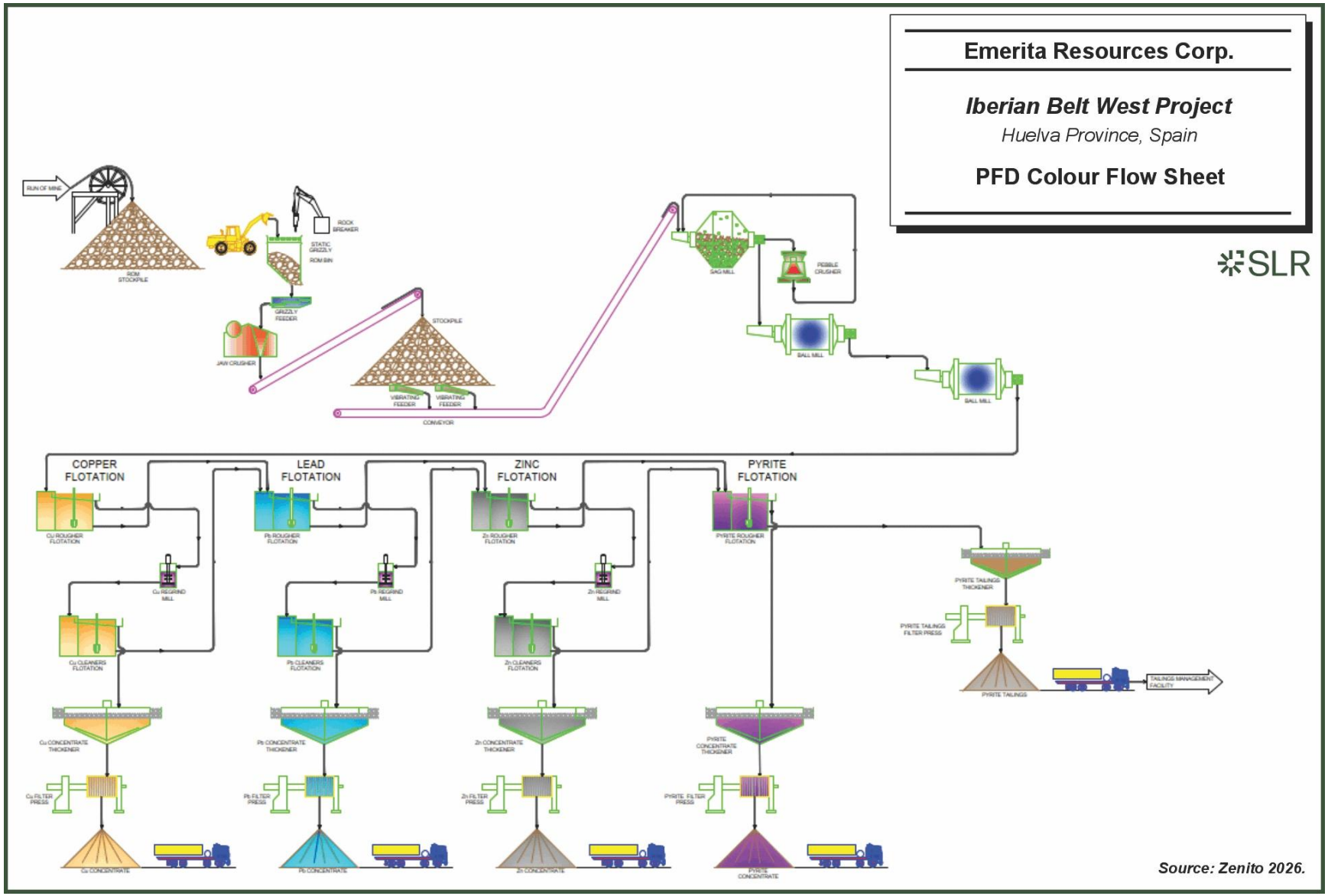
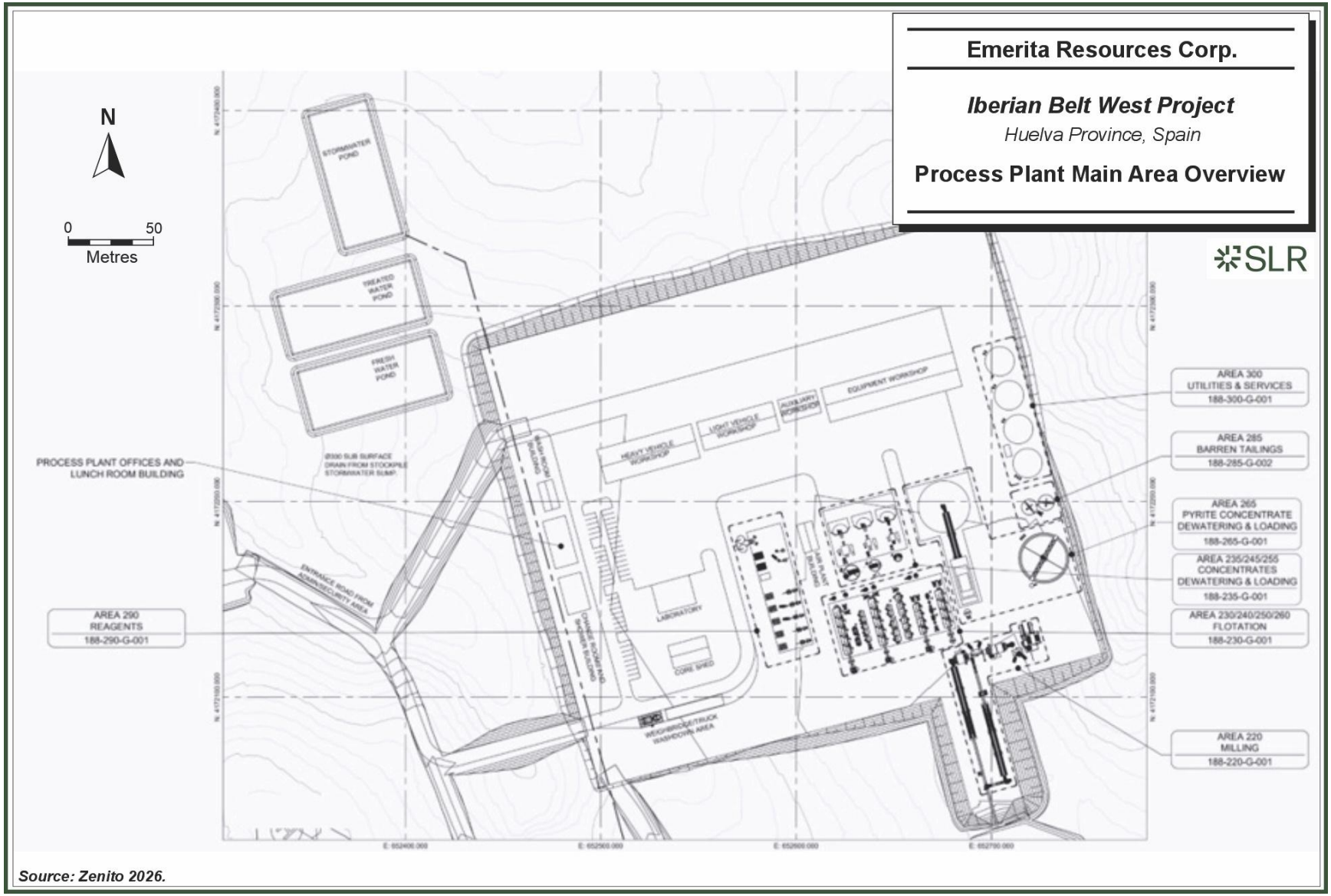


Figure 17-5: Process Plant Main Area Overview



Source: Zenito 2026.

17.4.2 ROM Pad and Primary Crushing

The main criteria for the crushing circuit is summarised in Table 17-4.

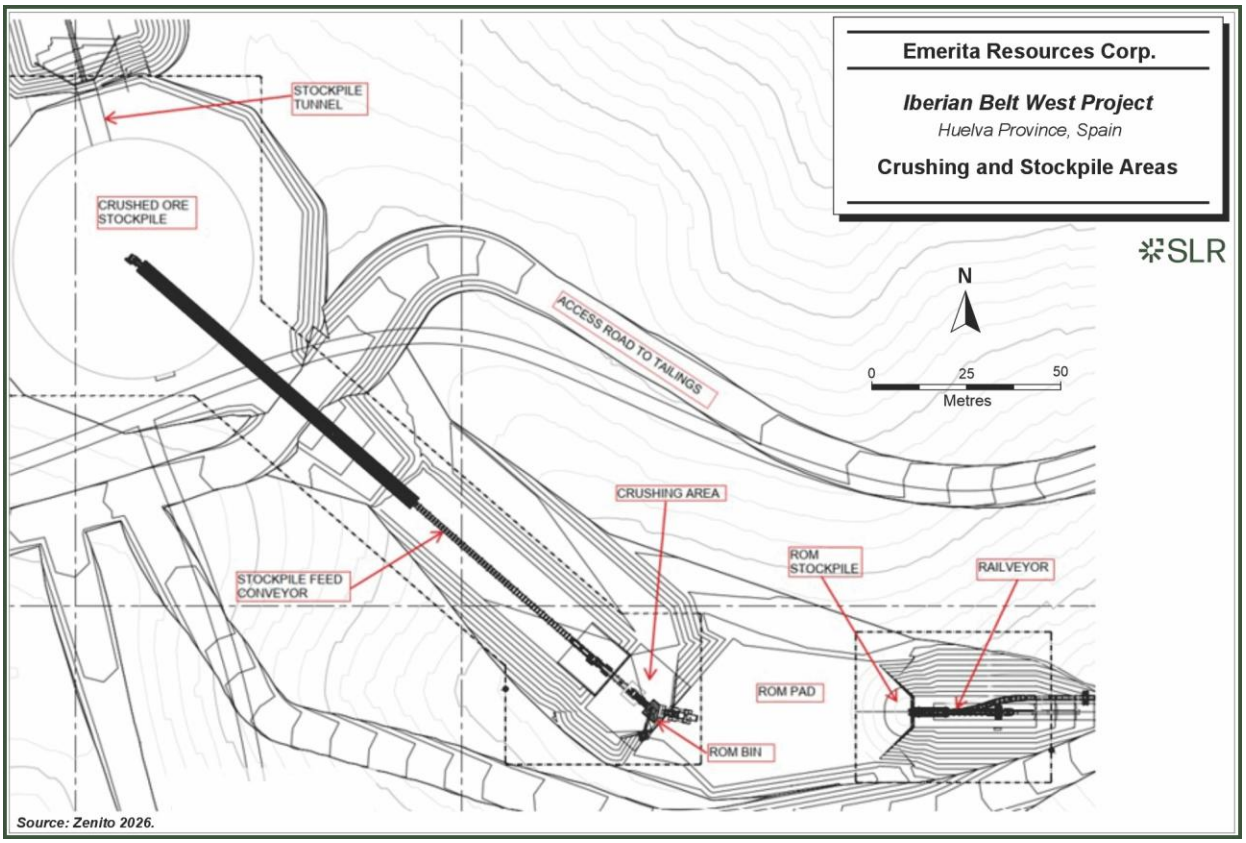
Table 17-4: Summary of Main Crushing Criteria

Parameter	Unit	Value
Crushing utilisation	%	75
Crusher type and size	mm	Jaw, 1200 x 870
Crushing throughput	t/h	400
Run of mine top size	mm	500
Crushing product P80	mm	87
Crushed ore stockpile live capacity	t	3,600

ROM ore will be conveyed to the surface from La Infanta, El Cura, and La Romanera by Railveyor, (a proprietary material handling system composed of a light rail train propelled by stationary drive stations developed by Rail-Veyor Technologies Global Inc) and discharged onto the ROM stockpile. Ore deposited at the ROM will be blended to even out the head grade feeding the flotation plant. The blended ore will be recovered by an FEL from the stockpile and dumped into the ROM bin through a static grizzly to prevent oversized rock (>500 mm) from entering the jaw crusher. A rock breaker located next to the grizzly at the ROM pad level will break the oversize so that it will pass through the static grizzly. The crushing equipment will be installed on a terrace 6.8 m lower than the ROM pad with a concrete retaining wall in between the two levels.

From the ROM bin, the ROM ore will be fed to the jaw crusher using a variable speed grizzly feeder. Small particles will pass through the feeder beams and fall onto the sacrificial conveyor. The oversize will be fed at a regulated rate into the jaw crusher where it will be crushed to -150 mm. The crushed ore will fall onto the sacrificial conveyor and be transported, together with the grizzly undersize, to the stockpile feed conveyor installed at a lower pad 4 m below the crushing pad. This conveyor will transport the crushed ore to the crushed ore stockpile. The crushing area is illustrated in Figure 17-6.

Figure 17-6: Crushing and Stockpile Areas



17.4.3 Crushed Ore Stockpile and Reclaim Tunnel

Located between the crushing area and main process pad, the crushed ore stockpile will be fed by the stockpile feed conveyor coming from the crushing plant. The crushed ore stockpile is 62 m diameter (approximately 24 hours milling) and will provide a buffer between the crusher, which will operate approximately 12 h/d and the milling circuit which will operate 24 h/d.

Two apron feeders will be installed inside a concrete reclaim tunnel located underneath the stockpile. In normal operations, with both apron feeders in operation, the live capacity will be 3,021 m^3. With only a single apron feeder operational, the live capacity drops to approximately 1,917 m^3. In this case, it is preferrable to specify design volume (m^3) rather than mass (tonnes), as the capacity of the stockpile in tonnes is somewhat variable depending on the bulk density (which varies from 2.5 t/m^3 to 4 t/m^3) of the ore from the different mines during the plant life.

17.4.4 Dust Suppression

Dust suppression will be a vendor package with its own control. Dust suppression will be based on dust capture. Collected dust will be fed back to the process.

17.4.5 Milling

The main criterion for the milling circuit is summarised in Table 17-5.

Table 17-5: Summary of Main Milling Criteria

Parameter	Unit	Value
Milling operating time	h/a	8,000
Milling throughput	t/h	150
Milling circuit product P_{80}	µm	45
Bond Ball Mill Work Index	kWh/t	14.37-14.79
Bond abrasion index		0.4189-0.6747
Primary mill type and size	m, kW	1 x SAG, 5.0 x 3.75, 1,400
Pebble crusher type		Cone
Secondary mill type and size	m, kW	1 x Ball, 4.5 x 6.75, 2,300
Tertiary mill type and size	kW	1 x Vertical stirred mill, 1,600

The crushed ore will be fed from the crushed ore stockpile onto the SAG mill feed conveyor by two variable speed apron feeders, with each one able to provide the required throughput on its own. The SAG mill feed conveyor will feed the SAG mill at a controlled rate. This rate will be controlled by a belt scale on the conveyor. Scats discharged from the SAG mill trommel will be recirculated by means of two conveyors and fed to a cone crusher which will discharge back to the stockpile reclaim conveyor and to the SAG mill. A magnet installed over the first recirculating conveyor will remove any steel from the circuit. Product from the SAG mill will be discharged to a pump box installed under the trommel and pumped to the ball mill cyclones from where the underflow solids will be fed by gravity to the ball mill feed chute. The product from the ball mill will be discharged to the same pump box where the SAG mill product is discharged, i.e., this pump box is shared by the two mills and located in between them. The mills will face each other at the discharge ends.

The overflow from the ball mill cyclones will be discharged to a pump box and pumped to the tower mill cyclones from where the underflow will be fed to a tower mill located underneath the cyclones for a tertiary milling stage. The tower mill product will be pumped back to the cyclones in closed circuit from which the overflow will feed by gravity to the first copper conditioner tank in the flotation area.

17.4.6 Flotation and Dewatering

The main criterion for the flotation circuit is summarised in Table 17-6.

Table 17-6: Summary of Main Flotation Criteria

Parameter	Unit	Value
Copper flotation circuit feed	t/h	150
Rougher cell size	m^3	4 x 30
Rougher design retention time	min	20
Copper regrind mill type	-	1 x Vertical stirred
Copper regrind mill power	kW	550
Fresh feed to regrind mill circuit	t/h	10.3

Parameter	Unit	Value
Regrind circuit product P80	µm	15
Copper cleaner 1 and scavenger cell volume	m^3	5 x 2.3
Copper cleaner 1 and scavenger design retention time	min	22
Copper cleaner 2 feed	t/h	3.0
Copper cleaner 2 cell volume	m^3	2 x 2.3
Copper cleaner 2 flotation design retention time	min	45
Copper cleaner 3 feed	t/h	2.55
Copper cleaner 3 cell volume	m^3	1 x 1.5
Copper cleaner 3 flotation design retention time	min	26
Lead flotation feed	t/h	148.6
Rougher cell size	m^3	5 x 50
Rougher design retention time	min	33
Rougher lead concentrate yield	%	25
Lead regrind mill type	-	1 x Vertical stirred mill
Lead regrind mill power	kW	2,500
Fresh feed to regrind mill circuit	t/h	37.1
Regrind circuit product P_{80}	µm	15
Lead cleaner 1 and scavenger cell volume	m^3	5 x 20
Lead cleaner 1 and scavenger flotation design retention time	min	50
Lead cleaner 2 feed	t/h	23.9
Lead cleaner 2 cell volume	m^3	4 x 20
Lead cleaner 2 flotation design retention time	min	25
Lead cleaner 3 feed	t/h	13.0
Lead cleaner 3 cell volume	m^3	2 x 20
Lead cleaner 3 flotation design retention time	min	28
Zinc flotation feed	t/h	144.9
Rougher cell size	m^3	5 x 50
Rougher design retention time	min	42
Rougher Zinc concentrate yield	%	19.2
Zinc regrind mill type		1 x Vertical stirred mill
Zinc regrind mill power	kW	1,500
Fresh feed to regrind mill circuit	t/h	27.8
Regrind circuit product P80	µm	10
Zinc cleaner 1 and scavenger cell volume	m^3	4 x 10

Parameter	Unit	Value
Zinc cleaner 1 and scavenger flotation design retention time	min	38
Zinc cleaner 2 feed	t/h	8.0
Zinc cleaner 2 cell volume	m^3	3 x 3
Zinc cleaner 2 flotation design retention time	min	20
Zinc cleaner 3 feed	t/h	5.42
Zinc cleaner 3 cell volume	m^3	2 x 3.0
Zinc cleaner 3 flotation design retention time	min	25
Pyrite flotation feed	t/h	141.5
Rougher cell size	m^3	4 x 50
Rougher design retention time	min	40
Rougher pyrite concentrate yield	%	64.9

17.4.6.1 Base Metal and Pyrite Flotation

There will be four flotation concentrates produced: copper, lead, zinc, and pyrite. There will be three flotation circuits for each of the base metals, consisting of roughers, regrind of rougher concentrate, primary cleaner with cleaner scavenger, secondary cleaner, and tertiary cleaner. The tailings from the cleaner scavenger will be recycled to the regrind mill. The tailings from the secondary and tertiary cleaners will be recycled back to the previous flotation stage. The rougher tailings together with the cleaner scavenger tailings will report to the next flotation circuit, i.e., copper tailings to the lead rougher, lead tailings to the zinc rougher, and zinc tailings will be pumped to the pyrite rougher.

There will only be a bulk roughing stage for the pyrite with the rougher concentrate fed to the pyrite concentrate dewatering circuit and the tailings to the pyrite tailings dewatering circuit.

Each concentrate flotation line will be located inside a steel framed, non-insulated, cladded building located adjacent to each other so that operators can easily access the different flotation lines across the four buildings. A hoist will run above each flotation line along an I-beam supported by its own structure for maintenance purposes. This arrangement reduces the span of the roof structures and therefore the associated costs of the roof and overhead cranes.

17.4.6.2 Copper, Lead, Zinc, and Pyrite Flotation

The cyclone overflow from the tertiary milling stage will flow by gravity to the copper conditioning tanks, which will operate in series. Reagents will be added to the two tanks before the slurry overflows to the copper rougher bank of flotation cells where a concentrate will be floated. This concentrate will be pumped to a cyclone in the copper regrind circuit. The cyclone underflow will flow to the copper regrind mill which fine grinds the coarse particles. The discharge of the mill joins the cyclone overflow and will be pumped to the first copper cleaner bank of flotation cells where the concentrate will be upgraded. The concentrate from this bank will be pumped to the second bank of copper cleaner flotation cells where the concentrate will be further upgraded. The concentrate will be pumped to the third bank of copper cleaner flotation cells where the final copper concentrate will be produced. This concentrate will be pumped to the copper concentrate thickener.

The tailings from the third bank of copper cleaner flotation cells will flow by gravity to the second bank and the tailings from this bank will flow by gravity to the first bank. The tailings from the first bank will flow by gravity to the copper cleaner scavenger flotation bank which will float any unliberated copper minerals. This concentrate will be pumped to the copper regrind milling circuit for further grinding to liberate the copper minerals.

The tailings from the copper rougher and cleaner scavenger flotation banks will be pumped to the lead flotation circuit. The lead flotation circuit is a copy of the copper circuit; only differing in the number of cells and size of the banks. The tailings from the lead rougher and cleaner scavenger flotation banks will be pumped to the zinc flotation circuit, which again repeats the same configuration as the previous circuits and only differs in number of cells and sizes.

17.4.7 Concentrates Dewatering and Loading

The main criteria for the concentrate dewatering circuits are summarised in Table 17-7.

Table 17-7: Summary of Main Concentrate Dewatering Criteria

Parameter	Unit	Value
Copper concentrate thickener feed solids rate	t/h	1.4
Copper concentrate thickener type	-	Hi-rate
Thickener diameter	m	4
Copper concentrate cake moisture	%	10
Filter type	-	1 x Plate and frame
Total filtration area	m^2	4.7
Lead concentrate thickener feed solids rate	t/h	3.73
Lead concentrate thickener type	-	Hi-rate
Thickener diameter	m	4
Lead concentrate cake moisture	%	10
Filter type	-	1 x Plate and frame
Total filtration area	m^2	9.5
Zinc concentrate thickener feed solids rate	t/h	6.87
Zinc concentrate thickener type	-	Hi-rate
Thickener diameter	m	8
Zinc concentrate filter feed solids	t/h	6.87
Zinc concentrate filter feed slurry	m^3/h	4.67
Cake moisture	%	10
Filter type	-	1 x Plate and frame
Total filtration area	m^2	18.9
Pyrite concentrate thickener feed solids rate	t/h	97.8
Pyrite concentrate thickener type	-	Hi-rate
Thickener diameter	m	25

Parameter	Unit	Value
Pyrite concentrate filter feed solids	t/h	97.8
Cake moisture	%	10
Filter type	-	1 x Plate and frame
Total filtration area	m^2	264
Pyrite tailings thickener feed solids rate	t/h	40.1
Pyrite tailings thickener type	-	Hi-rate
Thickener diameter	m	12
Cake moisture	%	10
Filter type	-	1 x Plate and frame
Total filtration area	m^2	108

The three base metal concentrates (copper, lead, zinc) will each be pumped to dedicated thickeners where the slurry will be thickened. The underflow will then be pumped to dedicated concentrate pressure filters. The filters will produce filter cakes with a moisture content suitable for transportable moisture limit. From the filter, each concentrate cake will drop by gravity to a conveyor located underneath each filter that will feed the concentrate stockpiles in dedicated bunkers from where the concentrates will be transferred using FELs into trucks for transporting to market.

The overflow from the three concentrate thickeners and the filtrate from the filters will be transferred to a shared process water transfer tank located near the Lead Thickener and recycled to the process water tank.

The dewatering equipment and stockpiles for each of the three concentrates are located indoors to protect the filter cloths and to store the concentrates in an enclosed environment. The three structures around the filters will be attached, forming one single building with an access door for trucks in front of each stockpile.

A hoist above each dewatering line will be installed on its own support structure for the maintenance works of the equipment.

17.4.7.1 Pyrite Concentrate Dewatering and Loading

Pyrite concentrate will be dewatered in a separate building due to the much larger size of dewatering equipment and concentrate stockpile.

The pyrite concentrate from the pyrite rougher flotation circuit will be pumped to the pyrite concentrate thickener. The thickener underflow will be pumped to a holding tank before being pumped to a pressure filter. Pyrite concentrate cake will drop by gravity onto a collecting conveyor under the filter that will transfer the cake to a stacker which will feed a 26 m diameter stockpile. Pyrite concentrate will be loaded by a FEL into a truck for transporting to the port or refinery. The filter will reduce the moisture to a level suitable for transporting by truck off site for sale to market.

The filtrate from the filter will be recycled to the return process water tank.

The pyrite building comprises two structures: a long, narrow structure for the filter and a larger square structure for the stockpile with a large opening on the side closest to the filter discharge.

A hoist above the filter press will be installed on its own support structure for the maintenance works of the equipment.

17.5 Reagents

The reagents area consists of three different sub-areas: the solid and liquid storage areas located indoors, and the lime storage area located in two outdoor silos.

17.6 Key Process Reagents

The principal reagents used for the base metal and pyrite flotation circuits and the consumptions for each ore source are shown in Table 17-8. The reagent consumptions are taken from the flotation tests.

Table 17-8: Key Process Reagents

Reagents[1]	Unit	Consumption for La Romanera	Consumption for La Infanta	Consumption for El Cura
Copper Flotation				
MIBC	g/t ROM	25	20	25
Lime	g/t ROM	7,110	1,598	2,160
SMBS	g/t ROM	1,450	1,200	1,100
$ZnSO_4$	g/t ROM	400	700	500
527E	g/t ROM	100	NA	75
CMC	g/t ROM	NA	500	NA
F1234	g/t ROM	NA	135	NA
Lead Flotation				
MIBC	g/t ROM	20	87	100
Lime	g/t ROM	198	315	210
SMBS	g/t ROM	400	600	400
$ZnSO_4$	g/t ROM	400	600	400
3418A	g/t ROM	95	85	43
Zinc Flotation				
MIBC	g/t ROM	100	225	92
Lime	g/t ROM	1,243	1,090	895
$CuSO_4$	g/t ROM	700	700	300
SIPX	g/t ROM	175	145	80
Pyrite Flotation				
Lime	g/t pyrite feed	1,080	0	0
H_2SO_4	g/t pyrite feed	NA	6,680	2,625
$CuSO_4$	g/t pyrite feed	450	759	210

Reagents[1]	Unit	Consumption for La Romanera	Consumption for La Infanta	Consumption for El Cura
PAX	g/t pyrite feed	108	182	31
MIBC	g/t pyrite feed	44	19	57

Notes:
1. Methyl isobutyl carbinol (MIBC); Sodium metabisulphite (SMBS); Carboxymethyl cellulose (CMC); Sodium isopropyl xanthate (SIPX); Potassium amyl xanthate (PAX)

In addition, flocculant will be added to the slurry flows going to the thickeners to improve the settling rates and clarity of the overflows. These have been estimated since no settling testwork has been performed.

17.6.1 Solid Reagents

Solid reagents make-up equipment and storage will be in a prefabricated steel frame building with non-insulated cladding. The make-up equipment for each reagent will be installed along one side of the building with a hoist and an enclosed hopper with bulk bag breakers above the associated make-up tank. The reagents will be stored directly opposite the make-up equipment on the other side of the building to minimise reagent handling time. The building will have a mono-pitch roof with the highest edge on the reagents make-up side of the building where more height is required.

17.6.2 Liquid Reagents

Liquid reagents make-up equipment and storage will be located in a prefabricated steel frame building with non-insulated cladding. The make-up equipment for each reagent will be installed along one side of the building. The reagents will be stored directly opposite the make-up equipment on the other side of the building to minimise reagent handling time. The building will have a double-pitch roof as no extra-height is required between storage and make-up.

17.6.3 Lime

Lime will be delivered in powder form and stored in two silos which will be located outdoors next to the liquid reagents building. The lime will be delivered from delivery tanker trucks to the silos by means of pneumatic conveying. The lime will be fed to the make-up tank by screw feeders. Bin activators will be installed at the bottom of the silos to ensure the lime flows as required.

17.7 Tailings Dewatering Area

The tailings dewatering area will be located near the IPS and tailings slurry will be pumped 1.5 km from the process plant to the tailings dewatering pad.

The slurry will be thickened in the pyrite tailings thickener from which the underflow will be pumped to a holding tank. and from there to a filter. The overflow will be piped back to the main process water tank at the process plant by gravity, as the thickener overflow is 22 m higher than the top edge of the process water tank.

17.8 Utilities - Processing and Surface Infrastructure

The utilities and services for the Project are outlined below.

17.8.1 Power

A 30 kV grid power line will be installed by the grid authority to supply the site.

Plant overall power requirements are shown in Table 17-9.

Table 17-9: Installed Power and Annual Power Consumption – Processing and Surface Infrastructure

Installed Power (kW)	Reactive Power (kvar)	Annual Consumption (kWh)
18,654	6,805	116,917,074

The power distribution data across the plant is shown in Table 17-10.

Table 17-10: Plant Distribution Voltage

Distribution Voltage	Unit	Detail
High Voltage (Transmission)		
Voltage	kV	30
Frequency	Hz	50
Phase	-	3
High Voltage (On-site distribution)		
Voltage	kV	15
Frequency	Hz	50
Phase	-	3
Medium Voltage (Equipment)		
Voltage	kV	6
Frequency	Hz	50
Phase	-	3
Low Voltage - Motors		
Voltage	V	400
Frequency	Hz	50
Phase	-	3
Low Voltage – General 3-Phase		
Voltage	V	400
Frequency	Hz	50
Phase	-	3
Low Voltage – General Single Phase		
Voltage	V	230
Frequency	Hz	50

Distribution Voltage	Unit	Detail
Phase	-	3
Medium Voltage Switchgear Control Voltage		
Voltage	VDC	110
Control Voltage (Motor control centre [MCC], control panels, heaters, solenoid valves)		
Voltage	V	110
Frequency	Hz	50
Phase	-	3

17.8.2 Air

17.8.2.1 High Pressure Air

The air compressors will be provided as vendor packages with their own control systems. These rotary screw compressors will supply high pressure compressed air for use as instrument air with minor use as process air. The vendor controller package will sense the air requirements and automatically start the second unit or put the compressor on idle as needed. Air filters are equipped with high differential pressure indicators to alert when the filter cartridge element is blocked. Each air receiver includes a pressure gauge and pressure transducer, with readings displayed on the supervisory control and data acquisition (SCADA) hardware. There will be two air compressors, one duty and one standby.

17.8.2.2 Low Pressure Air

The flotation cells will require low pressure air. There will be two air blowers (one duty and one standby) for all flotation plant. Air will be split and distributed as per each flotation line requirements. These will be provided as packages with their own control systems. The blowers will have variable speed drives (VSDs) to automatically adjust the speed to the air demand. Flow control of the flotation air will be manually adjusted at the flotation cells. There will be flow indicators at each flotation cell.

17.8.3 Water

17.8.3.1 Raw Water

A level sensor will be situated on the raw water tank. The level reading will be displayed on the SCADA and available as a trend. High and low levels will cause the relevant alarms and interlocking.

A flow meter will be situated on the raw water discharge pipe, and automatically measure the flow rate that will be linked to relevant alarms and interlocking.

A reserve for fire water will be held in the raw water tank. All other services draw water from above this reserve level.

17.8.3.2 Process Water

A level sensor will be situated on the process water tank. High and low levels will trigger the relevant alarms and interlocking. A flow meter will be situated on the process water makeup pipe.

The process water tank will be filled with overflow water from the concentrate and tailings thickeners, which will be transported to smaller transfer tanks where required, and pumped to the main process water tank. Make-up water for this tank will be a take-off from the pumped raw water. The process water tanks will be fitted with a float valve to maintain the appropriate level.

17.8.3.3 Potable Water

Potable water will be supplied to the plant from the general services potable water line.

17.8.3.4 Gland Water

The gland water will be filtered raw water, and controlled with a float valve. Pressure switches will be installed on the gland water pump and booster pump discharges.

17.9 Sampling Protocol

The sampling protocol for process control and metallurgical accounting uses automatic samplers on slurries where applicable. Composite samples will be taken over timed intervals, collected at the end of the shift and taken to the laboratory for analysis. Cross-cut slurry samplers will be used at key locations in the process., feed to copper flotation (head grade), final concentrates, and tailings. These samples will be analysed for the purpose of metallurgical accounting.

In addition, key process slurry streams will be sampled by pipe samplers and assayed online using an XRF device. The centrally located unit will be fed from multiple areas. The analyser output will be displayed on the SCADA for the key target and penalty elements. This will provide data for process control purposes.

17.10 Process Control

17.10.1 General

The process plant will contain sufficient instrumentation to enable the efficient production of a consistent quality of concentrates at an optimal rate. The basis of the control philosophy will ensure that the plant is safe to operate and simple to control.

The plant will include dedicated programmable logic controllers (PLCs) that will monitor and control plant functions. The PLCs will be interfaced with a desktop, computer-based SCADA system, which will be located in a dedicated control room inside the flotation building. The SCADA system will serve as the interface between operators and the PLCs, allowing operational personnel to make alterations to control loops as well as monitor data in the form of instantaneous measurements or logged data. The operators will be able to perform remote start-up and shutdown.

Certain packaged equipment (e.g., filters and thickeners) will typically be supplied with dedicated, vendor-programmed local PLCs to handle their specific sequencing and interlocks. These PLCs will be integrated into the main SCADA network for centralised monitoring and high-level setpoint adjustment.

17.10.2 Crushing and Milling

Feed to the crushing circuit will be controlled by mass flow meters to optimise the throughput.

The milling circuit will have the following controls:

- Feed rate control: the fresh feed rate will be controlled against mill power draw and/or bearing (load cell) pressure.
- Water/dilution control: sump and mill discharge water addition will be controlled based on cyclone feed density and mill feed density.
- Speed control: variable-speed drive of the SAG mill, speed adjustment to optimise power/load.

17.10.3 Flotation

The overall flotation circuit control philosophy is the optimisation of grade/recovery at each stage via the following controls.

- Level control: pulp level/froth depth automated per cell to stabilise residence time.
- Reagent control: collector/frother/depressant/activator dosing proportionate to circuit feed tonnage and analysis.
- pH control: lime addition to control the pH.
- Aeration control: air flow per cell tuned for bubble-particle contact and to manage froth stability/entrainment.
- On-stream analysis: samples of the important streams will be taken automatically and transferred to an analyser which will provide elemental analysis to enable assessment of the process.
- Metallurgical accounting: mass balance reconciliation across the four concentrate streams and final tailings.

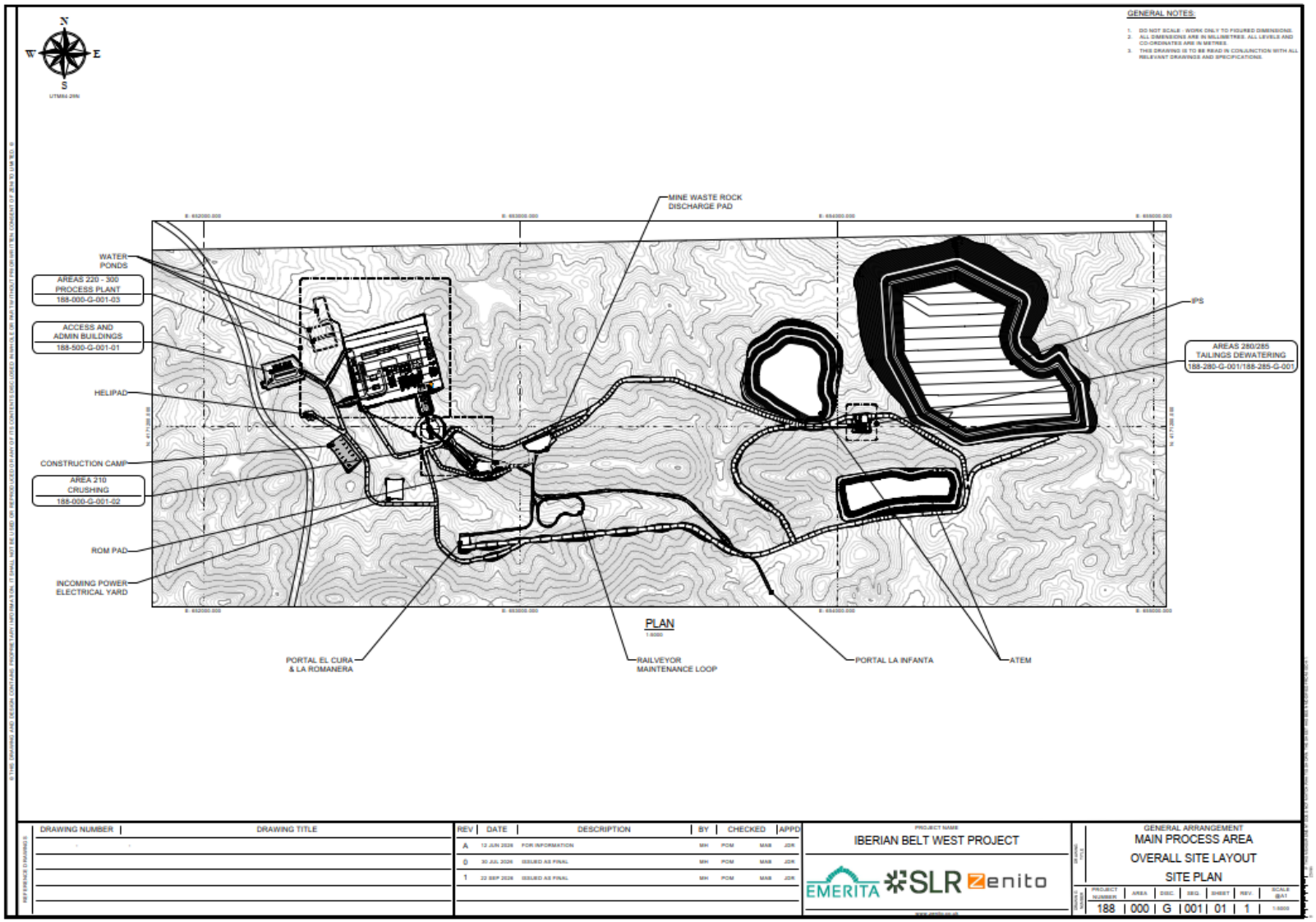
18.0 Project Infrastructure

Figure 18-1 illustrates the general infrastructure layout for the IBW Project (Appendix 18-1: Site Access and Transportation.

18.1.1 Project Roads and Access

The site access control gate will be located to the west of the process plant near the HU-5401 road (Figure 18-1). A main road and access roads within the Project boundary will be 9 m wide constructed of gravel, intended for two-way traffic. The site roads will connect all infrastructure locations within the Project boundary, with roads connecting the administration buildings, process plant, mine waste storage facilities (*Acopio Temporal de Estériles de Mina*, ATEMs), Integrated Process Residue Storage Facility (IPS), tailings dewatering area and mine portals.

Figure 18-1: General Layout



Source: Zenito 2026.

18.1.2 Local and Regional Road Traffic and Logistics

Local and regional roads outside of the Project boundary will see additional traffic as a result of the Project. The estimated increase in operational traffic due to Project product shipments is presented in Table 18-1. It is expected that an average of seven truck movements per day will be required for reagent and consumable deliveries. Additional traffic will be generated due to staff commuting and other mining activities. Project construction traffic should also be considered in due course.

Table 18-1: Additional Traffic due to Product Shipment

Product	Production (t/week)	Truck Load Capacity (t)	Days Loading per Week	Average Number of Trucks per Day
Pyrite	16,148.16	29	6	92.81
Copper	208.32	29	6	2.00
Lead	584.64	29	6	3.36
Zinc	1,078.56	29	6	6.20
			Total	**104.4**

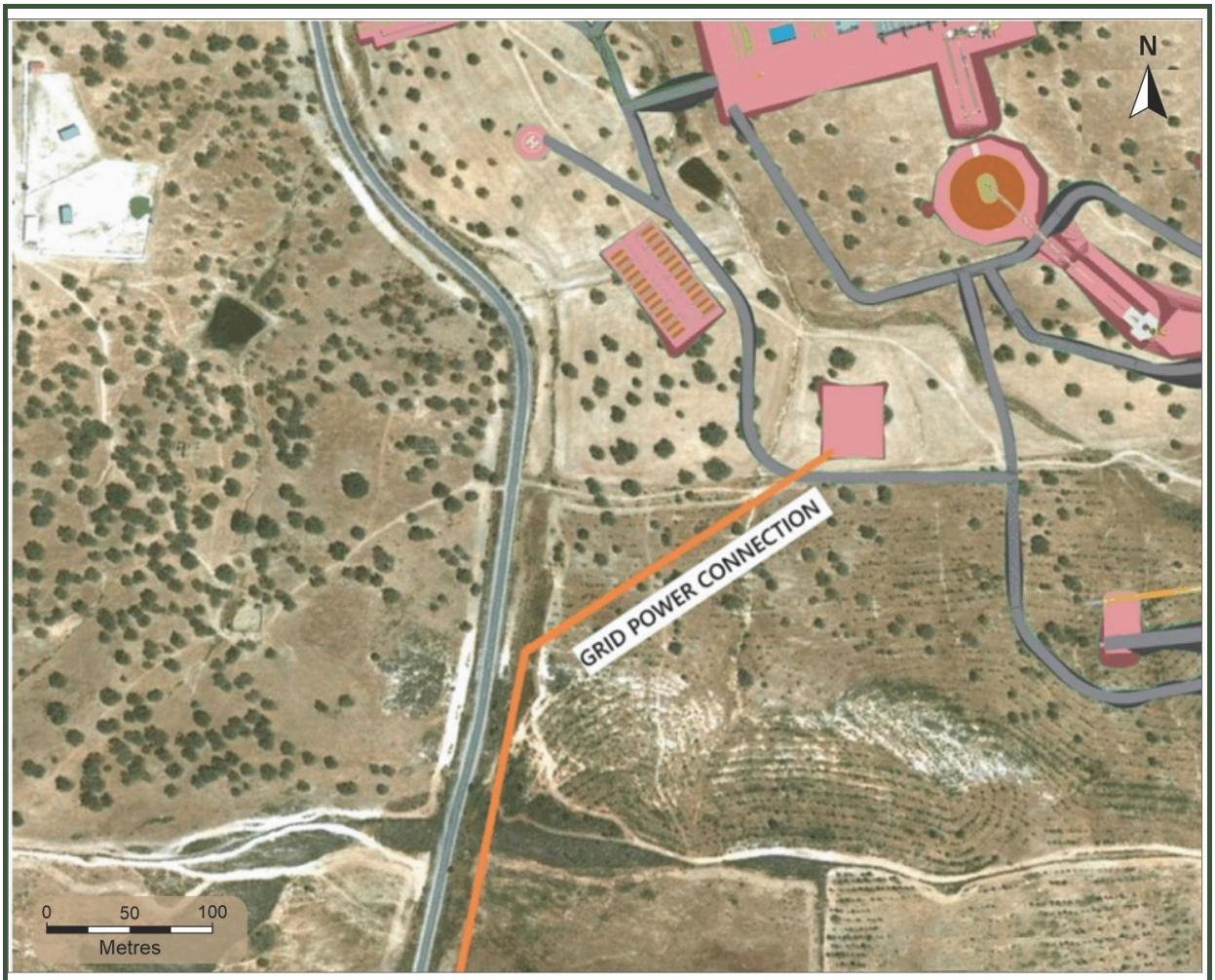
18.1.3 Airstrips, Rail Connections and Port Facilities

The accessibility is discussed in further detail in Section 5.1.

18.2 Power Infrastructure

The Project will be supplied from grid power from the grid substation at Puebla de Guzman, located at 37°32'56"N 7°14'30"W. A new connection will be required and the grid authority, Red Eléctrica de España, a public company responsible for granting access points and connections to the grid, will be responsible for this overland grid connection. Figure 18-2 illustrates the approximate grid power route connecting from the south to the on-site electrical yard.

Figure 18-2: Grid Power Supply



SLR

Emerita Resources Corp.

Iberian Belt West Project
Huelva Province, Spain

Grid Power Supply

Source: Zenito 2026.

The overall power requirements for the site are shown in Table 18-2. The processing and surface infrastructure has installed loads of 18.7 MW and estimated energy consumption of 116,917 MWh/a. Underground mining and underground infrastructure will be additional to the amount at approximately 8.1 MWh installed and 35,947 MWh/a annual consumption, calculated from the underground mining models for the three orebodies and their corresponding equipment duty and utilisation profiles.

Emerita have been in discussions existing power-generating companies in Huelva Province and with stakeholders involved in power projects currently in the permitting stage to source 80 MW to 100 MW connection from nearby renewable projects and the grid and this would be more than sufficient for current project requirements.

Puebla de Guzmán is host to a transmission-and-renewables cluster on the south side of the town, which are represented by several industrial-scale substations or SETs (subestación eléctrica de transformación). These include Red Eléctrica's 400 kV park which connects Spain to Portugal (Guillena–Puebla–Tavira) and its 220 kV SET finished in 2024. This the El Andévalo district's main evacuation node for hundreds of megawatts, managed by numerous service providers as issued through Red Eléctrica. Emerita currently maintains a 30 MW reservation on this node for which it issues payment on a quarterly basis refundable upon the securing of a service provider to access this node reconsidered through power supply for the same amount.

Table 18-2: Power Requirements by Area for the Project

Area Number	Installed Power (kW)	Reactive Power (kvar)	Annual Consumption (kWh)
100 - Mining	8,127	6,095	35,946,756
200 - General	1,170	526	4,550,838
210 - Crushing	591	228	2,970,691
220 - Milling	6,814	1,925	46,123,678
230 - Copper Flotation	1,007	410	6,892,245
235 - Copper Dewatering	72	38	387,420
240 – Lead Flotation	3,652	1,310	25,489,988
245 – Lead Dewatering	82	44	451,193
250 – Zinc Flotation	2,288	843	15,892,182
255 – Zinc Dewatering	82	44	443,221
260 – Pyrite Flotation	490	236	2,483,951
265 – Pyrite Dewatering	265	156	1,638,961
280 - Pyrite Tailings	250	138	1,364,738
290 - Reagents	126	74	586,710
300 - Utilities	1,190	577	6,130,160
400 - Infrastructure	575	259	1,511,100
Total	**26,781**	12,903	**152,863,832**

18.3 Water Management

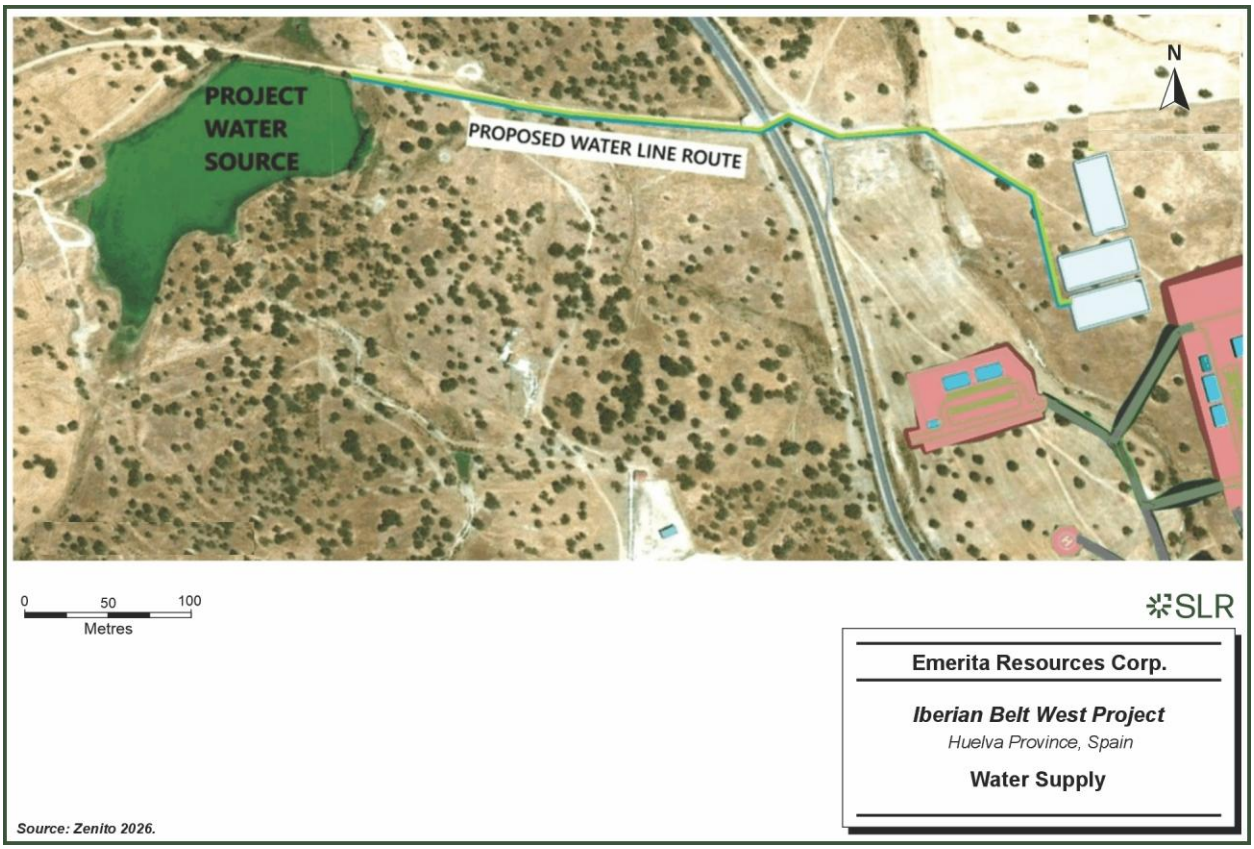
18.3.1 Water Supply

The Project sits 1 km to 2 km from the Andevalo Reservoir, (Figure 18-3). Emerita currently has a water permit to use water from the reservoir during exploration activities. In addition, the Company has applied for an Industrial Water Permit with the Confederación Hidrográfica del Guadiana which, if granted, will be effective in 2028 and subject to renewal every 5 years. Possessing this permit will grant Emerita a volume of 1.51 hm^3 per year (1 hm^3 = 1 x 10^6 m^3) under the 2028–2033 Water Management Plan to be sourced from the greater Andévalo Reservoir (water body ES040MSPF000206510).

An agricultural water allocation from the Guadiana River of 15 hm^3 exists of which only 2.3 hm^3 is being utilised. Unused allocation by the agricultural community (*comunidad de regantes*) within this allocation can be used for industrial purposes, but a company must receive permission from the agricultural community in order to do so. Emerita is actively negotiating access with the agricultural community to secure a portion of the agricultural water allocation to ensure industrial water supply during the interim between the present and the expected granting of the Industrial Water Permit allocation in January 2028. These negotiations are ongoing at the time of this report. Emerita has all the necessary water permits to complete its ongoing exploration activities, as they fall under the permissions granted by the AAU for these activities.

Water supply permits are not singular in their issuance as several parallel permitting streams must all be completed in order to secure water. Permissions for water will not be granted until the planning reserve, the AAU, the mining concession and the water concession are all in place.

Figure 18-3: Water Supply



18.3.2 Water Ponds and Drainage

A stormwater attenuation pond for capturing rainwater runoff will be located on the northwest side of the process plant. This pond will collect the stormwater from a drainage channel running from south to north along the western edge of the pad.

Two additional ponds will be located adjacent to the stormwater attenuation pond for raw/fresh water and treated water storage.

18.4 Process Plant Infrastructure

The process plant offices will be in a two-storey building with capacity for 10 desks, one meeting room, and a lunchroom. Adjacent to this building are the showers and locker room building for 20 people and 90 lockers.

18.5 Tailings and Waste Management

18.5.1 Mine Waste Management

Mine waste generated from underground development and mining operations will be managed through a combination of direct underground reuse, rockfill and CRF placement, temporary surface storage, and subsequent reuse. The ATEM provides the principal surface mine waste management facility and is also a potential source of suitable rockfill and closure material, subject to geotechnical and geochemical suitability and schedule availability.

The selected ATEM has a nominal storage capacity of approximately 844,000 m³ and a combined footprint of approximately 8.0 ha. The current mining schedule identifies approximately 3.91 Mt of total waste, of which approximately 2.47 Mt is routed to surface before reuse or return underground; this larger, time-dependent waste profile therefore controls the operational capacity assessment.

Mine waste is managed conservatively as sulphide-bearing material pending confirmation of the detailed geochemical, leachability, and drainage characteristics. The facility basis therefore incorporates controlled runoff and seepage management, clean water diversion, contact water collection, monitoring, and closure provisions.

The static ATEM capacity should not be interpreted as demonstrating adequate storage for all mine waste generated under the current mining schedule. PFS capacity assessment indicates that the existing ATEM is not sufficient for the unconstrained case in which all surface-routed waste passes through the facility. The selected operating basis therefore requires direct underground reuse and controlled routing/drawdown to manage peak occupancy. An additional temporary storage or expansion case of approximately 1.20 Mm³ is retained as a sensitivity should the required reuse and routing strategy not be achieved.

The recovery and sale of pyrite concentrate provides an additional waste management benefit by removing a substantial proportion of the sulphide-bearing material from the final flotation tailings stream. This reduces the quantity of residual tailings requiring management through underground paste backfill or surface storage. Combined with the selected PFS strategy of maximising underground reuse of suitable filtered tailings, pyrite concentrate production materially reduces the long-term surface tailings storage requirement and associated facility footprint compared with a conventional arrangement without pyrite recovery. The magnitude of this benefit is dependent on achieving the assumed metallurgical performance and securing commercially viable pyrite concentrate sales.

Closure planning includes final landform development, long-term drainage and runoff controls, cover and rehabilitation measures, and allocation of suitable mine waste to the IPS closure requirements where applicable.

Further Feasibility Study work should include updated waste-rock characterisation, confirmation of geotechnical and geochemical material classes, detailed annual routing and ATEM occupancy modelling, reconciliation with rockfill and CRF demand, confirmation of closure-material requirements, and detailed closure design.

18.5.2 Surface Residue Storage Facility

Filtered flotation tailings not placed underground as paste will be managed within the IPS. The selected PFS philosophy maximises beneficial underground use of suitable final flotation tailings and therefore substantially reduces the surface storage requirement relative to the permitted full-surface-storage configuration.

The authority-facing IPS configuration provides approximately 4.394 Mm³ of permitted storage capacity over approximately 36.4 ha. This geometry is retained as the permitting reference and full surface storage fallback case; it is not the selected integrated PFS cost case.

The selected PFS basis adopts an IPS capacity of approximately 0.65 Mm³, with an indicative screening footprint of approximately 5.4 ha. This capacity functions as an operational and contingency buffer and as residual tailings storage rather than as a full LOM permanent tailings repository. The 0.65 Mm³ case accommodates the current aggregate selected-case residual-

tailings range together with operating buffer, subject to confirmation through detailed annual campaign modelling.

Filtered tailings will be managed using dry-stack/filtered residue placement principles. The facility basis includes engineered containment, clean water diversion, contact water management, seepage control, monitoring, and provision for progressive closure and rehabilitation. Temporary inventory within the IPS will be influenced by paste campaign timing, filtration availability, operational outages, and any other residues formally assigned to the facility.

Closure will include final grading and landform development, drainage and stormwater controls, cover placement, and rehabilitation measures intended to provide long-term physical and geochemical stability.

Feasibility Study work should include detailed annual tailings/paste campaign simulation, confirmation of stacking and placement parameters, final storage and staging requirements, closure cover development, hydrologic design, and reconciliation of the selected PFS arrangement with permitting requirements.

18.6 Building and Site Facilities

The administration building will be located near the site access gate on the western side of the site. A gatehouse will be located at the turnoff from the HU-5401 road onto the Project site. The administration building will be a two-storey building with capacity for 20 desks, four individual offices, and a meeting room for 10 people. Next to this is a lunchroom with a 30-seat capacity as well as changing rooms, showers, and toilets with capacity for 10 people (five male and five female).

18.6.1 Assay Laboratory

An assay facility will be provided on site for mining, processing, and environmental analyses. The laboratory will be at the process plant area and will be equipped for the following analytical procedures:

- Sample preparation
- Instrumental analysis
- Wet analysis
- Fire assay
- Environmental analysis

A borehole well logging building is located near the laboratory for storage of drill samples.

18.6.2 Workshops

All workshops are located on the northern side of the process plant area terrace with direct access from the northwestern corner of the terrace, ensuring separation of heavy vehicles and delivery vehicles from process plant personnel.

The workshops will include (from west to east) a heavy vehicle workshop, light vehicle workshop, auxiliary workshop, and mechanical workshop and electrical/instrumentation workshop.

18.7 Workforce Accommodation

The two neighbouring towns of Paymogo and Puebla de Guzman represent potential sources of labour, accommodation, and general services. The population of Andalusia is highly educated, with access to Andalusian universities or other universities in Spain. The University of Huelva has active geology and engineering departments.

A designated area has been allocated for the construction of the temporary construction camp (50 m x 100 m). The construction contractor will design the camp layout, however there is sufficient space around to allow for flexibility in the design.

18.8 Fuel and Utilities

18.8.1 Fuel supply and storage

Diesel will be supplied by a fuel supplier and delivered to site by road tanker. The mine will establish the appropriate delivery frequency and supply arrangements aligned with the requirements of its location and operating demand. The fuel storage, tanks, containment, transfer areas, piping, and associated equipment will be designed in accordance with the Spanish/European rules and regulations.

The storage facility will include:

- Above-ground diesel tanks;
- Secondary containment using an impermeable bund; and
- A dedicated tanker unloading area with an impermeable surface, controlled drainage and spill containment.

18.8.2 Explosives magazines

The mine will establish an authorised explosives consumption depot supplied by a licenced explosives supplier.

The proposed arrangement will comprise:

- Dedicated storage for blasting explosives and separate storage for detonators and other initiating devices, subject to approved compatibility requirements.
- Restricted access for authorised personnel.
- An approved security system and communication arrangements.
- Designated arrangements for transferring explosives from the depot to working areas.

18.8.3 Communications Systems

A site-wide fibre-optic backbone will connect the process plant control room, mine operations office, underground infrastructure, administration buildings, laboratory, workshops, security and principal utility installations.

The proposed services will include the following:

- The mine will have two-way radio, emergency communications, mine monitoring data, and personnel tracking where adopted.

- Surface mining facilities will have radio, dispatch communications, and workshop data services.
- The process plant will use PLC/SCADA communications, operator interfaces, data history, and maintenance access.
- Water and tailings infrastructure will have telemetry for pumps, tanks, pipelines, monitoring stations, and remote facilities.
- Electrical infrastructure will have substation monitoring, power system data, and communications for protection where required.
- The administration and security will have IT, telephony, internet, CCTV, and access control.
- There will also be emergency communications with backup-power.

18.8.4 Sewage Treatment

Domestic sewage from all occupied mine, process plant, and infrastructure facilities will be collected and treated through a site-wide sanitation system using a central packaged sewage treatment plant supplemented by local arrangements for isolated facilities. The system will remain separate from process effluent, mine drainage, oily water, and stormwater.

The proposed collection system will serve toilets, washrooms, showers, kitchens, and accommodation where provided. Gravity sewers will be used where practical, with sewage pumping stations where elevations or distances require them.

A packaged biological treatment plant will be installed, with capacity to accommodate construction, commissioning, and steady-state operations.

It is proposed that the effluent is disposed of as an authorised environmental discharge, or treatment to a standard suitable for reuse. The reuse would be for process water or other non-potable applications.

18.8.5 Waste Management Facilities

The mine will provide segregated waste collection points at all operating facilities and a central waste management compound for temporary storage before collection by authorised waste contractors. The central compound will be located near the workshop and service area, with suitable vehicle access, with separation from sensitive drainage features. It would provide dedicated areas for recyclable materials, general waste, and hazardous waste.

The proposed hazardous waste storage facility will comprise a roofed, secure area with an impermeable floor, containment for liquid spills, and separate storage zones for incompatible materials. Clean stormwater will be excluded, and contaminated liquids will be collected rather than discharged into the general drainage system.

Waste will be segregated at source and transferred to the central compound using suitable containers and handling equipment. The operating philosophy will prioritise prevention, reuse, and recovery before disposal,

All wastes will be transferred off site, using appropriate transport contractors, to authorised destinations for disposal.

19.0 Market Studies and Contracts

Emerita commissioned Cuadri y de la Corte and Claight to carry out independent market studies and report on the base metal and Claight to address sulphur concentrates expected to be produced at the IBW Project. The studies reviewed market fundamentals, concentrate commercial terms, treatment charges, refining charges, potential European customers, logistics, regulatory requirements, and concentrate marketability. Some key findings from the reports, Cuadri y de la Corte (2025) and Claight (2026), are summarised in this section of the Technical Report.

19.1 Zinc Market Studies and Contracts

19.1.1 Zinc Market Overview, Global Demand, and Long-Term Outlook

Zinc is the fourth most widely consumed base metal globally and is primarily used as a corrosion protection material for steel products. Approximately 75% of global zinc consumption is used in galvanised steel applications, with the remainder used in die-casting alloys, brass production, chemicals, batteries, and other industrial applications. As a result, zinc demand is closely linked to activity in the construction, infrastructure, manufacturing, and transportation sectors.

Global zinc mine production is sourced from a diverse range of jurisdictions, with China, Peru, Australia, India, and the United States among the leading producing countries. While mine production is globally distributed, zinc smelting capacity is concentrated in Asia, particularly in China, which accounts for over 50% of global refined zinc production.

The independent market study prepared by Cuadri y de la Corte (2025) indicates that the zinc concentrate market has recently experienced periods of supply tightness due to mine closures, declining production, and limited concentrate availability. These conditions contributed to historically low treatment charges during 2024 and 2025 and highlight the importance of new concentrate supply entering the market.

Global zinc demand is expected to continue growing at a moderate rate. Global refined zinc demand increased by 1.9% in 2025, and industry forecasts referenced in the independent market study indicate that consumption growth could rise to 2.6% in 2026, although the International Lead and Zinc Study Group forecasts a more conservative 1.3% growth in global refined zinc demand and 1.4% growth in refined zinc production. This forecast growth is supported by continued growth in manufacturing activity, infrastructure investment, and urbanisation. While demand growth in Europe is expected to remain relatively moderate, emerging economies, particularly in Asia, are expected to remain the primary geographic drivers of long-term zinc consumption.

The long-term outlook for zinc remains positive due to its critical role in galvanised steel and infrastructure development, and the steel sector is expected to remain the dominant end-use market for zinc over the foreseeable future.

19.1.2 Zinc Concentrate Marketability

Zinc is a freely traded commodity with transparent global pricing and well-established international markets. Cuadri y de la Corte (2025) confirmed that zinc concentrate expected to be produced from the IBW Project is marketable through established European smelting and trading networks, although it will incur penalties for various deleterious elements. Zinc prices used by SLR in the PFS financial model are outlined in Table 19-1.

Table 19-1: SLR Zinc Pricing for PFS Financial Model

Price Scenario	Price (US$/t)
Reserve Price	2,975
Resource Price	3,415
Base Case Long Term Prices	2,980
September Average Spot Price	4,020

The zinc concentrate from the Project contains approximately 50% zinc, together with payable gold and silver credits. The study considers the concentrate to be of normal-to-high-quality commercial zinc grade and notes that the recoverable precious metals enhance its attractiveness to smelters. Penalties are highly likely to apply for elevated levels of mercury and other deleterious elements, depending on final concentrate specifications.

19.1.3 Potential Offtake Agreements

Cuadri y de la Corte (2025) identified a number of potential off-takers within the European Union. The largest zinc concentrate processing groups in Europe are Boliden, Glencore, Nyrstar (part of Trafigura), ZGH Boleslaw, and KCM Plovdiv. These operations collectively represent substantial zinc concentrate processing capacity and provide multiple potential marketing avenues for zinc concentrate from the Project. The study identifies Boliden as a particularly relevant potential customer due to its dependence on externally sourced concentrates to supplement feed requirements at its smelting operations.

19.1.4 Commercial Terms

The study reviewed prevailing industry norms for zinc concentrate sales and concluded that sales would likely occur under standard concentrate purchase agreements.

Potential penalties are likely to apply for mercury, arsenic, antimony, lead, copper, iron, cadmium, fluorine, and chlorine depending on concentrate composition and smelter requirements.

19.1.5 Marketing Strategy

The market study recommends targeting buyers who recognise value in contained silver and gold, maintaining relationships with multiple smelters and traders, conducting ongoing metallurgical optimisation to reduce impurity-related deductions, and leveraging the Project's proximity to European smelting capacity.

The study further notes that concentrate traders such as Glencore and Trafigura may provide an alternative sales channel where concentrate quality or impurity levels limit direct placement with smelters.

19.1.6 Contracts

At the effective date of this report, no zinc concentrate offtake agreements, agency agreements, sales contracts, hedging arrangements or forward sales contracts have been executed for the Project.

The independent market study identified multiple potential purchasers and concluded that no material barriers to the marketing of the zinc concentrate have been identified. Zinc concentrate

sales are expected to be negotiated under industry-standard concentrate purchase agreements at the time of production.

19.2 Lead Concentrate

19.2.1 Lead Industry Overview, Global Demand and Long-Term Outlook

Lead is a major global industrial metal with a diverse range of applications; however, demand is dominated by lead-acid battery production, which accounts for most global lead consumption. Additional uses include backup power systems, renewable energy storage, radiation shielding, construction materials, electronics, and various industrial applications. As a result, lead demand is closely correlated with automotive production, energy storage markets, and industrial activity.

Global leaders in production include China, Australia, Peru, Mexico, and the United States, with China accounting for more than 40% of global output. A significant proportion of refined lead production is sourced from recycled materials, with secondary production accounting for more than 60% of global refined lead supply.

The lead market is expected to experience steady growth, supported by continued demand for lead-acid batteries in automotive, industrial, and energy storage applications. The independent market study notes that battery demand remains the dominant driver of lead consumption and is expected to continue supporting the market over the long term. While increasing recycling rates are expected to remain an important source of supply, demand growth is forecast to continue, particularly in developing economies.

The long-term outlook for lead remains stable, supported by its established role in battery technologies and industrial applications. Although growth is expected to be modest, ongoing demand from transportation, backup power systems, and energy storage infrastructure is expected to support continued consumption of lead concentrates and refined lead products over the foreseeable future.

19.2.2 Lead Concentrate Marketability

Lead is a freely traded commodity with transparent global pricing and well-established international markets. The independent market study undertaken by Cuadri y de la Corte (2025) concluded that lead concentrate produced from the IBW Project should be saleable through established European lead smelters and concentrate traders, although commercial terms will depend on concentrate quality and impurity levels. Lead prices used by SLR in the PFS financial model are outlined in Table 19-2.

Table 19-2: SLR Lead Pricing for PFS Financial Model

Price Scenario	Price (US$/t)
Reserve Price	2,200
Resource Price	2,425
Base Case Long Term Prices	2,050
September Average Spot Price	1,871

The projected lead concentrate from IBW contains approximately 27% lead, along with significant silver and gold. The study notes that precious metal credits substantially enhance the attractiveness of the concentrate and help offset penalties associated with mercury content. Despite impurities, the concentrate is considered commercially attractive due to its precious

metal content, and the market study concludes that the concentrate should be acceptable to the market under normal commercial arrangements.

19.2.3 Potential Offtake Agreements

The market study identifies several established European lead concentrate consumers and processors. Major participants include Nyrstar, Glencore, KCM Plovdiv, and ZGH Boleslaw. In addition, concentrate trading companies such as Trafigura and Glencore may provide alternative marketing routes for concentrates that require blending or specialised placement.

19.2.4 Commercial Terms

The study identifies arsenic, antimony, and mercury as the principal deleterious elements likely to impact commercial terms for the sale of lead concentrate produced at the Project. These impurities are likely to result in penalties depending on the requirements and technical capabilities of individual smelters. The study concludes that these factors do not represent material barriers to concentrate saleability.

A key positive attribute of the Project lead concentrates is the contained precious metals. Precious metal credits are expected to contribute significantly to concentrate value and improve overall marketability. The study notes that precious metal content is an important factor in the commercial attractiveness of the lead concentrate, particularly for processed ore from La Romanera and La Infanta.

19.2.5 Marketing Strategy

The independent market study recommends targeting lead smelters and traders that place a premium on silver-bearing concentrates and can process concentrates with elevated impurity levels. Diversification of customers, pre-shipment quality control, and concentrate blending are identified as tools to optimise commercial terms and minimise penalties.

19.2.6 Contracts

At the effective date of this report, no lead concentrate offtake agreements, agency agreements, hedging arrangements or forward sales contracts have been executed for the IBW Project. The project is expected to market the lead concentrate through conventional concentrate sales agreements with smelters and/or traders.

19.3 Copper Concentrate

19.3.1 Copper Market Overview, Global Demand, and Long-term Outlook

Copper is one of the world's most important industrial metals and is widely regarded as a key catalyst for economic development, electrification, and the global energy transition. Primary end user applications include electricity transmission and distribution, renewable energy infrastructure, electric vehicles, electronics, telecommunications, industrial machinery, and construction. As a result, copper demand is closely linked to growth in industrial production, urbanisation, and investment in energy infrastructure.

Global copper mine production is concentrated in a number of major producing regions, with Chile, Peru, the Democratic Republic of Congo, China, and the United States among the leading producers. Smelting and refining capacity is heavily concentrated in China, which accounts for more than 50% of global copper smelter production and approximately 45% of global refined copper production.

Cuadri y de la Corte (2025) highlights that copper concentrate markets have experienced increasing supply tightness in recent years, driven by strong growth in global smelting capacity and constraints on concentrate availability. These market conditions have resulted in declining treatment and refining charges and demonstrate the ongoing requirement for new sources of copper concentrate supply.

Global copper demand is expected to remain robust, underpinned by continued growth in renewable energy generation; electric vehicles, power transmission infrastructure, digitalisation, and data centre development. Cuadri y de la Corte (2025) forecasts global refined copper consumption growth of approximately 2.4% in 2025 (against an actual 3% increase) and 1.8% in 2026, generally in line with industry consensus. Asia is expected to remain the principal driver of demand growth.

The long-term outlook for copper remains robust. Copper is widely recognised as a critical material for the global energy transition, with demand growth expected from renewable power systems, energy storage, electric vehicles and grid expansion. Consequently, ongoing urbanisation, industrial development and electrification are expected to support sustained demand for copper concentrates and refined copper products over the long term.

19.3.2 Copper Concentrate Marketability

Copper is a freely traded commodity with transparent global pricing and well-established international markets. The independent market study concluded that copper concentrate produced from the IBW Project should be marketable through established smelting and trading networks, although concentrate quality and impurity levels will influence commercial terms and customer selection. Copper prices used by SLR in the PFS financial model are outlined in Table 19-3.

Table 19-3: SLR Copper Pricing for PFS Financial Model

Price Scenario	Price (US$/t)
Reserve Price	12,120
Resource Price	13,775
Base Case Long Term Prices	11,470
September Average Spot Price	14,483

The projected copper concentrate from the Project contains approximately 20% copper, together with significant gold and silver credits. The concentrate contains elevated levels of antimony, mercury, and arsenic, which may restrict the number of suitable smelters and could result in substantial commercial penalties, particularly for antimony content. Despite the presence of these deleterious elements, the concentrate remains attractive due to its high precious metal content, particularly gold and silver. The study concludes that the concentrate's profitability and market attractiveness are largely driven by its precious metal content, and that the concentrate should be commercially saleable, subject to appropriate offtake agreements.

19.3.3 Potential Offtake Agreements

The independent market study identified several potential European copper concentrate consumers. The principal potential off-takers include Aurubis, Atlantic Copper, and Boliden. Atlantic Copper's smelter in Huelva, Spain, provides a strategically attractive off-taker due to its geographic proximity to the Project.

The study also identifies concentrate traders such as Glencore and Trafigura as potential marketing partners, particularly for concentrates requiring specialist placement or blending solutions.

19.3.4 Commercial Terms

The market study identifies several deleterious elements that may influence commercial terms depending on concentrate composition and offtake agreements. Deleterious elements include mercury, antimony, arsenic, bismuth, cadmium, and fluorine.

For the Project concentrate, antimony and mercury represent the primary commercial challenges; however, the study concludes that these issues can be managed through customer selection, blending strategies, and targeting smelters with suitable metallurgical capabilities.

A key positive attribute of the copper concentrate is the significant gold and silver content. The study repeatedly highlights precious metal credits as a major value driver and key contributor to concentrate value and overall marketability.

19.3.5 Marketing Strategy

The independent market study recommends focusing on buyers capable of maximising value from gold- and silver-rich concentrates and highlights the importance of maintaining multiple marketing channels. The study specifically recommends targeting smelters with precious metal recovery capabilities and continuing to investigate opportunities to reduce impurities, particularly in a concentrate with such high levels of antimony.

The study specifically notes that traders can play an important role in placing concentrates containing elevated deleterious elements by providing blending, logistics, and access to alternative customers.

19.3.6 Contracts

At the effective date of this report, no copper concentrate offtake agreements, agency agreements, hedging arrangements, or forward sales contracts have been executed for the IBW Project. The independent market study identified numerous potential customers within the European smelting sector and concluded that there are no material barriers to the sale of the anticipated copper concentrates, provided that concentrate specifications and impurity levels are appropriately managed. Copper concentrate sales are expected to occur under industry-standard concentrate purchase agreements negotiated at the time of production.

19.4 Pyrite Concentrate

19.4.1 Pyrite Concentrate/Sulphur Industry Overview, Global Demand, and Long-Term Outlook

Pyrite concentrate is primarily marketed as a source of sulphur and is predominantly used in the manufacture of sulphuric acid. Sulphuric acid is one of the world's highest volume industrial chemicals and is a critical reagent in fertiliser production, metal processing, chemical manufacturing, and battery material supply chains. As a result, demand for pyrite concentrate is closely linked to global sulphuric acid consumption.

According to the independent market study prepared by Claight (2026), global pyrite concentrate demand is estimated at approximately 19.7 Mt in 2026, with more than 80% of demand attributable to sulphuric acid production. China dominates both production and

consumption of pyrite concentrate and accounts for approximately 90% of global pyrite-based sulphuric acid production.

Demand for sulphuric acid is expected to increase over the long term, owing to the growing consumption in lithium processing, nickel high-pressure acid leaching operations, battery materials production, and battery recycling.

Claight (2026) notes that recent disruptions in global sulphur supply, combined with tight copper concentrate markets and strong sulphuric acid prices, have increased interest in pyrite as an alternative sulphur-bearing material. In addition to its sulphur value, pyrite concentrates containing recoverable precious metals may attract further value through gold and silver credits.

The long-term outlook for pyrite concentrate is considered positive, supported by anticipated growth in sulphuric acid demand and increasing requirements associated with the energy transition. The market study concludes that pyrite concentrate represents an established, globally traded product with multiple potential end markets and a favourable demand outlook.

19.4.2 Pyrite Concentrate Marketability

Pyrite concentrate is primarily marketed for its sulphur content and is sold through negotiated commercial agreements rather than a transparent, exchange-traded pricing mechanism. Despite market opacity, Claight (2026) concludes that the pyrite concentrate market is established and growing, with multiple potential customer groups. Unlike conventional base metal concentrates, the pyrite concentrate value is derived primarily from sulphur content, together with any recoverable gold and silver that may be present in the concentrate. Claight (2026) identifies three principal drivers of pyrite concentrate value, and SLR used the prices outlined in Table 19-4 in the PFS financial model, exclusive of precious metal credits.

Table 19-4: SLR Sulphur Concentrate Pricing for PFS Financial Model

Price Scenario	Price (US$/t)
Consensus Price	274
Oversupply (Conservative) Price	217
Extended ME Conflict Price	348
Reserve Price	215

Claight (2026) notes that current market conditions are supportive for pyrite concentrates due to strong sulphuric acid demand, elevated sulphur prices and high precious metal prices.

19.4.3 Potential Offtake Agreements

Two primary customer groups for pyrite concentrate were identified in Claight (2026): non-ferrous smelters and sulphuric acid producers. Non-ferrous smelters can recover gold and silver while also producing sulphuric acid from the contained sulphur. The study identifies several potential customers in Europe, including Aurubis, Boliden, Atlantic Copper, Glencore, and Nyrstar. The study notes that smelters generally place the greatest value on concentrates containing payable precious metals and can process concentrates with higher impurity levels than sulphuric acid producers.

Sulphuric acid producers generally prefer clean pyrite concentrates with low impurity levels and limited precious metal content.

19.4.4 Commercial Terms

Unlike base metal concentrates, pyrite concentrate is not traded on the basis of a globally recognised benchmark price. Claight (2026) notes that commercial terms are negotiated directly between buyers and sellers and are typically based on sulphur content, recoverable gold and silver content, smelter processing capabilities, impurity levels, and sulphuric acid market conditions.

The study identifies arsenic, mercury, and antimony as the principal deleterious elements that may influence commercial terms. The magnitude of any penalties depends on individual buyer capabilities and contractual arrangements.

19.4.5 Marketing Strategy

Claight (2026) concludes that a combination of European and Chinese customers represents the preferred long-term marketing strategy.

The study notes that, whilst Chinese buyers currently provide the strongest pricing support, European smelters generally provide greater contract stability and long-term offtake opportunities; a diversified offtake portfolio reduces marketing risk and can optimise the recovery of payable precious metals whilst also minimising impurity penalties.

The study concludes that pyrite concentrates containing precious metals are most likely to achieve maximum value through non-ferrous smelters rather than dedicated sulphuric acid producers.

19.4.6 Contracts

At the effective date of this report, no pyrite concentrate offtake agreements, agency agreements, hedging arrangements or forward sales contracts have been executed for the IBW Project.

The Claight (2026) market study identified multiple potential buyers in both the European and Asian markets and concluded that there are no material barriers to market entry for a pyrite concentrate product meeting typical industry specifications. Sales are expected to occur under industry-standard negotiated concentrate purchase agreements.

19.5 Commodity Prices Selected for the Economic Analysis

The economic analysis for the PFS considered a range of commodity price scenarios, including Reserves, Consensus and Resources price decks. The Consensus scenario was selected as the PFS Base Case, with long-term price assumptions of US$11,470/t copper, US$2,050/t lead, US$2,980/t zinc, US$3,750/oz gold and US$52/oz silver. Pyrite concentrate is valued at US$274/t under the Base Case.

The metal price assumptions are based on consensus broker forecasts. These forecasts typically contain a more detailed near-term outlook before converging towards, and flattening at, long-term price assumptions after approximately the first five years. In the Project's case, this initial forecast period broadly overlaps with the development and construction period. Consequently, by the time the operation reaches first ore and enters production, the price deck has substantially converged to the long-term assumptions. The PFS Base Case therefore effectively reflects long-term consensus commodity prices over the operating period, rather than relying on elevated or volatile near-term forecasts.

The pyrite concentrate price assumption is treated separately from the exchange-traded metal price assumptions. It is based on the Project-specific, tailored pyrite market study discussed earlier in this report, which considered the expected characteristics and marketability of the Project's pyrite concentrate. The resulting Base Case assumption is US$274/t of pyrite concentrate.

Table 19-5 below shows the commodity price assumptions under each of the scenarios considered.

Table 19-5: Commodity Price Assumptions for the Economic Analysis

Long term Metal Prices	Consensus (Base Case Long-Term)
Pyrite Concentrate (US$/t)	274
Copper Price (US$/t)	11,470
Lead Price (US$/t)	2,050
Zinc Price (US$/t)	2,980
Gold Price (US$/oz)	3,750
Silver Price (US$/oz)	52

19.6 Conclusion

Based on the findings of the independent market studies conducted by Cuadri y de la Corte (2025) and Claight (2026), SLR considers the base metal concentrates expected to be produced from the IBW Project marketable through established smelting and trading networks. Although certain concentrates contain elevated levels of deleterious elements that may attract penalties or, particularly in relation to the copper concentrate, restrict the number of potential customers, the significant gold and silver credits, the availability of multiple European smelters and traders, and the Project's location within the European market position Emerita’s products as favourable within the market.

SLR considers the pyrite concentrate expected to be produced from the IBW Project to be marketable through established sulphuric acid and non-ferrous smelting markets. Demand growth for sulphuric acid and the presence of recoverable precious metals provide support for a positive long-term outlook.

The assumptions applied in the independent market reports are considered reasonable and consistent with current market conditions.

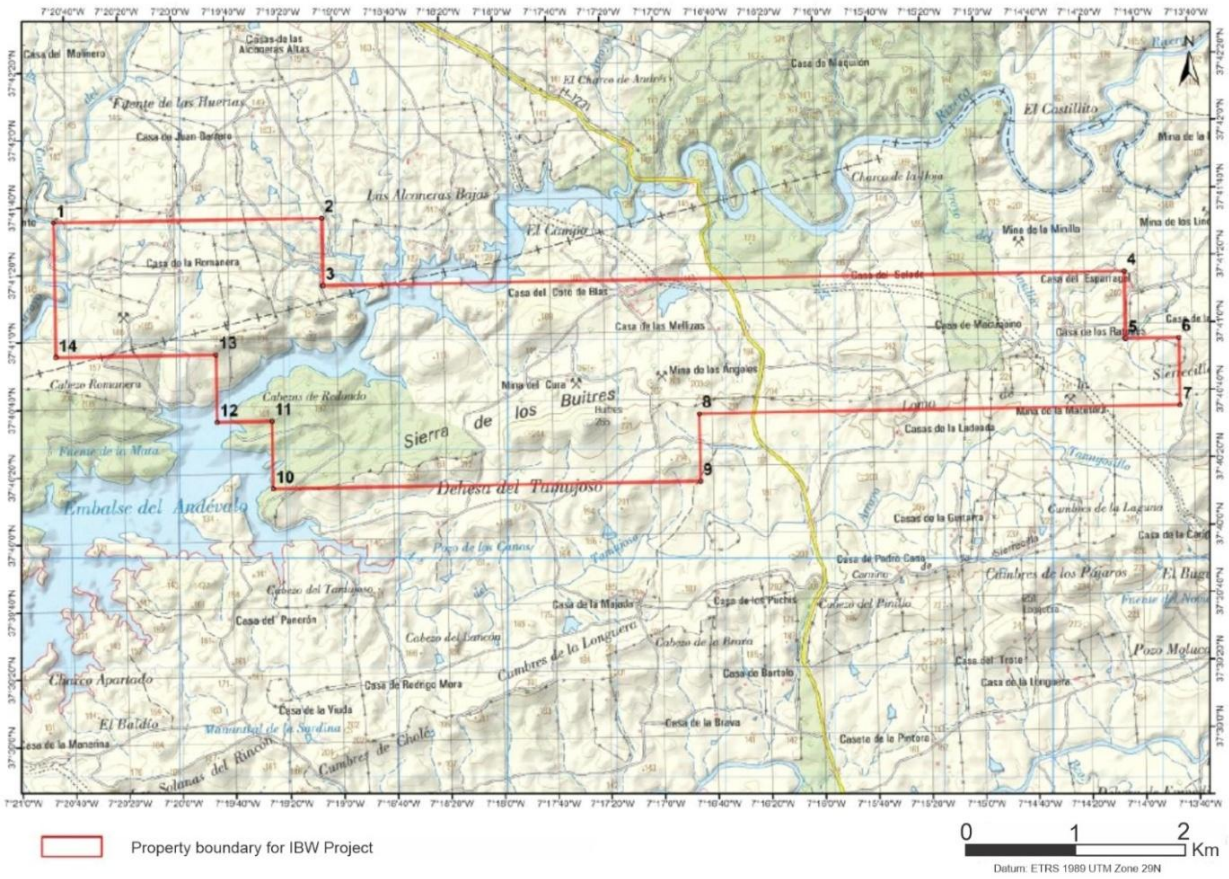
20.0 Environmental, Permitting and Social Impact

20.1 Project Status

20.1.1 Introduction and Project Background

The IBW Project is located in the southwestern Huelva Province of the autonomous community of Andalusia, Spain, approximately 9 km east of the Portuguese border (Figure 4-2). The exploration permit area covers an area of 1,545.6 ha at the eastern edge of the Andévalo Reservoir (Figure 20-1).

Figure 20-1: IBW Project Exploration Permit Boundary



Geologically, the IBW Project is situated within the IPB, which is a geological province renowned for its high-grade Zn, Pb, Cu, Ag, and Au mineral deposits. Mining in the district is reported to date back to pre-Roman times, with visible remnants of ancient shafts, pits, and dumps still present at the three principal deposits of La Romanera, La Infanta, and El Cura.

Emerita commenced initial drilling on the Project in mid-2021 at La Infanta, the easternmost deposit, expanding to La Romanera to the west in mid-2022, and then drilling at El Cura commencing in early-2024 (Table 10-1 and Figure 10-1).

20.1.2 Permitting and Legislation

20.1.2.1 Environmental Permitting

Mining projects in Spain are regulated through a combination of national mining legislation, environmental permitting frameworks, and sector-specific regulations governing waste, water, land use, cultural heritage, and other disciplines. The permitting process for the Project is ongoing, with a number of permits currently being undertaken, submitted, pending approval, or granted.

The Project's permit register is summarised in Appendix 20-1.

Unified Environmental Authorisation (AAU)

In December 2023, Emerita submitted an application of the AAU, an integrated environmental permit covering the Project's 2023 MRE mining exploitation scenario. The AAU, required in environmentally protected areas, was registered with the Junta de Andalusia (the Junta) in July 2024, initiating the permitting process.

A public consultation process for the AAU took place between May and July 2026, allowing stakeholders to provide feedback on the Project. Comments provided were submitted to the Junta for review and resolution of stakeholder feedback, with an environmental ruling expected at the end of 2026. A positive ruling signifies that the Regional Office of Industry, Energy, and Mines in Huelva is satisfied with the AAU submission, which then initiates final administrative hearings and resolution of comments and concerns, expected to be completed in Q1 2027.

The final AAU documentation will be evaluated by the Regional Office of Industry, Energy, and Mines and Regional Office for Sustainability and the Environment in Huelva, followed by approval by the Junta in Seville due to the Project's Declaration of Strategic Interest (DSI) status in Andalusia. This approval process is estimated to be finalised in Q2 2027. Upon completion of the final resolution, the Exploitation Permit will be authorised and issued by DT Minas (Huelva) and DG Minas (Sevilla).

In preparation of the AAU, numerous baseline studies were undertaken, detailed in Section 20.1.3.

20.1.2.2 Relevant Legislation

National Standards

The national standards outlined in Table 20-1 collectively define the minimum binding environmental and social baseline for the IBW Project, particularly in relation to environmental impact assessment, mining waste and rehabilitation, water management, worker safety, and cultural heritage protection.

Table 20-1: Applicable National E&S Requirements

Standard	Purpose and E&S Requirements
Spanish Mining Law 22/1973	Establishes the legal requirements for exploration and exploitation of mineral resources, including obligations to protect the environment and rehabilitate affected areas.
General Regulations for the Mining Regime (RGRM – Royal Decree 2857/1978)	Develops the Mining Law, detailing permitting procedures, technical obligations, safety, and environmental conditions for mining operations.
Royal Decree 975/2009 on Waste from Extractive Industries and Rehabilitation of Areas Affected by Mining Activities (as amended by RD 777/2012)	Transposes Directive 2006/21/EC; regulates mining waste management (tailings and waste facilities), requires a Restoration Plan and a Mining Waste Management Plan, public consultation, and financial guarantees to ensure rehabilitation post-closure.
Law 21/2013 on Environmental Impact Assessment (EIA)	Establishes the EIA regime for projects, including screening, scoping, impact assessment, public participation, and environmental conditions in the final decision. Provides the basis for the AAU.
Spanish Water Law (Recast Text – RDL 1/2001) and Basin Regulations (Confederación Hidrográfica del Guadiana)	Regulates water use, abstraction, discharge, and protection of surface and groundwater bodies, including permitting and quantitative/qualitative status objectives.
National Waste and Soil Protection Legislation (e.g. Law 7/2022 on Waste and Contaminated Soils for a Circular Economy)	Sets general principles for waste prevention, management hierarchy, and contaminated soil management, complementing sector specific mining waste rules. Applies to non-mining wastes and potential soil contamination associated with all project infrastructure.
Occupational Health and Safety Framework (Law 31/1995 and implementing regulations)	Establishes obligations for employers regarding worker health and safety, risk assessment, training, preventive measures, and occupational risk management.
Cultural Heritage and Archaeology Legislation (State and Andalusian)	Regulates the protection of archaeology and cultural heritage, including pre-exploration and mining surveys, intervention permits, and chance find procedures. Directly linked to the Archaeological Intervention Project and AAU permits.

The IBW Project is also aligned with the objectives of the EU *Critical Raw Materials Act* (CRMA 2023), aiming to strengthen European supply chain resilience.

International Standards

A number of international standards may apply depending on the needs of the Project according to Good International Industry Practice (GIIP). The international standards most relevant to the Project are summarised in Table 20-2.

Table 20-2: GIIP International Standards

Standard	Purpose and E&S Requirements
Equator Principles IV (EPs)[1]	Risk management framework adopted by financial institutions to assess and manage a Project's E&S risks. The EPs are constituted of ten principles: • Principle 1 – Review and Categorisation; • Principle 2 – Environmental and Social Assessment; • Principle 3 – Applicable Environmental and Social Standards; • Principle 4 – Environmental and Social Management System and Equator Principles Action Plan; • Principle 5 – Stakeholder Engagement; • Principle 6 – Grievance Mechanism; • Principle 7 – Independent Review; • Principle 8 – Covenants; • Principle 9 – Independent Monitoring and Reporting; and • Principle 10 – Reporting and Transparency.
International Finance Corporation Performance Standards (IFC PS)[2]	Outlines commitments and responsibilities related to environmental, social, H&S and community aspects for integrated management of risks and impacts. The IFC PS are composed of eight standards: • PS 1 – Assessment and Management of Environmental and Social Risks and Impacts; • PS 2 – Labour and Working Conditions; • PS 3 – Resource Efficiency and Pollution Prevention; • PS 4 – Community Health, Safety, and Security; • PS 5 – Land Acquisition and Involuntary Resettlement; • PS 6 – Biodiversity Conservation and Sustainable Management of Living Natural Resources; • PS 7 – Indigenous Peoples; and • PS 8 – Cultural Heritage.

[1] Equator Principles (2020) equator-principles.com

[2] International Finance Corporation (2012) ifc.org/en/insights-reports/2012/ifc-performance-standards

Standard	Purpose and E&S Requirements
European Bank for Reconstruction and Development Performance Requirements (EBRD PR)[3]	Promotes environmental and social sustainability through definition of responsibilities for assessment and monitoring of E&S risks. The EBRD PR are constituted of ten requirements: • PR 1 – Assessment and Management of Environmental and Social Risks and Impacts; • PR 2 – Labour and Working Conditions; • PR 3 – Resource Efficiency and Pollution Prevention and Control; • PR 4 – Health, Safety and Security; • PR 5 – Land Acquisition, Restrictions on Land Use and Involuntary Resettlement; • PR 6 – Biodiversity Conservation and Sustainable Management of Living Natural Resources; • PR 7 – Indigenous Peoples; • PR 8 – Cultural Heritage; • PR 9 – Financial Intermediaries; and • PR 10 – Information Disclosure and Stakeholder Engagement.
World Bank Group Environmental, Health and Safety (WBG EHS) General Guidelines[4]	Provides technical references for general and industry-specific examples of GIIP, allowing for establishment of project-specific targets. Where host country regulations differ from those within the WBG EHS guidelines, the more stringent guidance should be adopted.

Additional good practice guidelines include:

- European Union directives;
- The Copper Mark;
- The Global Industry Standard on Tailings Management (GISTM);
- Extractive Industries Transparency Initiative (EITI); and
- International Labour Organization (ILO) conventions and United Nations human rights instruments.

20.1.2.3 Current Project Status

The IBW Project comprises polymetallic zinc, copper, and lead deposits, divided into three areas: La Infanta, El Cura, and La Romanera. The Project's permit area encompasses all three deposits. Emerita holds 100% ownership for the IBW Project, having received the mineral rights and public tender on September 1, 2020. The exploration permit was granted for a period of 26 months on July 12, 2021, with the option to renew for a further 3 years.

[3] European Bank for Reconstruction and Development (2019) ebrd.com/home/who-we-are/ebrd-values/ebrd-environmental-social-sustainability/reports-and-policies/performance-requirements

[4] World Bank Group (2007) documents.worldbank.org/en/publication/documents-reports/documentdetail/157871484635724258

On September 9, 2023, Emerita Resources España SLU applied to the Junta for an exploitation permit for the IBW Project. The exploitation permit application covers the same area as the existing IBW Project exploration permit. Granting of the exploitation permit is dependent on the award of the AAU, as discussed in Section 20.1.2.1.

The Project includes underground mining operations, accessed through an underground ramp. The life of mine (LOM) for the Project is anticipated to be 23 years, comprising a 2-year pre-production phase, 17 years of production, and a 4-year closure and restoration period.

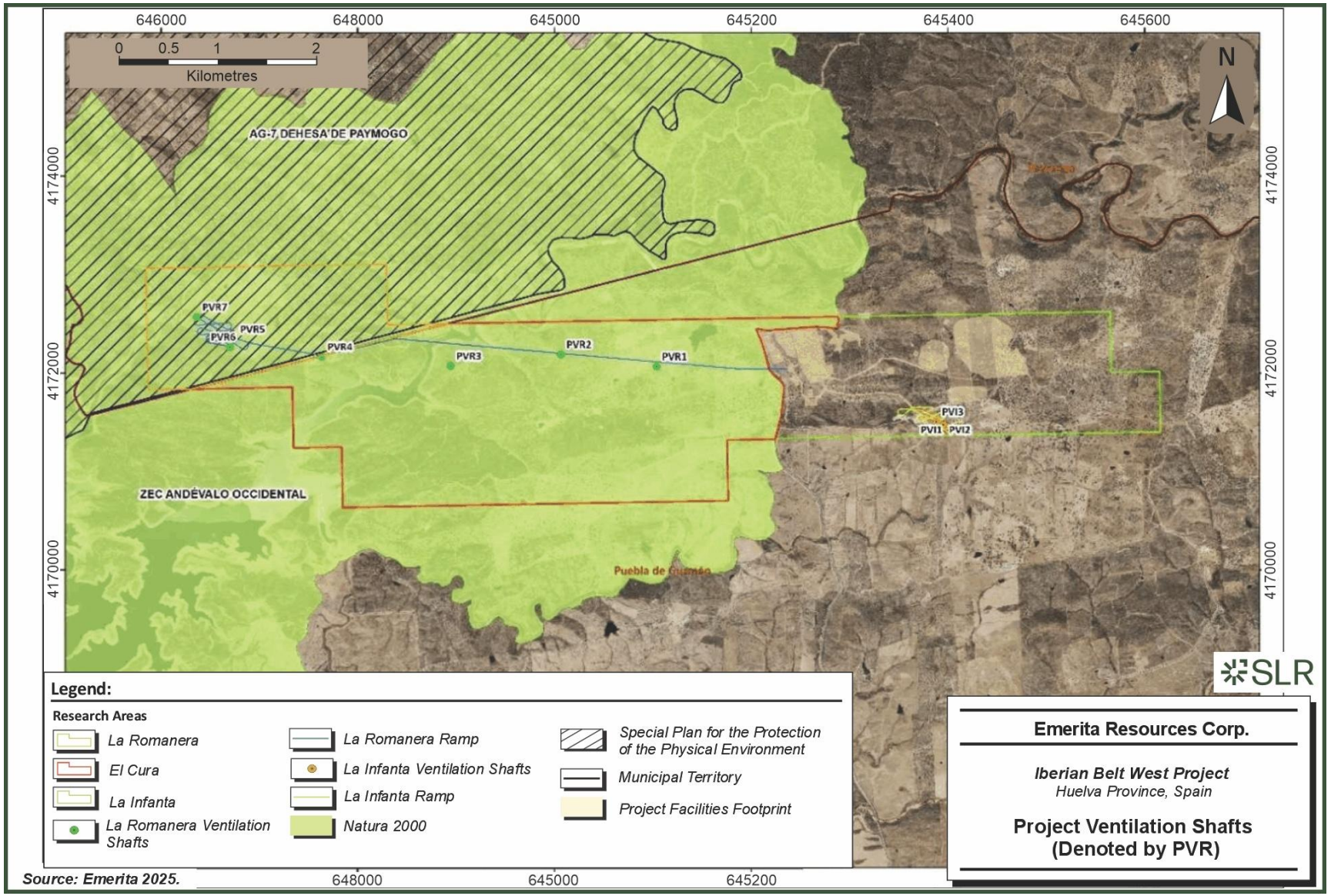
Ore will be fed into the ore processing plant for recovery via flotation, for the production of base metal concentrates (Cu, Pb, Zn) as well as a saleable pyrite concentrate. Tailings material will be stored in a surface filtered-tailings/residue facility (*Instalación de Pasta Seca*; IPS). Waste rock from mining activities and construction of the underground ramp system will be stored in a temporary waste rock stockpile prior to use for backfilling of the underground mine.

Other Project facilities include access roads, ventilation shafts, ore stockpile area, process water treatment plant, domestic wastewater treatment plant, water supply network, and other supporting facilities, occupying a total surface land area of 87.1 ha. The majority of Project facilities will be located in the La Infanta section of the permit area (Figure 4-4 and Figure 18-1) to avoid interaction with the Andévalo Occidental Special Area of Conservation (*Zona de Especial Conservación*, ZEC) to the west. Ventilation shafts for underground mining operations constitute the only surface infrastructure within the ZEC (Figure 20-2).

The current Project permit applications, including the exploitation permit and associated AAU, are based on the 2023 concept study undertaken by IPH. They may therefore require amendment or updating to reflect the current PFS mine schedule, proposed infrastructure, and revised mass balance, including the IPS and ATEM.

A number of E&S studies have already been undertaken, detailed in Section 20.1.3. The E&S studies may also require updating to align with the current PFS.

Figure 20-2: Project Ventilation Shafts (Denoted by PVR)



20.1.3 Environmental and Social Studies

A number of E&S baseline studies have been undertaken or are ongoing, to establish baseline conditions, identify potential risks, and influence the Project's engineering design (Table 20-3). These studies provide the technical foundation for the AAU and subsequent permitting stages.

Baseline data and identified risks outlined in these studies will be provided in Section 20.2, and management and social development plans in Section 20.3.

Table 20-3: E&S Studies Undertaken to Date

Specialist Study	Scope
Environmental	
Atmospheric Pollutant Dispersion Study (Meteosim; April 2024)	Determination of potential operational atmospheric impacts through characterisation of anticipated Project emissions and meteorological and dispersion modelling. Modelling considered total suspended particles (TSP), PM_{10}, $PM_{2.5}$, CO, SO_2, and NO_2, assessed in accordance with national legislation (Section 20.2.1.2). The study also defines recommendations for improvement of air quality and reduction of potential impacts.
Noise Impact Assessment (Sacener; November 2025)	Definition of baseline noise levels and assessment of noise impacts during the Project's operational phase (Section 20.2.2). Primary noise sources included underground mining and ventilation shafts, processing plant, water treatment plant, and material handling and transport.
Natural Environment and Landscape Diagnostic Study (Biogeos; June 2023)	Baseline characterisation of flora, fauna and ecosystems within the Project area, including habitats of community interest (HCIs) and protected species (Section 20.2.3). Sampling was conducted across a 10-month period between 2022 and 2023, across the permit area. Baseline landscape features were also identified, with assessment of visual receptors and vulnerability.
Natura 2000 Impact Assessment (GTA; December 2024)	Evaluation of potential interactions between the Project and Natura 2000 protected sites (Section 0). The study details habitats, flora, fauna, and sensitive ecological processes, along with potential impacts and required mitigation measures.
Hydrogeological-Hydrological Conceptual Model (GSO; July 2024)	Development of a conceptual model describing groundwater and surface water dynamics, recharge, flow patterns, and potential Project interactions with water resources (see Section 20.2.4). Project water balance, discharge, and management measures were also outlined in the study.
Surface Water Quality Reports (Laboratorios Microal; December 2022)	Analysis of baseline surface water resources sampled between August and September 2022 to establish baseline surface water quality. Parameters measured include metal concentrations, pH, and conductivity. Further details are provided in Section 20.2.4.1.
Soil Baseline Study (DSM; November 2022)	Characterisation of baseline soil quality, physical–chemical properties, and potential contamination indicators (historical mining) to support future monitoring and rehabilitation planning (Section 20.2.5).

Specialist Study	Scope
Environmental Impact Assessment (GTA; December 2024)	Analysis of potential impacts to environmental receptors from Project activities and facilities throughout construction, operation, and closure. The study includes waste management and access alternatives, as well as recommended mitigation measures and monitoring programmes.
Restoration Plans (For Derivative Mining Concession Application) (Emerita; August 2025)	Description of planned rehabilitation activities for Project facilities and Project-affected environmental aspects. These plans focus on waste rock and tailings facilities, processing plant, and water treatment ponds. The restoration plans also outline a cost estimate for rehabilitation, and a proposed implementation schedule (see Section 20.3.8).
Social	
Value proposition study (Karungen; 2025)	Preliminary stakeholder perception analysis (a value proposition study). Preliminary analysis of local perception, perceived challenges, and some socio-economic background of the study area following 15 in-depth interviews conducted between April and May 2025, followed by a management workshop in May 2025.
Internal Social Baseline and Risk Assessment – Andévalo Region (Emerita; ongoing)	Internal socio-economic baseline and risk analysis for the Andévalo region, identifying social sensitivities and potential risks, assessing compatibility of mining activities with local livelihoods, and supporting Project planning and stakeholder engagement strategies. This study is ongoing and was not available during the development of this PFS.
Archaeological Activities (Marcos Garcia; March 2023, May 2024)	Two Reports on Preventive Archaeological Intervention developed through surface surveys and test excavation of the La Romanera, El Cura and Sierrecilla permit areas.

20.2 Environmental and Social Setting and Risks

20.2.1 Climate and Air Quality

20.2.1.1 Climate

The IBW Project is located in southwestern Spain, within a Mediterranean climate regime, categorised as Csa according to the Köppen-Geiger system (hot summer Mediterranean climate). The region has a high water stress risk as well as a medium wildfire and coastal flooding risk, with 33,000 ha of land being scorched in a large wildfire in August 2026 (Ghirlanda 2026).

Temperatures in the Project area vary throughout the year, ranging in 2022 between an average of 9.1°C in January and 27.1°C in July. A minimum temperature of 0.1°C was recorded in January, with a maximum recorded temperature of 39.9°C in July. Annual rainfall averages between 500 mm and 600 mm, with minimal rainfall during the summer months (lowest measured rainfall in July) and peak rainfall between October and December, measuring 70 mm to 90 mm per month. The region experiences periods of high evapotranspiration and summer droughts, typical of inland Andalusia.

The predominant wind direction in the Project area is from the northwest in spring, summer, and autumn, and from the east in winter. Wind speeds are low, with the majority of winds staying below 5 m/s and an average of 2.5 m/s.

20.2.1.2 Air Quality

The region is predominantly rural, with limited heavy industry in the immediate vicinity of the Project. Baseline air quality is therefore expected to generally be good, with regional traffic, agricultural activities, and Saharan dust episodes assumed to be the main contributors to dust and air pollution.

Atmospheric pollutant dispersion modelling was undertaken for the operational phase of the Project as per emissions estimated for Project activities defined in April 2024 and meteorological data from 2022. Results obtained show no exceedances in air quality limit values outlined in national legislation (Royal Decree 102/2011[5]) for total suspended particles (TSP), particulate matter under 10 µm (PM_{10}), $PM_{2.5}$, carbon monoxide (CO), sulphur dioxide (SO_2), and nitrogen dioxide (NO_2) at any defined receptors within and surrounding the permit area. The nature and sensitivity of these receptors have not yet been defined.

20.2.1.3 Climate and Air Quality Risks

Potential air quality emissions arising during the Project's construction and operation periods are fugitive dust ($PM_{2.5}$ and PM_{10}) and combustion emissions. Fugitive dust may be generated through earthworks and construction activities, vehicle movements, material handling and exposed surfaces (such as stockpiles, waste rock dumps, and storage areas). Combustion emissions relate to greenhouse gas (GHG) emissions from vehicles, mobile and static plant equipment, and emissions from power generation.

Due to the early stage of the Project, dedicated baseline air quality surveys have not yet been undertaken, however, are likely to be engaged at a later date. Despite the absence of baseline air quality surveys, the following preliminary management measures have been considered and may be integrated into the Project's planning and design to avoid or reduce the impact of dust and combustion emissions on sensitive receptors:

- Paving of internal roads to limit exposed surfaces;
- Speed limits for vehicles along Project roads;
- Use of covers at transfer points and stockpiles;
- Use of water for dust suppression on roads and exposed stockpiles, especially during dry weather and periods of high winds;
- Progressive rehabilitation of disturbed land;
- Optimisation of layout to reduce haul distances and fuel consumption;
- Selection of energy efficient equipment and mobile fleet;
- Evaluation of grid connection and renewable energy options to reduce reliance on fossil fuels; and

[5] Royal Decree 102/2011, of 28 January, on the improvement of air quality (2011) boe.es/buscar/act.php?id=BOE-A-2011-1645

- Potential to develop a GHG inventory and reduction roadmap aligned with the Greenhouse Gas Protocol[6] and International Finance Corporation Performance Standards (IFC PS).

20.2.2 Noise

Noise levels are low in the Project's permit area due to the rural, agricultural nature of the land. The closest towns are Paymogo, 5.1 km north of the permit boundary, and Puebla de Guzmán, 6.8k m south of the permit boundary. The HU-5401 road connecting the two towns passes through the permit area just to the west of the proposed mine facilities, and constitutes the primary source of noise in the Project area.

Baseline noise levels (24-hour and short-term [15-minute]) were measured in January 2024 at the proposed mine facilities (Figure 20-3) and the La Romanera ventilation shaft locations (Figure 20-4). Average short-term (15 minute) daytime noise levels ranged from 38.7dBA at P-04 to 54.1dBA at P-02.

A summary of baseline noise levels collected during the 24-hour surveys is provided in Table 20-4.

Table 20-4: Baseline Noise Levels (24-hour)

Monitoring Point	Maximum (dBA)	Minimum (dBA)	Day (Average) (dBA)	Afternoon (Average) (dBA)	Night (Average) (dBA)
24h-1	45.8	28.4	41.4	35.4	30.7
24h-2	48.3	27.3	35.9	28.0	28.3

[6] Greenhouse Gas Protocol (2026) ghgprotocol.org

Figure 20-3: Noise Monitoring Locations at the Proposed Mine Facilities

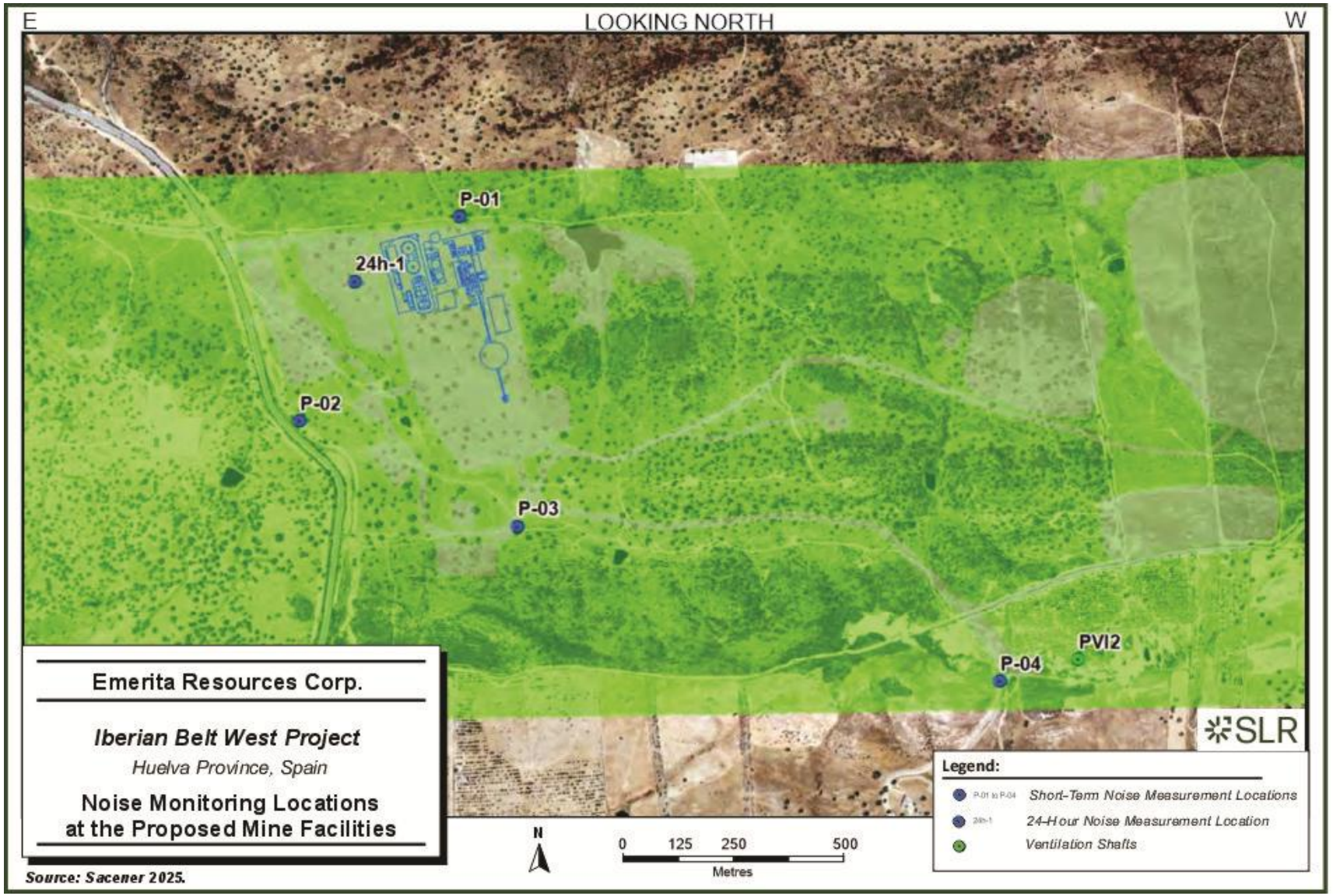
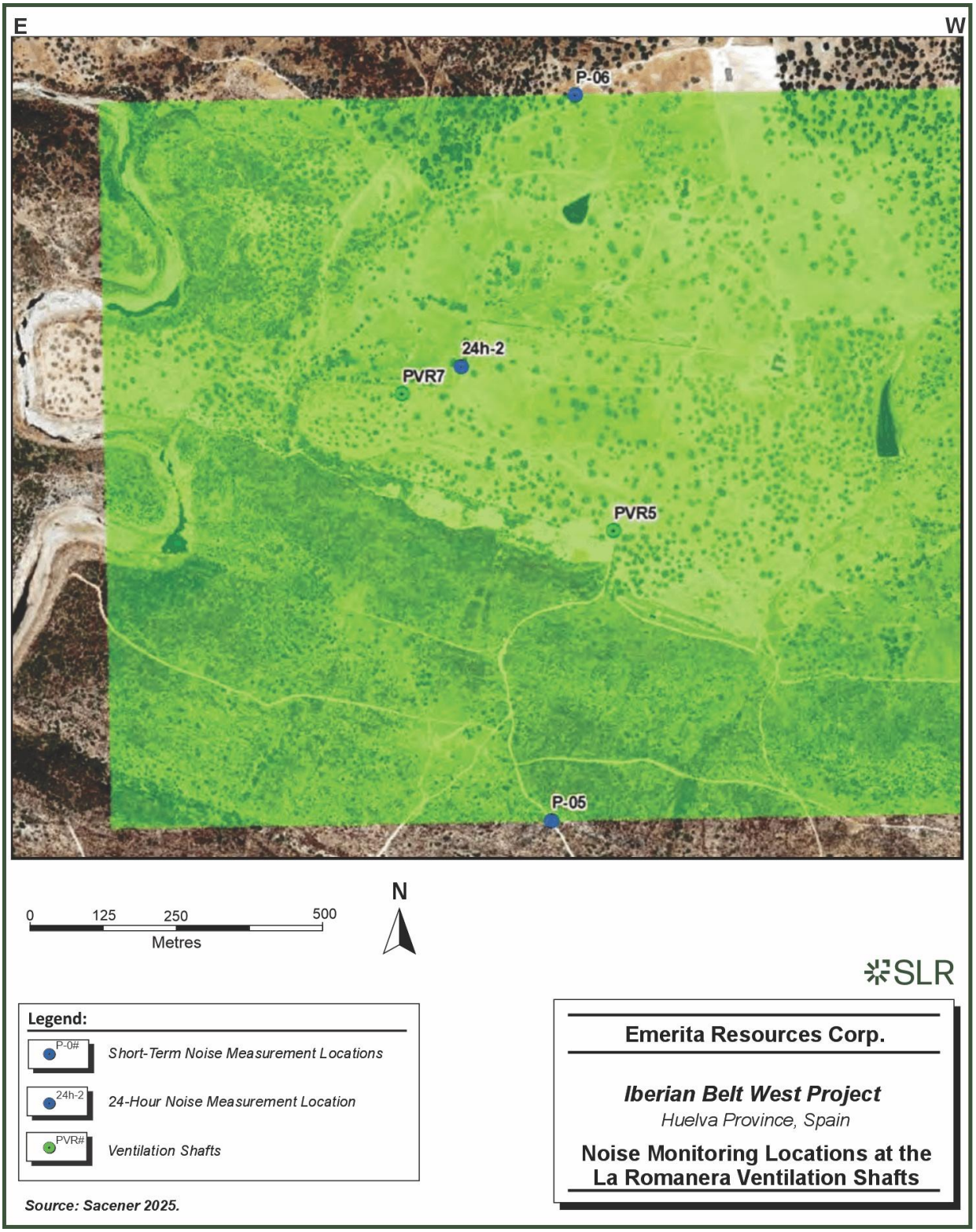


Figure 20-4: Noise Monitoring Locations at the La Romanera Ventilation Shafts



Primary Project noise sources during the construction period are anticipated to be vehicles and other mobile equipment, earthworks, and construction of Project facilities. During operation, noise from underground mining operations is expected to be minimal, with surface activities and facilities such as the processing plant, water treatment plant, material transport, and ventilation shafts constituting the main sources of noise emissions.

Noise level guidelines are provided in Royal Decree 1367/2007[7] for built-up areas, with a stipulation for reduction of these guidelines by 5 dB in rural areas. These guidelines, as well as those provided in the WBG EHS are outlined in Table 20-5. Where guideline levels differ, the most stringent level should be implemented.

Table 20-5: Noise Level Guidelines (dBA)

Receptor	Daytime (RD 1367/2007)	Evening (RD 1367/2007)	Night (RD 1367/2007)	Daytime (WBG EHS)	Night (WBG EHS)
Residential	65	65	55	55	45
Industrial	75	75	65	70	70

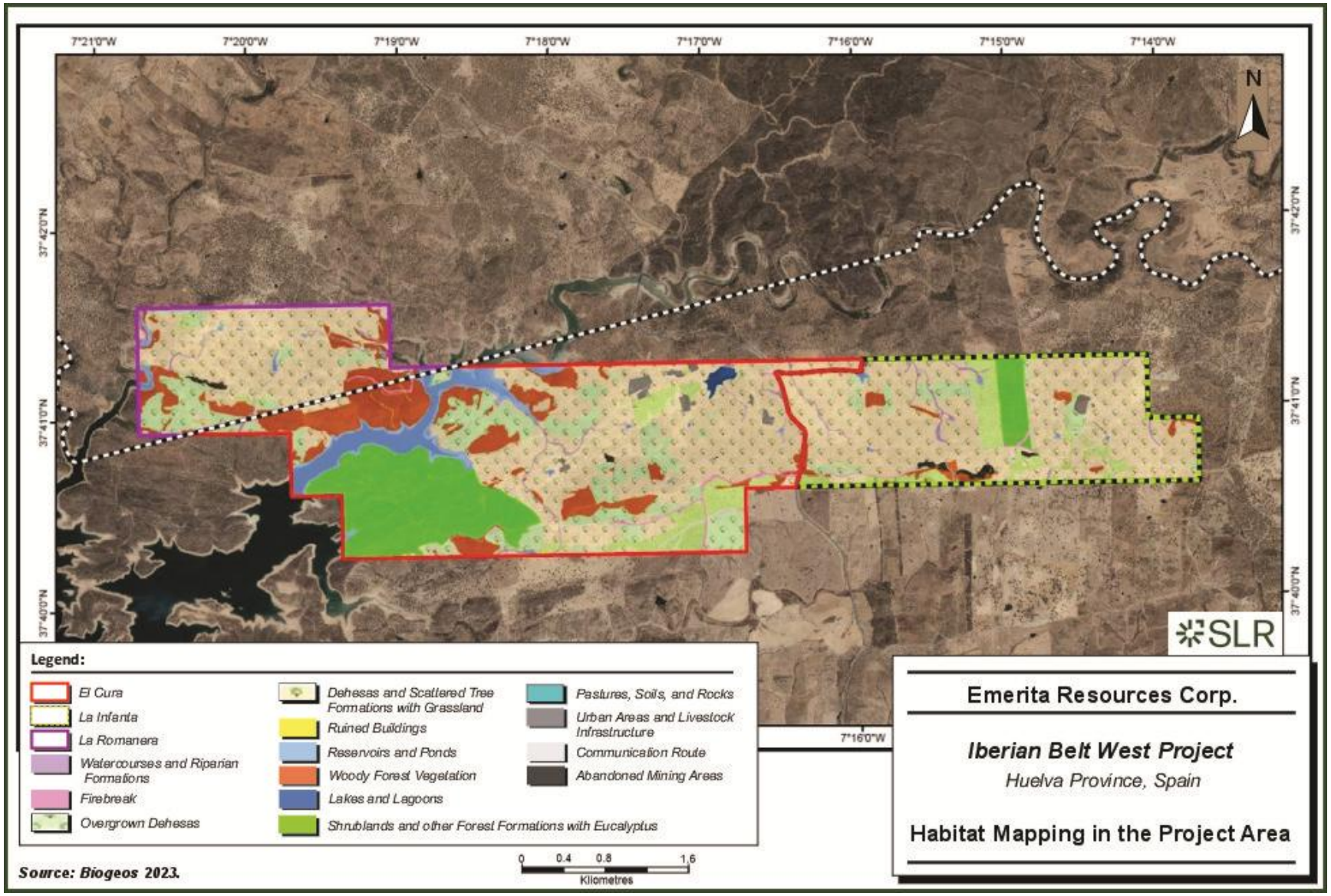
20.2.3 Biodiversity

Vegetation and land use in the Project area is divided into 13 categories based on information provided in the Andalusian Natural Heritage Information System (SIPNA). The total mapped area covers 1,539.5 ha of the Project area, differing slightly from the overall Project area (1,546.6 ha) by approximately 6 ha. This minor discrepancy results from differences in the spatial datasets and calculation methodologies used for individual Project components and does not affect the overall assessment conclusions.

The predominant vegetation and land use types within the Project area include pastures of varying cover, scattered grassland formations, wooded forests, reforested eucalyptus stands, soils, rocks, and reservoirs and ponds (Figure 20-5; Biogeos 2023). Other land types include watercourses, firebreaks and urban areas, including transport routes and abandoned mining areas.

[7] Royal Decree 1367/2007 of 19 October, implementing Law 37/2003 of 17 November on Noise, with regard to noise zoning, quality objectives and noise emissions boe.es/eli/es/rd/2007/10/19/1367/con

Figure 20-5: Habitat Mapping in the Project Area



A total of 12 Habitats of Community Interest (HCIs) have been identified and categorised according to the Andalusia Environmental Information Network as part of the Habitats Directive (Artero et al., 2020). These include lakes, rivers and riparian habitats, scrubland, grassland, pastures and meadows, woodland and forests, and rocky areas.

A total of 157 species of fauna were observed: 110 birds, 17 mammals, 12 amphibians, 9 reptiles, and 9 fish. Of these species, four are categorised as Near Threatened according to the International Union for Conservation of Nature (IUCN) Red List of Threatened Species, with one species listed as Vulnerable. Roughly three-quarters of identified fauna are classified under Royal Decree 139/2011 (implementing the List of Wild Species Subject to Special Protection and the Spanish Catalogue of Threatened Species), protecting them from hunting and game activities.

Over 300 species of flora have been identified in the Project area (6 native trees, 46 shrubs, and 280 herbaceous plants), none of which are endangered at a national level.

Direct habitat loss associated with Project infrastructure is limited in area due to the underground nature of mining operations, however, sensitive pasture habitats and associated HCIs will be disturbed by the Project's surface infrastructure and activities. New access roads and increased traffic may contribute to habitat fragmentation and disturbance of fauna.

A mitigation hierarchy has already been considered for the Project with the goal of no net loss through:

- Avoidance and minimisation of impacts – Implementation of mitigation measures within the Project design, such as locating the main surface facilities outside of the Andévalo Occidental ZEC to minimise impacts to sensitive biodiversity;
- Restoration and progressive rehabilitation – Progressive rehabilitation of disturbed areas through soil management, revegetation, and restoration of impacted habitats. These measures should be implemented as early as possible to allow for restoration of temporary access roads and construction facilities;
- Fauna-focused mitigation measures – Use of collected baseline data to establish exclusion zones around nesting / roosting sites and implementation of road and ramp crossings to reduce barrier effects; and
- Offsets / no net loss / net gain – Provision of biodiversity offsets should mitigation and management measures not be sufficient, including enhancement of degraded pastures and restoration of riparian corridors. Biodiversity offsets are measurable conservation actions outlined for unavoidable impacts, aiming to achieve no net loss and preferably net gain where prevention and mitigation measures are proven insufficient (IUCN 2021). Biodiversity offsets are a last resort, at the bottom of the mitigation hierarchy, therefore priority should be given to avoidance of impacts (mitigation hierarchy: avoid, minimise / reduce, restore / rehabilitate, compensate / offset).

20.2.3.1 Protected Areas

The Project area was identified to overlap one protected area during the Natura 2000 Impact Assessment – the Andévalo Occidental ZEC (GTA 2024). This 52,981 ha site is protected under the Habitats Directive due to the presence of 16 protected habitats and 46 protected species, including 33 birds, 5 fish, 4 mammals, 2 reptiles, one amphibian species, and one plant species.

The Project's permit area overlaps approximately 11 km^2 of the ZEC, including the La Romanera and El Cura deposits, and area of cultural interest and forestry (*Dehesa de Paymogo)* within the La Romanera deposit (Figure 4-4).

To limit impacts to the ZEC and *Dehesa de Paymogo* associated with traffic, noise, dust, habitat loss and fragmentation, disruption of roosting and foraging areas, etc. from mining operations, mitigation measures have been embedded into the Project design. These measures include locating the majority of surface infrastructure such as the processing plant, water treatment plant, and waste storage areas outside of the ZEC, within the La Infanta area. The only surface infrastructure planned in the ZEC are ventilation shafts and their associated platforms for underground mining operations, which have been optimised to avoid the most sensitive areas of biodiversity. The La Romanera and El Cura areas will be connected via an underground ramp to avoid land clearance within the ZEC for access roads and movement of haul trucks.

Further mitigations applied to the Project to reduce impacts to the ZEC include:

- Hydrological protection measures for watercourses crossing the protected area;
- No further construction of access roads to the ventilation shaft sites, as a network of tracks is already present on site. Off-road movement of Project traffic should also be prohibited to avoid widening of tracks and further encroachment into sensitive biodiversity areas;
- Removal of both topsoil and vegetation during earthworks to ensure collection of propagules for use during restoration and revegetation;
- Restoration of land surrounding the ventilation shafts once construction is complete, including decompaction, replacement of 30 cm thick topsoil, and revegetation. This will result in approximately 1,800 m^2 of land being restored within a short period of time; and
- Dismantling, decommissioning and sealing of ventilation shafts upon cessation of use, removal of concrete platforms, and restoration of land through decompaction, replacement and enhancement of the 30 cm thick topsoil layer, and revegetation.

Water collected from dewatering of the mine and wastewater associated with the wastewater treatment plant are proposed to be discharged into watercourses within the ZEC, however the characteristics of discharged water are not known at this stage. Guidelines outlined in the EU Environmental Quality Standards (Directive 2008/105/EC; EU 2008) and WHO Guidelines for Drinking-Water Quality (WHO 2022) should be applied to discharges into watercourses, with the aim of preserving water quality and maintaining their ecological status.

Any significant residual impacts, or impacts that have not been sufficiently mitigated, may result in delays to, or additional conditions within, the AAU, affecting the Project's permitting status. Visible or perceived damage to the ZEC may also result in a negative public opinion. A Habitats Regulation Assessment is therefore recommended to accurately determine potential impacts and appropriate management, compensation, or offset measures based on the ZEC's unique designation.

20.2.4 Hydrology and Hydrogeology

20.2.4.1 Surface Water

The Project area lies within the Guadiana catchment, in the upper catchment of the Malagón River and Andévalo Reservoir, with additional drainage to the Arroyo del Ansillar and several unnamed ephemeral streams. The Malagón River begins in the Sierra Pelada to the northeast of the permit area, flowing over a distance of 53 km.

The Project area is traversed by a 2.5 km stretch of the Malagón River, 1.5 km of the Ansillar Stream, the Los Ratones and Tamujoso streams, and several other unnamed streams that flow into larger watercourses outside of the Project's permit area (Figure 20-6; GSO 2024). These watercourses flow into the Andévalo Reservoir, immediately southwest of the Project area, which subsequently flows into the Guadiana River.

With the exception of the Malagón River and the Tamujosillo and Albahacar streams, surface watercourses in the Project area are ephemeral, with water flow only during storm events. Small dams have also been built on streams in the Project area for storage of water for livestock.

One official surface water monitoring station is located close to the Project area on the Malagón River, sitting 0.9 km north of where the HU-5401 road intersects the permit boundary. Flow rates measured at this station are highly variable, ranging from 0 m^3/s to 800 m^3/s, with an average flow rate of 1.6 m^3/s between 1969 and 2008.

Surface water quality sampling was undertaken across the permitting area during the summer months (August and September 2022) for measurement of metals content, conductivity, pH, and other in situ parameters. Results from this survey shows water quality characteristic of a mineralised region, such as the IPB, with the highest copper, zinc, and arsenic concentrations measured downstream of a Roman slag heap in the La Romanera area (9.8 mg/L, 162 mg/L, and 3.3 mg/L, respectively). Water within the La Romanera area also measured the highest in situ conductivity (1,682 µS/cm), indicating a high concentration of dissolved ions.

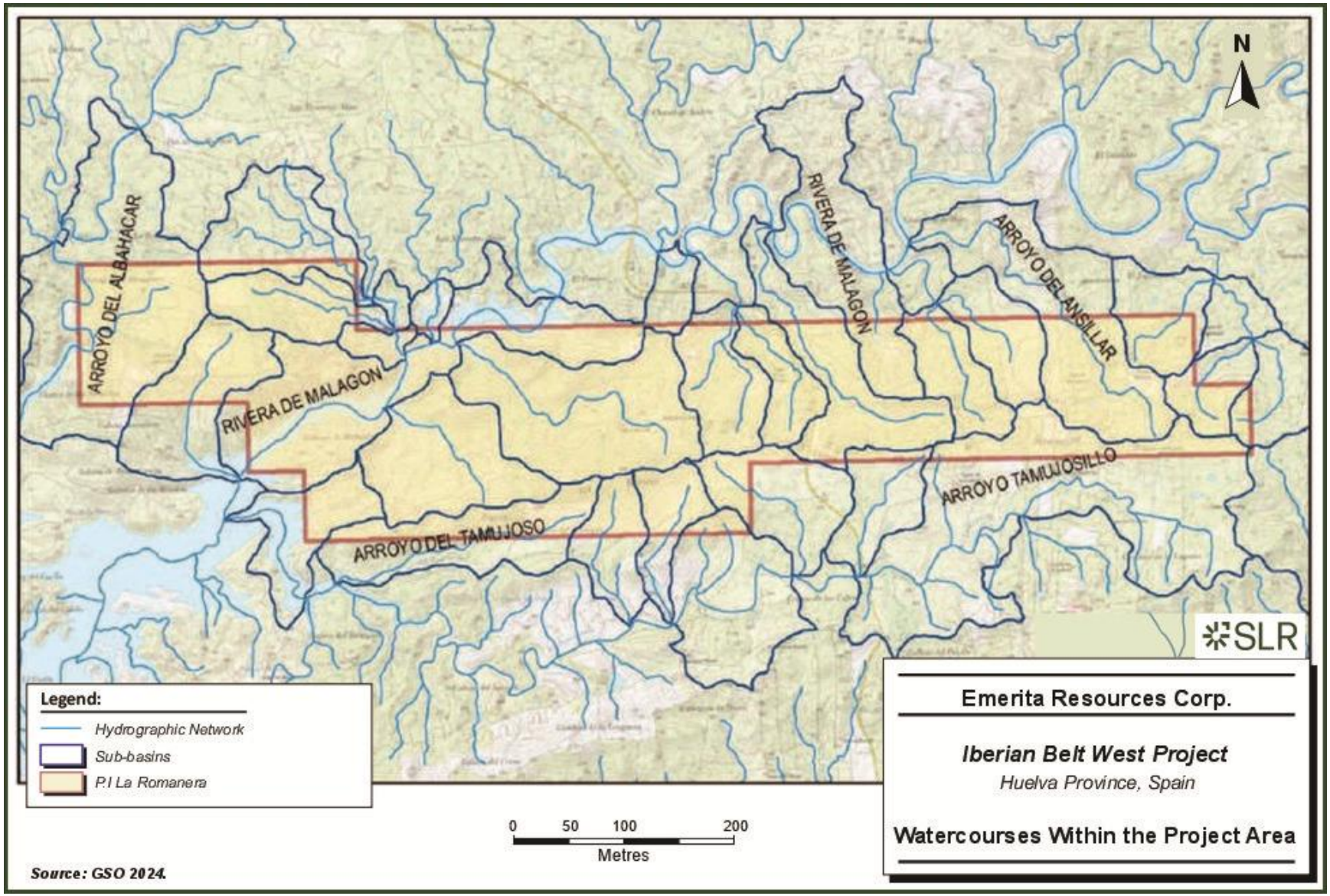
These baseline water quality results show exceedances in guidelines provided in Royal Decree 817/2015[8], indicating historical surface water contamination and acid rock drainage (ARD).

Despite the presence of historical contamination, mitigation measures should be implemented for the Project to avoid further degradation of surface water quality. As stated in Section 0, dewatered mine water and wastewater from the wastewater treatment plant are planned to be discharged into nearby watercourses. As the Project is upstream of the Andévalo Reservoir, an important water resource, any discharged water should be treated, and relevant guidelines (such as WHO drinking water guidelines; WHO 2022) should be followed.

Seasonal variability has not yet been defined due to sampling being limited to the dry summer months. This variability, along with flow parameters in surface watercourses, should be analysed prior to construction.

[8] Royal Decree 817/2015, of 11 September, which establishes the criteria for monitoring and evaluating the state of surface waters and environmental quality standards (2015) boe.es/buscar/act.php?id=BOE-A-2015-9806

Figure 20-6: Watercourses Within the Project Area



20.2.4.2 Groundwater

No regionally significant groundwater resources have been identified within the Project permitting area. Groundwater encountered to date is associated primarily with private water supply wells and deep mineral exploration boreholes and is interpreted to occur within a series of free-flowing (artesian), confined, and semi-confined fractured aquifer systems.

The preliminary conceptual hydrogeological model comprises four heterogeneous hydrostratigraphic units, as summarised below:

- The uppermost unit extends from the ground surface to approximately 50 m depth. This unit comprises weathered and stress-relief fractured competent bedrock, locally hydraulically connected to colluvial deposits, alluvial deposits, and surface water bodies (including the Andévalo Reservoir). The unit is strongly influenced by seasonal rainfall, resulting in relatively rapid recharge and groundwater level responses. A limited number of low-yield private wells extract water from this unit. The estimated hydraulic conductivity is 10^{-7} m/s to 10^{-9} m/s.
- An intermediate hydrostratigraphic unit extends from approximately 50 m depth to the lower extent of the mineralised sequence. Groundwater flow is interpreted to occur primarily through the principal fracture network, with limited hydraulic connectivity outside these structures. The estimated hydraulic conductivity is 10^{-8} m/s to 10^{-9} m/s.
- The mining hydrostratigraphic unit is confined to a semi-confined fractured groundwater system associated with the massive sulphide deposits. Groundwater flow is controlled predominantly by fractures and structural discontinuities, with local groundwater pressures potentially reflecting long-residence formation water. This unit is consistent with hydrogeological conditions observed elsewhere within the IPB, where groundwater flow is dominated by structurally controlled fracture permeability.
- An impermeable basement unit at depths greater than 150 m.

The conceptual hydrogeological model is considered preliminary and will be refined as additional geological, hydrogeological, groundwater monitoring, and hydraulic testing data become available. No data has been collected regarding groundwater quality at this stage of the Project, however a sampling survey should be conducted prior to construction to establish baseline conditions. Groundwater quality analysis should encompass heavy metals content, pH, total dissolved solids (TDS), and total suspended solids (TSS) as a minimum due to the presence of the ZEC and Andévalo Reservoir, to ensure compliance with EU standards such as the Water Framework Directive and Groundwater Directive (EU 2000).

20.2.5 Soils and Contaminated Land

Soils in the Project area are generally poor quality for agricultural purposes, with shallow, stony profiles, coarse textures, and low pHs. Where oak forests dominate, soils are of higher quality, with finer textures and greater soil depths.

Analysis of the upper 0.45 m soil resource shows a background geochemical signature consistent with the mineralisation of the IPB (elevated sulphur and metal contents). Soils within the vicinity of historical mine waste, however, show interaction with acid rock drainage (ARD) and metal-rich leachates, with significant concentrations of metals and other chemicals including the following:

- Maximum measured arsenic concentration of 920 mg/kg in La Infanta;

- Maximum copper concentration of 11,000 mg/kg in La Infanta;
- Maximum lead concentration of 28,000 mg/kg in La Infanta; and
- Maximum zinc concentration of 11,000 mg/kg in La Infanta.

These concentrations are higher than industrial guidelines applicable to contaminated soils outlined in Decree 18/2015 of Andalusia[9], and significantly higher than those relating to human health and the environment set by the Canadian Council of Ministers of the Environment (CCME 2025). The spatial footprint of this contamination is generally limited to zones close to historical mine waste, however, development of management plans for disturbance of land throughout the Project is important at an early stage to avoid the spread of contaminated soils and pollution of surface and groundwater. Where feasible, the Project may incorporate partial remediation (e.g., encapsulation within engineered facilities) as part of mine development. Further geochemical test work and risk assessment will be developed in subsequent Project phases to refine the understanding of contaminant mobility, potential exposure pathways, and appropriate management and rehabilitation strategies.

Soil properties within the Project area also make them vulnerable to erosion, contamination, and loss of the soil resource, particularly along access roads and in operational areas. These risks are expected to be managed through standard good practice measures, including:

- Topsoil stripping and stockpiling for later rehabilitation;
- Erosion and sediment control (drainage, diversion channels, sediment traps, progressive stabilisation);
- Careful siting and lining of waste and process facilities; and
- Implementation of spill prevention and response procedures.

Detailed management plans will be developed as the Project progresses, and will be included within an Environmental and Social Management Plan (ESMP) as part of the Environmental and Social Impact Assessment (ESIA).

20.2.6 Socio-economics

The Project is located in the Andévalo region of Huelva (Spain), encompassing the municipality of Paymogo and surrounding rural areas. Two social studies have been commissioned to date, the Karungen study (2025), focused on stakeholder perception analysis, and an internal Social Baseline and Risk Assessment – Andévalo Region (ongoing study).

20.2.6.1 Communities

The communities closest to the Project area include Paymogo, Las Herrerias, Puebla de Guzmán, Santa Bárbara de Casa, and Tharsis. Their populations and locations are presented in Table 20-6. The Project's permit area encompasses 788.6 ha of agricultural land, with planned Project infrastructure overlapping 87.1 ha.

[9] Decree 18/2015, of 27 January, approving the regulations governing the regime applicable to contaminated soils (2015) juntadeandalucia.es/boja/2015/38/3

Table 20-6: Communities Located Proximally to the Project

Settlement	Population (2025; INE 2025)	Distance from Permit Boundary (km)	Direction
Paymogo	1,132	5	NW
Las Herrerias	289[10]	8	S
Puebla de Guzmán	3,071	7	S
Santa Bárbara de Casa	1,144	14	NE
Tharsis	1,840	16	SE

20.2.6.2 Community Characteristics

Several stakeholders in the Karungen study described the Project surroundings as an impoverished area with an aging population. These communities are characterised by low population density, a predominantly rural socio-economic structure, and livelihoods largely dependent on agriculture, livestock grazing, small local businesses, and land-based economic activities. The region maintains an active institutional framework, with local authorities engaged in community development and land-use management.

From the limited data collected to date, key vulnerable groups identified are the Roma population in Paymogo, with high levels of structural unemployment, informal economy, and school absenteeism, as well as elderly people.

The capacity of local resource infrastructure for health, education, housing, etc., is not yet understood. Future studies should include an assessment of infrastructure capacity to absorb worker and population influx and population growth. Lack of understanding of this capacity and lack of mitigation can lead to housing price inflation, pressure on local services, and reduced well-being for local communities.

20.2.6.3 Land Tenure and Access

Emerita holds a 100% interest in the IBW Project. The mineral rights and exploration permit were acquired by its subsidiary, Emerita Resources España SLU., through a public tender. Exploration permit No. 15.029 was granted on July 12, 2021, for an initial period of 26 months, with the option to renew for a further 3 years.

On September 9, 2023, Emerita Resources España SLU. applied to the Delegación *Territorial de Energía y Minas* in Huelva Province, Junta de Andalucía, for an exploitation permit for the IBW Project. The permit comprises 51 mining claims covering 1,545.6 ha and extends approximately 18 km in an east-west direction. Exploitation permits in Spain, when granted, have an initial 30-year term and may be extended for two subsequent 30-year periods.

In accordance with Article 88.1 of the General Regulations for the Mining Regime (Royal Decree 2857/1978), the rights attached to the exploration permit are extended while the exploitation permit application is being processed. This allows ongoing exploration at the La Romanera, La Infanta, and El Cura deposits. The Restoration Plan, which is required for the exploitation permit

[10] Las Herrerías is a village in the municipality of Puebla de Guzmán, Huelva. Population from 2024 taken from the Self-Protection Plan, Emerita 2025

application, was approved on July 12, 2021, and its validity is extended while the exploitation permit application is under review. See Section 4.3 for more information on land tenure.

Mineral rights and surface land rights are separate under Spanish mining legislation. Emerita has access agreements with local landowners covering the main exploration area, allowing surface exploration and prospecting in exchange for nominal monetary compensation. If a conflict arises between the surface rights owner and the mineral rights holder, Spanish mining legislation provides for temporary surface occupation, allowing access to carry out authorised exploration works.

To maintain the exploration concession in good standing, Emerita must pay an annual concession fee (€1,319, based on the Project's 51 claims) and fulfil the exploration investment requirements.

For the proposed mining operations, especially the construction of surface infrastructure, an assessment of land tenure, ownership, and current land use within the areas required for the Project should be undertaken to identify potential constraints, land access requirements, and stakeholder considerations. Depending on the assessment, land access requirements for construction and operations might require land acquisition and/or land lease.

20.2.6.4 Land Use

Land use in the area is predominantly agricultural. Within the site boundary, immediately north of the proposed Project footprint, is Finca El Coto, a farm comprising multiple agricultural buildings and livestock enclosures. Several smaller farm properties are also located to the east of the site boundary.

To expand the assessment of land tenure constraints, potential impacts on livelihoods and physical structures within the Project footprint should be evaluated to minimise the risk of physical and economic displacement. This analysis needs to assess the extent of disruption to assets, land use, and traditional livelihoods, particularly agriculture and grazing activities located within or adjacent to the permit area. This disruption may be due to land acquisition for above-ground infrastructure, ground subsidence, changes to groundwater levels and quality, physical restrictions during construction, and deposition of dust on fields.

20.2.6.5 Transport

Road HU-5401 connects the Paymogo and Puebla de Guzmán communities and passes through the Project footprint. To minimise risk of disruption for local communities, the use and traffic on this connecting road needs to be well understood.

20.2.6.6 Stakeholder Engagement and Expectations

Stakeholder Engagement Undertaken to Date

Initial stakeholder engagement activities and preliminary stakeholder mapping were undertaken in 2025, when Emerita commissioned a preliminary stakeholder perception analysis for the IBW Project (Karungen 2025). A total of 15 in-depth interviews and a subsequent management workshop were conducted between April and May 2025.

The breakdown of stakeholders interviewed is summarised in Table 20-7.

Table 20-7: Interviewed Stakeholders as part of the Karungen Study

Variable	Categories	Number of Interviewees per Category	Percentage (%)
Gender	Men	12	80.0
	Women	3	20.0
Type of stakeholder	Internal	7	46.7
	External	8	53.3
Stakeholder category	EMERITA employee	7	46.7
	Political expert	1	6.7
	Academic expert	1	6.7
	Public Sector (mayors of Puebla de Guzmán and Paymogo)	2	13.3
	Contractor	2	13.3
	Civil society	1	6.7
	Business association of Huelva	1	6.7

Stakeholder Engagement Findings

Key findings show that the Project has good local social acceptance, rooted in the area's mining identity and the hope of jobs and demographic recovery. This support is not yet matched by a clear public narrative, settled water balance, and landowner strategy. Additional stakeholder outreach is highly recommended.

Key stakeholder concerns include:

- Fear of water contamination, consumption, proximity to the Andévalo dam, and an unfinished Project-wide water balance;
- Slow, multi-level, political permitting process seen as a bottleneck for investors. Risk that permits become a political weapon after the Aznalcóllar judgment[11];
- Nearby ZEC, fear of waste and residual contaminants. Persisting mining stigma from past liabilities;
- Limited public knowledge of the Project and doubt that the mine will actually open. Some neighbours already work for Emerita, building credibility; and
- Abandoned promises should the Project become financially unviable.

Findings indicate a high level of expectations due to the lack of alternative development opportunities and employment in the area. While these expectations contribute to greater social acceptance of the Project, if not properly managed, they may result in community frustration if anticipated benefits are not realised. Managing this risk will require clear and transparent communication regarding the actual benefits that the Project can provide, including employment

[11] The Aznalcóllar trial concerned alleged corruption and procedural irregularities in the award of the Aznalcóllar mine concession in Andalusia, Spain, following a long-running legal dispute over the 2015 tender process.

opportunities and funding, while avoiding overpromising and prioritising local communities in the distribution of Project benefits.

Stakeholders also associate historical mining activities with ARD and degraded watercourses, therefore may be predisposed to view any new mining development through the lens of past environmental impacts. If Emerita is not clearly perceived as both differentiating its operations from historical mining practices and actively contributing to improved environmental management or remediation, even minor incidents may be interpreted as reinforcing existing negative perceptions, potentially undermining trust and stakeholder confidence.

Preliminary Stakeholder Mapping for Future Engagements

The preliminary stakeholder perception analysis for the IBW Project (Karungen 2025) identified the key stakeholders for any future engagement, including:

- Regional and national media;
- Political and administrative authorities (local, provincial, regional and national);
- Business and sector associations;
- Private companies and suppliers, including other mining companies operating in the region;
- Local and community civil society including religious and heritage associations; and
- Academia and technical experts.

Engagement to date heavily relied on internal stakeholders and community leaders. For a more nuanced perspective and a better understanding of worries and challenges, more stakeholders should be engaged, including:

- Landowners and farmers;
- Women; and
- Local community members, including elderly, unemployed, youth, people with disabilities, ethnic minorities (i.e., the local Roma population), etc.

20.2.7 Health, Safety, and Human Rights

20.2.7.1 Community Health and Safety

Communities within the Project's area of influence have access to Spain's national public healthcare system, which provides universal coverage. Local healthcare infrastructure consists primarily of small primary care centres with limited capacity, typical of rural municipalities in the Andévalo region. More advanced medical services are available in larger urban centres such as Valverde del Camino (68 km by road) and Huelva (75 km by road). Most common causes of death in the Huelva region in 2025 were circulatory system conditions and malignant tumours, with tracheal, bronchial, and lung cancer the most common (Cano Heredia, M., 2026).

To better understand potential impacts on human health, future studies should include an assessment of health infrastructure, determinants of health (e.g., lifestyle; the environment; safety risks, such as prevalence of crime, substance abuse, and gender-based violence; food systems; housing quality; and availability), and most common diseases including any communicable diseases such as tuberculosis and sexually transmitted infections in the local communities. This is required to understand the general health of the population and the

expected impacts from environmental pollution and worker influx (in terms of communicable diseases, gender-based violence, and potential increase in anti-social behaviour). Moreover, traffic and road safety risks associated with increased heavy-vehicle circulation on rural roads needs to be better understood.

20.2.7.2 Human Rights

Spain maintains a strong legal and institutional framework for the protection of human rights, although several challenges persist in relation to housing, gender-based violence, poverty and social exclusion (Table 20-8).

Table 20-8: Human Rights Challenges

Human Right	Context in Spain
Housing	19,347 evictions recorded between January and September 2025, more than 90% linked to economic reasons. The government extended measures suspending evictions for individuals with extreme economic vulnerability until the end of the year (Amnesty International 2025).
Gender-based and sexual violence	Nationally significant issue. Despite national funding for 52 crisis centres, only 10 were operational by mid-year 2025, prompting a year-end deadline for all autonomous communities to open planned facilities (Amnesty International 2025).
Poverty and social exclusion	In 2023, 26.5% of the population was at risk of poverty or social exclusion, while 9% experienced severe material or social deprivation, both increased compared with the previous year. Single-parent households, third-country nationals, and unemployed individuals, as well as southern regions of Spain and the Canary Islands were disproportionately affected (Human Rights Watch 2024).
Labour rights	Occupational health and safety (OHS) standards considered appropriate for Spain's principal industries. Spanish legislation protects workers who remove themselves from situations that could endanger their H&S. Most frequent workplace H&S violations in the services sector, followed by the food, wood, iron, steel and construction industries (U.S. Department of State 2024a).
Human trafficking	Strong performance in combating human trafficking through increased convictions of traffickers and greater provision of assistance to victims (U.S. Department of State 2024b).

Considering the above, the following human rights risks are relevant to the Project:

- Access to land and natural resources, particularly for agricultural and grazing activities.
- Labour and working conditions, including OHS and contractor management.
- Supply chain risks, particularly regarding subcontractors operating in rural areas.
- Disproportionate impacts on vulnerable groups, especially the Roma population, including risks of exclusion, poverty, or unequal access to benefits.
- Gender-based violence triggered by worker influx.

These assumptions are based mostly on a national context, understanding of local human rights context is crucial to better understand human rights risks in the Project area. Key stakeholder interviews with human rights NGOs and interviews with relevant local stakeholders will be key in understanding local risks.

20.2.8 Cultural Heritage

Within and around the Project area there is a dense archaeological inventory, including:

- Charco de las Herrerías (BIC[12]), a prehistoric/Chalcolithic fortified settlement.
- La Romanera (Romanera I), with "indications of mining and metallurgical operations: shafts, slag heaps, drainage trench, furnace wall fragments," dated to Roman High Empire and contemporary times.
- La Romanera III, a medieval settlement.
- Minas Grupo Malagón, a Roman mining site.
- Cerro del Castillito (BIC), a defended settlement with slate masonry walls and occupation from the 3rd millennium BCE to the 1st–3rd centuries CE.

These archaeological areas are presented in Figure 20-7.

Emerita has commissioned and completed preventive archaeological prospections in the La Romanera and El Cura areas and in Sierrecilla–La Infanta. A review of survey results against the General Catalogue of Andalusian Historical Heritage (CPGHA) and other information confirmed that cultural heritage resources may be affected in the La Romanera permit area. Archaeological protection measures are therefore required as per the Regulations on Archaeological Activities approved by Decree 168/2003 of June 17, 2003, including archaeological monitoring of all earthworks associated with the construction of ventilation shafts PVR-5, PVR-6, and PVR-7, due to their proximity to the Roman archaeological site La Romanera. The boundaries of the archaeological site must be clearly demarcated and protected throughout the construction period to prevent any impacts.

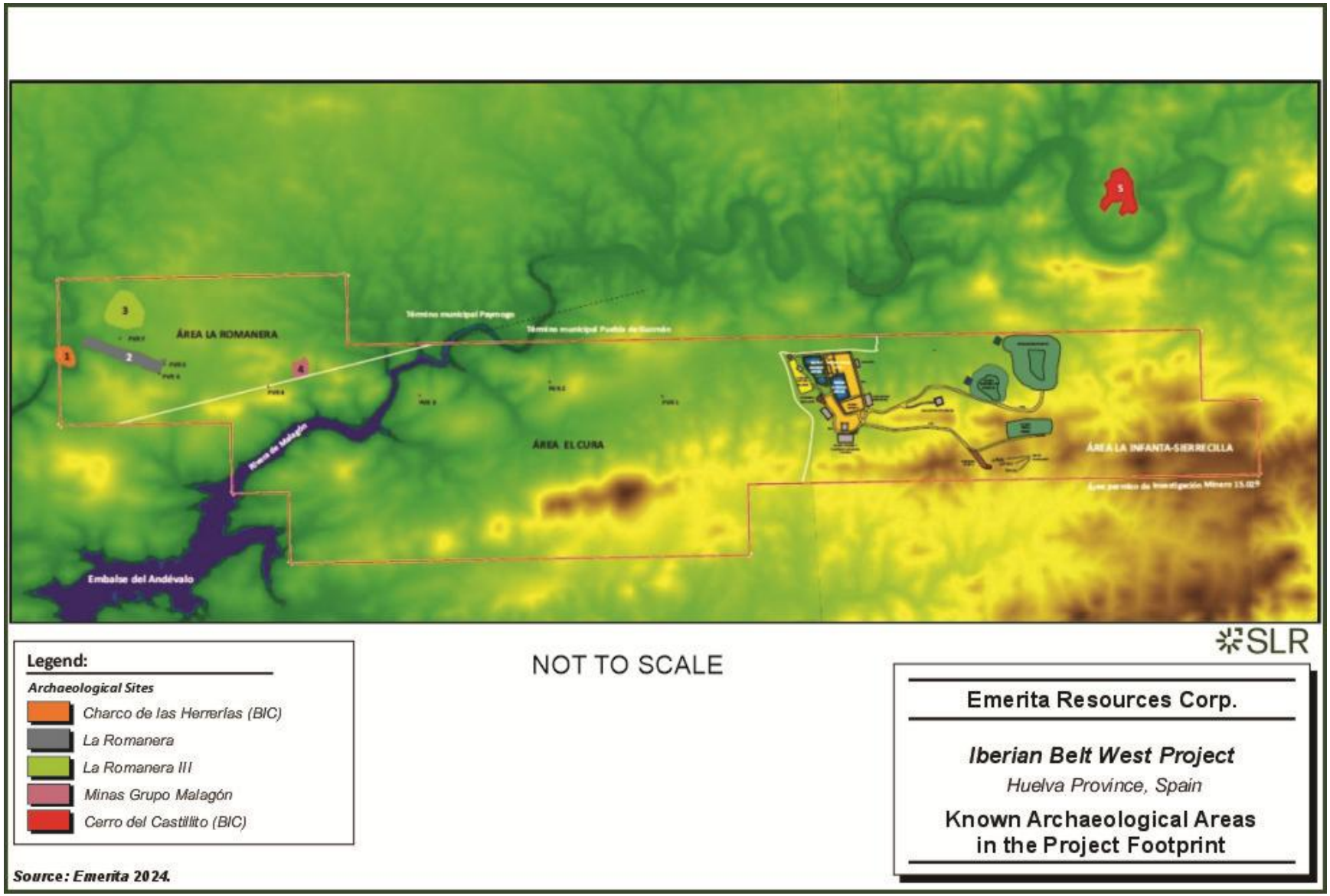
No archaeological evidence was documented in the Sierrecilla–La Infanta survey area, however there remains a risk of chance finds, particularly in areas closer to known sites. According to the resolution, it is mandatory to notify the Delegación Territorial of any chance archaeological finds within 24 hours, therefore development of a chance-find procedure for the Project is required.

Mitigation and management measures for archaeology and cultural heritage impacts include:

- Installation of protective metal mesh fencing around the perimeter of the La Romanera archaeological site to establish a physical barrier against accidental encroachment by machinery during the construction of ventilation shafts PVR 5 and 6.
- Archaeological monitoring of surface earthworks during ventilation shaft construction in the La Romanera and El Cura areas to identify underlying archaeological features not visible on the surface.
- Development of a chance finds procedure and training for relevant workers to mitigate risks to unknown archaeological assets. The procedure will require immediate cessation of works in the vicinity of the find, the area to be secured, and relevant authorities and qualified specialists to be notified within 24 hours. Construction activities will only recommence once the find has been evaluated and any required mitigation, documentation or preservation measures have been completed in accordance with applicable legal requirements and international good practice.

[12] BIC, *Bien de Interés Cultural* in Spanish, which translates to Asset of Cultural Interest, is the highest legal designation of heritage protection in Spain.

Figure 20-7: Known Archaeological Areas in and around the Project Footprint



20.3 Environmental and Social Management

20.3.1 Mining Waste Management

The Project's mining waste management strategy integrates temporary surface storage, underground reuse of mine waste and tailings, and management of contact water. The current PFS basis reflects selected flotation of base metals plus sale of pyrite concentrate and therefore excludes the previous PFP / cyanide-related residue and water streams.

The principal mining waste facilities and systems comprise the temporary mine waste rock stockpile (*Acopio Temporal de Estériles de Mina*; ATEM), the IPS, and the underground paste and rockfill systems. The ATEM and IPS configurations described in the existing Restoration Plan remain relevant as the authority-facing permitting basis; however, the current PFS mine schedule and process mass balance have refined their expected operating functions and required capacities.

Further details for the following waste sections are provided in Chapter 16 (Mining Methods) and Chapter 18 (Project Infrastructure), and included Appendix 20-2.

20.3.1.1 Waste Rock Storage

Waste rock from construction and underground mine development will be temporarily stored in the ATEM before progressive removal for reuse as underground or cemented rockfill where feasible, or later used in closure works.

The existing Restoration Plan provides a storage capacity of approximately 844,000 m³ over an area of 8.03 ha. Generation of approximately 3.88 Mt of mine waste is currently anticipated, however direct-to-underground routing and accelerated reuse of mine waste will be utilised where practicable to control the storage requirement within the ATEM at any one time. Additional temporary capacity may be required if the required drawdown is not achieved.

Waste rock is anticipated to be generally non-hazardous, however some material is non-inert, and sulphide-rich pyritic waste may have acid generating and metal leaching potential. Conservative waste rock management will therefore be applied until further geochemical testing is complete.

The ATEM design includes engineered basal containment, drainage, segregation of clean and contact water, and collection of runoff. Contact water will be directed to the Project’s water treatment system for reuse or post-treatment discharge to reduce the risk of environmental contamination, and clean runoff will be diverted around the facility where practicable.

Following removal of the stored material, the ATEM footprint will be regraded and rehabilitated through placement of suitable soil, revegetation, and post-closure monitoring in accordance with the approved restoration requirements.

For further detail, see Appendix 20-2.

20.3.1.2 Tailings Storage

The current PFS strategy is to maximise the beneficial use of suitable filtered flotation tailings (~88% solids by weight) as underground paste backfill. The previous permitting assumption that approximately 60% of tailings would be used underground and 40% permanently stored on surface is not used as the current PFS operating basis.

Under the current PFS basis, almost all tailings will be used for underground backfill over the LOM, therefore the surface IPS storage capacity is approximately 0.65 Mm³ over 5.4 ha, differing from the permitted restoration basis of 4.39 Mm³ over 36.4 ha. This does not constitute a revised permitted layout, therefore subsequent design and permitting reconciliation is required.

As in Section 20.3.1.1, waste material may be sulphide-bearing with potential acid generation and metal leaching characteristics, and are treated conservatively pending further geochemical testing. The IPS design therefore includes containment and drainage systems for management and treatment of clean and contact water.

Final closure requirements will depend on the actual volume of material remaining within the IPS at the end of operations. The closure concept comprises stable final landforms, sealing or covering of stored residue, water management, revegetation, and long-term monitoring.

Further details are provided in Appendix 20-2.

20.3.1.3 Backfill

The current mine schedule includes two separate fill streams: approximately 4.47 Mm³ of pastefill (primarily tailings material), and 1.71 Mm³ of rockfill over the LOM.

Backfilling provides both operational and environmental benefits by supporting underground openings and maximising reuse of mine waste and flotation tailings within the mine, thereby reducing the volume and footprint of permanent surface waste storage. The principal environmental controls associated with underground backfill include confirmation of the geochemical suitability of backfill material; Project-specific filtration, rheology, strength, and pumpability testing; controlled binder and water addition; operational paste quality control; water management; segregation of unsuitable materials; infrastructure inspection and maintenance; and coordination of backfill placement with the mine sequence and geotechnical requirements.

The final paste recipe, binder demand, water content, material acceptance criteria, and monitoring requirements will be refined during the next Project phase. Further details are included in Appendix 20-2.

20.3.2 Non-Mining Waste Management

Non-mining wastes generated throughout the LOM will be managed separately from extractive waste in accordance with applicable Spanish and EU waste legislation and the waste management hierarchy of prevention, reuse, recycling, recovery, and disposal.

A Project-wide Non-Mining Waste Management Plan has not been provided for review as part of the current PFS information, therefore a formal plan should be completed prior to construction and integrated with the ESMP. The plan should define waste streams, classification, segregation and storage requirements, responsibilities, approved transport and disposal routes, documentation and traceability requirements, spill-response measures, and contractor-management requirements.

20.3.2.1 Wastewater

The Project will generate different water and wastewater streams that require separate management according to their source and quality.

Domestic sewage and sanitary wastewater from offices, welfare facilities, and other occupied areas will be managed through the Project's dedicated sanitary wastewater system, separate to mining and process/contact water circuits.

The current PFS water treatment basis includes an indicative 500 m³/h water treatment plant, with an assumed annual utilisation of 60%. Water treatment sludge (approximately 1,300 tpa of dry sludge) is retained as a separate residue stream. The final design and sludge disposal requirements will be confirmed at a later Project stage.

20.3.2.2 Hazardous Waste Management

Potentially generated non-mining hazardous wastes include waste oils and lubricants, fuels and contaminated materials, waste chemicals, acid and alkalis, laboratory and medical waste, contaminated soils, and other materials classified as hazardous under applicable legislation.

Until the Project-wide Waste Management Plan is finalised (prior to construction), hazardous wastes should be segregated and managed through secure, covered storage arrangements incorporating secondary containment. Storage areas should include spill-response equipment and controls to prevent release to soil, surface water, or groundwater.

Hazardous waste inventories, movement records and disposal documentation should be maintained, and off-site transport, treatment, and disposal undertaken only through appropriately authorised contractors and facilities. Hazardous non-mining wastes should not be placed within the ATEM, IPS, or underground backfill system unless the material has been specifically characterised, demonstrated to be technically and environmentally compatible, and its proposed use or disposal route is permitted.

20.3.3 Pyrite Concentrate Management

Under the selected PFS process route, pyrite concentrate is treated as a product stream rather than as a waste or process residue. It is therefore not assigned to ATEM, IPS or paste backfill under the selected base case.

No dedicated long-term pyrite-concentrate storage facility is included within the selected design, however a 30-day covered temporary storage facility is planned should temporary on-site product storage be required. The final requirements for pyrite-concentrate product specifications and management will be confirmed at a later Project stage.

20.3.4 Water Management and Water Treatment

The Project water-management system includes the underground mine, process plant, ATEM, IPS, paste backfill facilities and any pyrite-concentrate handling or storage areas. The strategy is based on segregation of clean and contact water (diversion of clean water and treatment of contact water), minimisation of contact between runoff and mine-affected materials, and maximisation of recycle and reuse, to meet operational and environmental requirements.

The current process/contact-water treatment allowance is anticipated to be approximately 2.63 Mm³/y of treated water, however the treatment requirement and demonstrated capacity will be confirmed at a later Project stage. The final water treatment design remains dependent on completion of a site-wide water balance, water-quality modelling and treatment test work.

Further details are provided in Appendix 20-2.

20.3.5 Social Management

20.3.5.1 Emerita *Compromiso Sostenible* Foundation

Social management for the Project is structured around a dedicated institutional mechanism—the Emerita *Compromiso Sostenible* Foundation (Emerita Sustainable Commitment Foundation in English) —supported by formal corporate policies, management systems, monitoring programmes, and local employment and procurement initiatives. This framework provides a structured approach to social performance consistent with international good practice and supports the Project's long-term Social Licence to Operate (SLO).

Organisational Structure and Community Team

The Foundation operates under a defined governance and operational structure designed to ensure accountability, transparency, and effective delivery of social programmes through strong local integration and continuous engagement with communities. The two main operational areas are the Social Programme, responsible for community initiatives and stakeholder engagement, and Projects Administration, responsible for financial management, compliance, and reporting.

Community-level roles include a Territorial Advisor responsible for field coordination, local engagement, and liaison with community stakeholders, and a Local Office Representative, based in Paymogo, ensuring day-to-day implementation and territorial presence.

Corporate Policies, Management Plans, and Monitoring Programmes

The Foundation and the Company are supported by formal policies and management systems, including the following key policies (aligned with IFC PS and GIIP for social governance):

- Whistleblowing / Grievance Policy, providing confidential and anonymous reporting channels, protection against retaliation, and formal investigation procedures.
- Data Protection Policy, ensuring compliance with applicable regulations and secure handling of personal data.
- Transparency Policy, requiring publication of annual reports, financial statements, and disclosure of project results.
- Code of Ethics, establishing principles of integrity, respect, responsibility, equity, and transparency, and prohibiting corruption, fraud, discrimination, and misuse of resources.

Management plans and monitoring include annual planning approved by the Board of Trustees, defined project selection and evaluation criteria, and monitoring of social impact indicators, financial execution, reporting requirements, and internal grievance, data and conflict-of-interest controls. These systems ensure traceability, accountability, and continuous improvement of social programmes.

Local Employment and Procurement Initiatives

The Company promotes local economic development through targeted employment and procurement measures. This includes priority hiring of local workforce supported by training and skills development programmes, as well as education-to-employment pathways such as scholarships. Support is given to local suppliers and service providers, and funding provided for community-based economic initiatives to stimulate local entrepreneurship.

These initiatives aim to maximise local economic benefits, reduce social inequality, and strengthen long-term regional resilience.

20.3.5.2 Stakeholder Engagement Plan

A Stakeholder Engagement Plan (SEP) will be developed and implemented to ensure ongoing, transparent, and meaningful engagement with stakeholders throughout the Project lifecycle.

The SEP expands on already identified key stakeholder groups (Section 20.2.6.6), and defines appropriate methods and frequencies of engagement based on stakeholder interests, concerns, and the Project's risk profile. Engagement activities will include information disclosure and consultation regarding Project activities, potential impacts, mitigation measures, and opportunities for stakeholder participation.

The SEP will be implemented in accordance with GIIP and lender requirements, including IFC PS 1, and will be periodically reviewed and updated as the Project progresses. Stakeholder feedback will be documented and considered in Project planning and decision-making processes, while a dedicated grievance mechanism will provide stakeholders with a formal avenue to raise concerns and seek resolution of Project-related issues.

20.3.5.3 Grievance Mechanism

Currently there is no formal grievance mechanism in place. A Project-level grievance mechanism will be established prior to construction to provide stakeholders with an accessible and transparent process for raising concerns related to Project activities. The mechanism will be designed in line with GIIP and lender requirements, scaled to the Project’s risks and impacts, and will be monitored and periodically reviewed throughout the Project lifecycle to support constructive relationships with stakeholders.

Multiple grievances channels will be made available, including verbal, written and electronic formats, with the option to submit complaints anonymously. All grievances will be recorded, acknowledged, investigated, and responded to within defined timeframes, with outcomes communicated to complainants and tracked through a grievance register. The mechanism will be disclosed through ongoing stakeholder engagement activities to ensure stakeholders are aware of their rights and the available avenues for raising concerns.

20.3.6 Occupational Health and Safety

Emerita has already developed dedicated OHS documentation for the IBW Project, namely a Safety Report prepared by INERCO (July 2025) and a Self-Protection Plan prepared by Emerita (September 2025). Together, these documents provide a framework for OHS management, emergency preparedness, and site security.

20.3.6.1 Training

OHS training has been developed for the Project covering both direct employees and contractors, with the following key elements:

- Site-specific induction training for all staff and contractors, covering key risks, personal protective equipment (PPE) requirements, emergency procedures, and reporting of incidents, near misses, and unsafe conditions.
- Task-specific and risk-based training for personnel performing higher-risk activities that are required to hold role-specific qualifications (e.g., drilling, earthworks, explosives, heavy equipment operation).
- Contractors are integrated into the same OHS framework as Emerita staff, requiring compliance with Emerita’s OHS policies and procedures.

- Ongoing refresher training and regular toolbox talks (daily/weekly, depending on activity) focussing on recent incidents, changes in procedures, and seasonal or activity-specific risks (e.g., heat stress, fire risk, heavy rains).

A comprehensive Training Matrix and Annual Training Plan will be developed during the next phase of the Project.

20.3.6.2 Security

The Security Report and Self-Protection Plan together define a basic but robust security concept for a greenfield mining project in permitting phase, with the following main components:

- Perimeter control and fencing around critical areas (e.g., explosive magazines and key infrastructure) to prevent unauthorised access and interference with operations.
- Management of access through controlled entry gates, visitor registration procedures, identification badges for employees and contractors, and vehicle access control (permits, inspections, speed limits, designated routes).
- Security personnel to monitor access points, conduct patrols, support emergency response, and coordinate with site management in case of incidents.

The documents effectively outline the core elements of a Security Management Plan, however a formal plan should be developed, aligned with IFC PS and Voluntary Principles on Security and Human Rights.

20.3.6.3 Occupational Health and Safety Management

Emerita has already established a structured OHS management framework, supported by the work of INERCO and the internal Self-Protection Plan, providing a strong basis for later certification under ISO 45001 or equivalent. The Project's OHS organisation includes an OHS lead and other officers responsible for site-based and overall OHS strategies, and external specialised support (INERCO) for regulatory alignment.

OHS indicators (incidents, near misses and corrective actions) will be reported regularly, and review meetings conducted at least monthly to track performance. Accident and incident findings and corrective/preventive actions will be formally documented and fed back to the workforce to avoid recurrence.

Emerita has implemented an internal, anonymous grievance mechanism where workers can report harassment, interpersonal conflicts, and safety breaches not resolved through the above channels. The mechanism is based on non-retaliation and aims to foster a culture of transparent reporting and trust.

20.3.6.4 Fire Safety

The Self-Protection Plan and Safety Report address fire safety as a core risk area, with the following key elements:

- Fire water and firefighting resources – dedicated fire water storage areas sized according to applicable Spanish regulations and industrial standards, fire hydrants or hoses in critical areas, and portable fire extinguishers.
- Fire detection and alarm systems in enclosed or high-risk areas (e.g., electrical rooms, control rooms, fuel storage).

- Emergency fire safety protocols including clear roles and responsibilities, evacuation routes, and fire response training.

Detailed hydraulic calculations, equipment specifications, and integration with plant design will be further developed during Feasibility and Detailed Engineering.

20.3.6.5 Emergency Preparedness and Response

The Self-Protection Plan constitutes the core Emergency Preparedness and Response (EPR) system elements for the IBW Project, consistent with Spanish regulatory requirements for industrial self-protection. The EPR system covers and defines the following areas:

- Credible emergency scenarios (fire, explosion, spill, medical emergency, severe weather, external threats, etc.).
- Organisational structure and communication protocols for emergency response.
- First aid and medical response, including on-site trained first aiders and basic medical equipment, and use of local health centres and hospitals as referral facilities.
- Coordination with local emergency services in line with Spanish self-protection regulations, including identification, communication and alignment with local emergency services (fire brigade, civil protection, medical services, police)
- Periodic drills to test the effectiveness of the EPR system and continuous improvement through debriefings and corrective actions.

20.3.7 Community Health and Safety Plan

A Community Health and Safety Plan (CHSP) will be developed and implemented prior to the commencement of construction to manage and monitor potential risks to local communities arising from Project activities throughout the construction, operation, and closure phases of the Project. The plan will establish measures to prevent or minimise impacts from population influx, noise and vibration, dust, hazardous materials, emergency situations, and interactions between the workforce and local communities. The CHSP will define responsibilities, procedures for communities, monitoring requirements, and stakeholder communication protocols. The plan will be reviewed periodically to ensure its continued effectiveness and alignment with applicable regulatory requirements and good international industry practice.

As part of the CHSP, a Traffic Management Plan will be developed to manage risks associated with Project-related vehicle movements. The plan will include designated haulage routes, speed restrictions, driver training, vehicle maintenance requirements, and monitoring procedures to minimise risks to local communities, road users, pedestrians, livestock, and agricultural activities. The Traffic Management Plan will be reviewed periodically and updated as necessary throughout the life of the Project to reflect changing operational requirements.

20.3.8 Mine Closure

20.3.8.1 Restoration Requirements

Mine closure in Spain is governed by Royal Decree 975/2009, on the management of waste from the extractive industries and the protection and rehabilitation of the area affected by mining activities. The Decree requires submission of a Restoration Plan, stipulating that "no authorisations, permits or concession regulated by the Mining Law may be granted without an authorised restoration plan"[13].

A Restoration Plan was developed for the Project in 2025, and resubmitted to the Government of Andalusia in April 2026 for permitting purposes following revisions and clarifications. Upon confirmation of International Financial Institution (IFI) standards applicable to the Project (such as IFC PS / EBRD PR), this Restoration Plan should be amended to reflect guidelines stipulated by the IFI, and a formalised conceptual mine closure plan developed.

Restoration and Closure Plans

The Project's restoration plan covers the full footprint of the Project, including underground mining chambers; ventilation shaft platforms; ATEM; IPS; surface platforms; water management ponds; mining roads and access tracks; and other ancillary areas. Table 20-9 outlines progressive rehabilitation and final closure activities that will be undertaken on site to restore disturbed land as early as possible.

Table 20-9: Progressive Rehabilitation and Closure Activities

Activity	Description
Progressive rehabilitation	Progressive backfilling of mine waste into underground voids. Backfilling and dismantling of water management ponds when no longer required. Profiling of the ATEM and IPS slopes. Progressive decommissioning and revegetation of temporary Project roads and construction platforms.
Final closure	Dismantling and removal of all non-permanent facilities (e.g. processing plant, ATEM, water treatment plant, storage areas and supporting facilities). Sealing of the IPS and retention of the associated drainage facilities. Regrading of disturbed surfaces to stable slopes (<30%) and placement of topsoil to avoid erosion and sedimentation. Revegetation using native species and re-establishment of natural drainage. Backfilling or securing of ventilation shafts and underground access points.

Biodiversity offsetting may also be required during closure to counteract potential impacts to the Andévalo Occidental ZEC.

Stakeholder engagement is also an important aspect of the Project's closure activities, and includes the local municipalities of Paymogo and Puebla de Guzmán, regional authorities of with the government of Andalusia, environmental agencies and managers of the Andévalo Occidental ZEC, archaeological authorities, landowners and livestock operators, and local communities. ICMM mine closure guidelines reiterate the importance of ongoing stakeholder

[13] Royal Decree 975/2009 (2009) boe.es/buscar/doc.php?id=BOE-A-2009-9841

engagement throughout the life of the Project to manage social risks and identify mutually beneficial closure outcomes for both the Project and local communities.

The following closure opportunities were identified for the Project, which should be further considered as the Project progresses, particularly during development of the conceptual and final mine closure plans:

- Restoration of degraded historical mining areas.
- Long-term land use for livestock, forestry, and conservation
- Enhancement of Andévalo Occidental ZEC habitat connectivity
- Strengthening of social licence through early and transparent closure planning
- Potential for diversification of land use

Post-Closure Monitoring

A post-closure monitoring period of 5 years to 10 years (30 years for the IPS in accordance with Royal Decree 975/2009) will be maintained to ensure long-term success of restoration activities. During this time, the viability of revegetated areas will be monitored to allow for implementation of corrective measures such as supplementary watering or repeat revegetation. Soil stability, erosion, and compaction will also be monitored, as well as hydrological performance related to runoff, sedimentation, and water quality.

The structural stability of remaining infrastructure will be monitored, with periodic inspections for cracks and signs of damage, as well as any potential impacts to human health or the surrounding environment, such as discharges of ARD. Safety inspections will be carried out on sealed shafts and underground access points, with signage indicating potential risks to land users.

Corrective actions will be implemented if monitoring indicates deviations from expected performance. These actions will be developed as part of the Mine Closure Plan.

20.3.8.2 Asset Retirement Obligations (AROs)

Project Closure Costs

The Project's AROs approach has been developed considering both national and international good practice standards, including Royal Decree 975/2009, ICMM Integrated Mine Closure Good Practice Guide, and ICMM's work on financial concepts for mine closure. The Project's ARO framework also reflects general principles from International Financial Reporting Standards (IFRS) / International Accounting Standards 37 (IAS 37).

The Project's current AROs in the form of the restoration plan resubmitted to the government of Andalusia in April 2026 outline a total restoration budget of €38.4 million (including VAT) for all areas and activities included in Table 20-10. This cost represents the current best estimate of the physical closure and post-closure obligations for the entire Project, summarised in Table 20-10. Contingencies, inflation adjustments, reporting and compliance costs associated with regulatory follow-up and performance verification, have also been included in this cost.

Table 20-10: Activities Included in Project AROs

Activity	Description
Physical Closure and Dismantling of Facilities	
Removal of non-permanent and temporary facilities	Removal of ventilation shafts, ATEM, IPS, surface infrastructure, water management ponds, roads, and other ancillary areas including process equipment, buildings, storage areas, and laydown areas. This includes required labour and equipment.
Decommissioning of water management infrastructure	Decommissioning of auxiliary water ponds and associated hydraulic structures, and subsequent infilling or reshaping.
Demolition and dismantling of surface platforms and IPS / ATEM infrastructure	Including segregation, classification, and off-site management of demolition waste and recyclable materials.
Progressive Rehabilitation and Final Landform Rehabilitation	
Regrading and reprofiling of disturbed surfaces	Including ATEM, IPS, roads and other disturbed areas to stable landforms consistent with pre-mining topography and hydrology.
Revegetation and habitat restoration	Using native species, with the explicit objective of achieving no net loss of habitat and, where feasible, restoring identified Habitats of Community Interest.
Rehabilitation of mining roads and tracks	Including removal, decompaction, revegetation, and re-establishment of natural drainage.
Underground and Subsurface Closure	
Sealing and securing of underground access points and ventilation shafts	Including physical barriers, backfilling or plugging, and long-term stability measures to prevent accidental access and ensure geotechnical safety.
Management of residual water flows from underground workings and restored ponds	Including long-term drainage and erosion control measures.
Post-Closure Monitoring and Aftercare	
Vegetation monitoring and maintenance	Including replanting, weed control and erosion repair during the closure and post-closure periods.
Monitoring of water quality, drainage performance and structural stability	Monitoring of restored landforms, ponds, and slopes, with defined timeframes and performance indicators.
Ongoing environmental surveillance	Confirm that restoration objectives such as stability, no significant erosion, and habitat recovery are being met.

These obligations are aligned with the Project's vision to return the Project affected areas to their pre-mining state as far as possible during mine closure, with no net loss of habitat.

The Project's AROs should be continually updated to reflect:

- Design changes;
- Changes in regulatory obligations, including AAU and Natura 2000 requirements (which may include biodiversity offsetting costs) and future amendments to Spanish or EU environmental, mining, or waste legislation;

- Inflation, labour and material cost changes, and waste management market changes; and
- Increased Project knowledge (reduction in uncertainties), including knowledge of baseline environmental and social conditions.

As the footprint and volume of the IPS is likely to be reduced following the revised saleable output of the processing operation, the AROs developed in April 2026 may already require updating.

The Restoration Plan, defined in Section 20.3.8.1, is primarily technical and environmental in nature, therefore social retirement obligations such as workforce transition and redundancy costs and fulfilment of social and community development commitments through closure are only included conceptually. Stakeholder engagement is planned to continue into the closure planning phase, particularly regarding future land uses of restored areas and opportunities to integrate closure works with local development objectives. Social commitments and expectations arising from this engagement will be reflected in the scope and cost of AROs at a later date, especially where they require additional restoration features, extended monitoring, or community-focused measures.

20.4 Future Work (Environmental and Social Roadmap)

20.4.1 Environmental and Social Scoping Study

Upon confirmation of the Project's chosen IFI requirements (e.g., IFC PS, EBRD PR), an E&S scoping study should be undertaken to assess alignment of current Project information with IFI standards and identify any compliance gaps. Key scoping tasks include:

- Review of available information and summary of existing baseline information and gaps, including relevant available information such as baseline studies, census and cadastral data, and satellite imagery to identify potential sensitive receptors;
- Review and assessment of Project alternatives such as location, technology, design, mitigation options and the no-project scenario, including evaluation of prior decisions against E&S risks, stakeholder engagement outcomes, and application of the mitigation hierarchy;
- Identification of interested and affected stakeholders, including vulnerable and underrepresented groups, and scoping-stage consultation to inform key ESIA issues;
- Design and implementation of an ESIA scoping process to identify key E&S issues and risks associated with the Project to be addressed in the ESIA, in line with IFI requirements; and
- Design of required ESIA baseline studies based on gaps in IFI requirements identified within existing baseline information.

These activities will define the scope and work programme for the ESIA, including Project description and alternatives, regulatory context, baseline overview and data gaps, baseline design, identification and screening of key E&S risks and impacts (including cumulative and associated facility risks), and E&S management plans.

20.4.2 Stakeholder Engagement Plan

A SEP will be developed as part of the scoping / feasibility phase, expanding on the work already undertaken to date through the Emerita *Compromiso Sostenible* Foundation.

A preliminary SEP should include:

- Identification and mapping of affected and interested stakeholders, including vulnerable and under-represented groups;
- Definition of early-stage disclosure, engagement and feedback arrangements to identify key E&S issues for the ESIA, further developing those established by the Emerita *Compromiso Sostenible* Foundation; and
- Procedures for capturing and applying stakeholder feedback to inform the ESIA scope and the transition to a formalised, ESIA-stage SEP.

20.4.3 Baseline Data Collection

As part of the E&S scoping study, compliance of existing baseline information with relevant IFI requirements should be determined, and if necessary, a programme defined for additional E&S baseline surveys for the ESIA, with the aim to provide a representative picture of the current state of the physical, biological, and socio-economic environment relevant to the Project. An example programme is outlined in Appendix 20-3 (based on preliminary review of currently available information).

20.4.4 Environmental and Social Impact Assessment (ESIA)

The objective of the ESIA is to determine the potential E&S impacts of the IBW Project in all of its phases (construction, operation, and closure). It identifies the sources of potential impacts associated with the Project's infrastructure and activities, as well as considers impacts from Project-induced social changes, such as direct and indirect employment, economic inputs, and demographic changes. Impacts are assessed with regards to the appropriate IFI framework and Project-specific criteria (Appendix 20-3).

20.4.5 Environmental and Social Management Plan

A standalone ESMP should be developed as part of the ESIA, outlining measures that will be implemented to avoid and reduce the Project's E&S impacts in accordance with the applicable laws, regulations, and best practices. The final list of required management plans would be determined during development of the ESIA; however, the following plans are likely to be applicable to the Project:

- E&S management and monitoring plan
- Biodiversity monitoring plan
- Biodiversity action plan
- GHG, Climate change, and air quality monitoring plan
- Soils and erosion control monitoring plan
- Noise and vibration monitoring plan
- Emergency prevention, preparedness and response plan
- Mining and non-mining waste monitoring plan

- Water and wastewater monitoring plan
- Community management and development plan
- OHS monitoring plan
- Community health and safety monitoring plan
- Chance finds procedure
- Conceptual mine closure and rehabilitation plan

20.4.6 Additional Studies

20.4.6.1 Livelihood Restoration Plan

An assessment of impact on livelihoods should be developed as part of the ESIA. A Livelihood Restoration Plan (LRP) should be developed where Project activities result in economic displacement or restrictions on access to land, natural resources, or livelihood activities. The LRP will identify affected households and vulnerable groups, assess the nature and extent of livelihood impacts, and define measures to restore, and where feasible improve, affected persons' livelihoods and standards of living. The plan will establish eligibility criteria, livelihood restoration measures, consultation and grievance processes, implementation responsibilities, monitoring indicators, and funding arrangements to ensure affected persons are able to achieve livelihood outcomes that are at least equivalent to pre-Project conditions, in line with applicable lender requirements (IFC PS5) and international good practice.

21.0 Capital and Operating Costs

21.1 Capital Costs

21.1.1 Basis of Capital Cost Estimate

The capital cost estimate for the IBW Project has been prepared to a PFS level of accuracy (±15%). It is considered consistent with an Association of the Advancement of Cost Engineering (AACE) Class 4 estimate. The estimate incorporates mining, process plant, infrastructure, water management, tailings management, paste backfill infrastructure, Owner's costs, indirect costs, contingency, and closure costs. The estimate is presented in flat, real US dollar terms.

Mining capital costs were developed from first principles using detailed mine schedules, equipment productivities, and vendor quotations. Major mobile equipment quotations were obtained from Epiroc and Normet, supplemented by cost data from Sandvik Group, MacLean Engineering, and Hermann Paus Maschinefabrik GmbH. Infrastructure and fixed equipment costs were derived from vendor quotations, contractor pricing, historical project data, and the SLR cost database.

The underground mine capital cost estimate comprises the following key elements:

- Capitalised development costs including lateral development mining in waste for service ramps and Railveyor declines (including portal construction), footwall and level access drives, mine infrastructure installations (excluding the backfill plant), and vertical development for material passes, ventilation, and escapeways.
- Mobile equipment purchases, including the purchase of new mobile equipment units during the pre-production period to establish the initial mining fleet and, as production ramps up, to increase the size of the fleet as required to sustain production demands.
- Mobile equipment overhauls and replacements.
- Miscellaneous, fixed, and other equipment. This category includes fixed equipment such as primary and secondary ventilation fans, dewatering pumps, electrical substations and power centres, refuge chambers, technical equipment and software, and minor plant. It also includes allowances for communications infrastructure and tools.

Processing and infrastructure capital costs were prepared by Zenito using vendor quotations, budget pricing, and factored estimated and benchmarked costs from comparable projects. The process plant estimate includes crushing, grinding, comminution and flotation circuits, concentrate dewatering, pyrite processing, tailings dewatering, reagents handling, utilities, and supporting infrastructure.

Capital costs associated with the ATEM facilities, IPS facility, paste backfill system, and water treatment infrastructure were developed by SLR using project-specific engineering designs, equipment sizing, vendor quotations, and benchmarked cost data. The estimates include direct construction costs, associated infrastructure, and contingency allowances considered appropriate for the PFS level of study. These facilities support mine waste management, filtered tailings storage, underground paste backfill distribution, and contact water treatment requirements.

The water treatment plant has been estimated using a Build-Own-Operate (BOO) strategy, reflecting Emerita's preference to engage a specialist operator with the technical expertise and resources required to manage water treatment operations and associated regulatory

obligations. Under this arrangement, the facility is assumed to be designed, owned, operated, and maintained by the third-party service provider.

The underlying capital requirement was established based on SLR's first-principles estimate, including an additional mobilisation allowance.

No financing costs associated with the BOO arrangement have been included in the financial model.

Off-site infrastructure costs have been estimated by Emerita, taking into consideration the well-developed regional infrastructure surrounding the Project. The estimates reflect the anticipated requirements for connections to and, where necessary, upgrades of existing infrastructure to support Project development and operations.

Owner's costs have been factored based on benchmarks derived from comparable mining projects, industry databases, and recent technical studies.

Closure and rehabilitation costs have been estimated by Emerita based on the project-specific restoration plan prepared for the IPS facility in accordance with applicable Spanish mining regulations. The estimate includes costs associated with final landform stabilisation, installation of cover and drainage systems, infrastructure decommissioning, revegetation, environmental monitoring, and post-closure maintenance. The resulting closure liability has been incorporated into the financial evaluation through progressive rehabilitation expenditures during operations and a post-closure provision for final closure and long-term monitoring activities.

21.1.2 Capital Cost Summary

The project capital cost estimate comprises initial capital, sustaining capital, and closure costs over the life of the operation. Initial capital includes the costs required to establish mining, processing, infrastructure, and supporting facilities prior to commencement of operations, together with an appropriate contingency allowance. Sustaining capital reflects ongoing capital investments required to maintain production capacity and operational performance throughout the project life, while closure costs provide for site rehabilitation and decommissioning activities.

The total capital requirement for the IBW Project is estimated at US$858.2 million, comprising initial capital, sustaining capital, and closure costs. Initial capital is estimated at US$566.7 million, sustaining capital at US$279.5 million, and closure costs at US$12.0 million. A US$63.6 million contingency, 15% of initial capital costs, is also included in the initial capital cost estimation.

A summary of the estimated project capital costs is presented in Table 21-1.

Table 21-1: Project Capital Cost Summary

Category	Cost (US$ million)
DIRECT COSTS	**394.7**
Mine-Related	189.1
Process-Related	126.6
Mine waste / ATEM	4.5
Tailings / IPS	19.3
Paste Backfill	43.8

Category	Cost (US$ million)
Water Treatment Plant Contractor Mobilisation Fee	6.8
Infrastructure (off site)	4.7
INDIRECT COSTS and EPCM	**36.3**
Processing Indirect Cost and EPCM	26.1
Mine waste / ATEM	0.7
Tailings / IPS	2.9
Paste/backfill	6.6
OWNER'S COSTS	**19.7**
CONTINGENCY	**63.6**
Mining Contingency	28.4
Processing and Infrastructure Contingency	22.9
Water and Waste Management Infrastructure	11.7
Off-Site Infrastructure	0.7
FINANCING	**-**
Financing	-
OTHER COSTS	**52.4**
Working Capital (Processing Component)	1.7
Capitalised Initial Operating Costs	50.7
INITIAL CAPITAL	**566.7**
Sustaining Capital	**279.5**
Escalation	-
Post-Mine Closure Costs*	12.0
TOTAL PROJECT CAPITAL	**858.2**

21.1.3 Initial Capital

Initial capital costs include the following components:

- Underground mine development
- Underground mobile equipment fleet purchases
- Railveyor installations
- Process plant construction
- Mine waste and water treatment infrastructure
- Tailings and filtered tailings infrastructure
- Paste backfill system

- On-site and off-site infrastructure
- EPCM and Owner's costs
- Working capital and capitalised pre-production operating costs

The largest components of the initial capital estimate are mine-related infrastructure and capital development costs (US$189.1 million), process plant and site infrastructure costs (US$126.6 million), and water, tailings, and paste backfill infrastructure (US$67.6 million direct cost basis).

Direct processing costs include the following components:

- All labour required for project construction and management activities (excluding EPCM)
- All material and equipment required for construction
- Mechanical, electrical, control, instrumentation, civil works, earthworks and piping installation services
- Transport and freighting services
- Construction and installation

Indirect processing costs are associated with, but not directly related to, the capital build of the Project and cannot tangibly be identified or directly attributed to the Project. The following capital indirect costs are included:

- Accommodation
- Construction facilities

21.1.3.1 Mining

Total mining capital is estimated at US$438.9 million, comprising US$189.1 million of pre-production (initial) capital and US$249.8 million of deferred (sustaining) capital.

La Romanera accounts for the majority of the mining capital estimate (US$354.3 million), reflecting the scale of underground development, Railveyor infrastructure, and mobile equipment required to establish the operation.

Development costs represent the largest component of the mining capital estimate, accounting for approximately 52% of total mining capital.

Deferred capital is primarily associated with ongoing underground development and equipment replacements required to sustain production over the LOM, with the majority of sustaining capital attributable to La Romanera and the future development of the La Infanta and El Cura deposits. A breakdown of the mining capital estimate by deposit and major cost category is presented in Table 21-2.

Table 21-2: Mining Capital Cost Summary by Deposit and Cost Category

Mining Capital Costs	Total (US$ M)	Pre-production (US$ M)	Deferred (US$ M)
La Romanera			
Capital equipment costs	127.6	47.9	79.7
Capital Railveyor costs	25.2	20.4	4.8
Capital development costs	196.0	89.2	106.8
Misc. capital costs	5.5	4.4	1.1
Total Capital Costs: La Romanera	**354.3**	**161.9**	**192.4**
La Infanta			
Capital equipment costs	3.6	-	3.6
Capital Railveyor costs	3.5	-	3.5
Capital development costs	17.4	-	17.4
Misc. capital costs	2.1	-	2.1
Total Capital Costs: La Infanta	**26.6**	**-**	**26.6**
El Cura			
Capital equipment costs	23.0	13.6	9.4
Capital Railveyor costs	-	-	-
Capital development costs	33.8	13.0	20.7
Misc. capital costs	1.3	0.6	0.7
Total Capital Costs: El Cura	**58.0**	**27.2**	**30.8**
TOTAL MINING CAPITAL COSTS	**438.9**	**189.1**	**249.8**

In addition, operating costs of US$50.7 million incurred during the pre-production period have been capitalised in accordance with the Project accounting approach and are included within the initial capital estimate under “Other Costs” category.

21.1.3.2 Processing

Processing capital is estimated at US$177.3 million, including US$126.6 million of direct costs and US$49.0 million of indirect costs. The estimate is primarily driven by mechanical equipment, installation activities, electrical systems, and process plant infrastructure. Indirect costs include EPCM, construction facilities, contingency, commissioning allowances, and working capital required to support plant start-up. The processing capital cost estimate is summarised by major cost category in Table 21-3.

Table 21-3: Processing Capital Cost Summary by Major Cost Category

Processing Capital Costs	Cost (US$ million)
200 - Processing	**119.74**
Process / workshop / warehouse	17.46
Washroom Building	0.03
Civil Works	5.85
Concrete works	6.65
Concrete works for buildings	0.64
Control & Instrumentation	6.07
Earthworks - Bulk Cut - Transitional	1.16
Earthworks - Bulk Cut - Rock	3.23
Earthworks - Bulk Fill	0.88
Electrical	8.10
Mechanical	40.61
Installation	14.17
Forklift	0.08
FEL	1.06
Pick up	0.15
Bobcat	0.03
Piping	4.08
Platework	5.41
Support steel works	4.06
300 - Utility and Services	**2.38**
Process / workshop / warehouse	0.03
Civil Works	0.10
Concrete works	0.14
Control & Instrumentation	0.15
Electrical	0.20
Mechanical	1.00
Installation	0.35
Piping	0.10
Platework	0.27
Support steel works	0.04

Processing Capital Costs	Cost (US$ million)
400 - Infrastructure	**4.45**
Vestrooms and showers	0.12
Offices	0.18
Laboratory	0.18
Kitchen & Dining Building	0.12
Process plant: offices, kitchen & dining room, vestrooms, showers & toilets	0.23
Access Control Gate Building	0.03
Civil Works	0.09
Concrete works	0.20
Concrete works for buildings	-
Earthworks - Bulk Cut - Transitional	1.42
Earthworks - Bulk Cut - Rock	0.94
Earthworks - Bulk Fill	0.93
Direct Total	**126.56**
Control and instrumentation	0.28
Electrical	0.28
Mechanical	0.38
Process	0.28
Spares	0.20
Accommodation	2.46
Construction facilities (4% of directs)	4.33
Contingency (15%)	*22.90*
EPCM	17.72
First Fills	0.20
Indirect Total	**49.04***
Working Capital	1.67
Cash reserve	-
Management reserve	-
Critical and insurance spares	0.84
Operating spares and consumables	0.84
Working Total	1.67
Processing Total	**177.27**

* Note: Indirect costs presented in this table include the contingency allowance of US$22.9M, which is shown separately in the Financial Model and Economic Analysis.

21.1.3.3 Tailings, Waste and Water Management

Capital costs associated with tailings, waste, and water management infrastructure total US$74.4 million and comprise the ATEM facilities, the IPS, the paste backfill system and water treatment infrastructure. The estimate supports the management of mine waste, filtered tailings, contact water, and backfill distribution requirements generated by the planned mining and processing operations. Further details regarding the ATEM and IPS are provided in Section 18 and 20. A summary of the tailings, waste, and water management capital costs is presented in Table 21-4.

Table 21-4: Tailings, Waste, and Water Management Capital Cost Summary

Cost Category	Cost (US$ million)
Mine Waste / ATEM	4.49
Tailings / IPS	19.26
Paste Backfill	43.84
Water Treatment Plant Contractor Advanced Mobilisation Fee	6.78
Total	**74.37**

21.1.3.4 Off-Site Infrastructure

Off-site infrastructure capital totals US$4.7 million and comprises water supply and telecommunications infrastructure. The relatively modest capital requirement reflects the availability of established regional infrastructure and limited requirements for major off-site development. A summary of the surface infrastructure capital costs is presented in Table 21-5.

Table 21-5: Off-Site Infrastructure Capital Cost Summary

Cost Category	Cost (US$ million)
Water Supply / Pipelines	3.30
Telecom / Communications	1.38
Total Off-Site Infrastructure	**4.68**

21.1.3.5 Indirect

Indirect costs and EPCM total US$36.3 million and comprise project management and EPCM services associated with delivery of the Project. The majority of indirect costs are attributable to the process plant and infrastructure works, with smaller allowances associated with the ATEM, IPS, and paste backfill facilities. A summary of indirect costs and EPCM is presented in Table 21-6.

Table 21-6: Indirect Costs and EPCM Summary

Indirect Costs and EPCM	Cost (US$ million)
Processing Indirect costs and EPCM	26.13
Mine waste / ATEM	0.67
Tailings / IPS	2.89
Paste/backfill	6.58
Total	**36.27**

21.1.3.6 Contingency

A contingency allowance of 15% has been applied to all major capital cost categories, including mining, processing and infrastructure, water and waste management infrastructure, and off-site infrastructure.

The contingency allowance is intended to provide for uncertainties associated with the PFS level of engineering and cost estimating. It has been applied to account for potential growth in quantities, pricing uncertainty, and minor scope development within the defined project scope and should not be considered a provision for major scope changes or project expansion.

No formal quantitative contingency analysis has been undertaken. The selected allowance is based on engineering judgement and reflects the current level of project definition, available design information, vendor inputs, estimating methodology, and overall estimate maturity.

The adopted contingency allowance is considered appropriate for a PFS-level study and is at the lower end of the range typically applied to projects at a similar stage of development. As the mining method and floatation flowsheet are conventional and therefore present a lower technological risk and uncertainty the lower contingency is acceptable.

21.1.4 Sustaining Capital

Sustaining capital totals US$279.5 million over the life of the operation and includes:

- Replacement and overhaul of underground mobile equipment.
- Deferred mine development.
- Paste backfill system upgrades and equipment replacements.
- Tailings and water management infrastructure renewals.
- Process plant replacement and refurbishment programs.

Mobile equipment replacement and overhaul represents the largest sustaining capital component and has been scheduled according to equipment life and original equipment manufacturer (OEM) recommendations.

21.1.5 Closure Costs

Total Closure and Rehabilitation costs have been estimated at US$17.1 million (€18.85 million including VAT, or €15.58 million pre-VAT at an exchange rate of 1.10 USD/EUR), based on the restoration plan currently accepted by the Government of Andalusia.

The estimate comprises approximately US$12 million associated with final closure works and post-closure monitoring obligations, together with approximately US$5.1 million for progressive rehabilitation. Progressive rehabilitation costs are incurred during the LOM and have therefore been included within operating costs, while final closure costs are incurred following the cessation of mining operations.

Closure and rehabilitation costs for the IPS have been estimated based on the restoration plan prepared for the Project and in accordance with the methodology outlined in Spanish mining restoration regulations.

The closure scope includes final landform grading, installation of a drainage and cover system over the facility, decommissioning and removal of infrastructure, waste disposal, soil preparation, revegetation, tree planting, and long-term environmental monitoring.

The restoration plan also includes maintenance and replacement of monitoring equipment, periodic technical inspections, and post-closure vegetation management. The estimated direct rehabilitation cost is €13.1 million, increasing to approximately €15.6 million following application of indirect costs and contractor profit. Table 21-7 presents the closure and rehabilitation cost estimate incorporated into the financial model.

As the financial model has been prepared on a VAT-exclusive basis, the rehabilitation provision has been incorporated using the pre-VAT closure cost estimate. The closure strategy assumes progressive rehabilitation where practical during operations, followed by final closure activities at the end of mine life and a post-closure monitoring period of at least 30 years for the tailings facility.

Table 21-7: Summary of Closure and Rehabilitation Cost Estimate

Closure Cost Category	Cost (€ million)	Cost (US$ million)
External slope rehabilitation	0.47	0.52
Monitoring equipment maintenance/replacement during operations	1.35	1.48
Final closure of upper platform	6.09	6.69
Post-closure technical monitoring and inspections	1.15	1.26
Post-closure equipment maintenance/replacement	2.13	2.34
Post-closure vegetation maintenance and replacement	1.91	2.11
Sub-total restoration cost	13.09	14.40
G&A (13%)	1.70	1.87
Contractor profit (6%)	0.79	0.86
Sub-total before VAT	**15.58**	**17.14**
VAT (21%)	3.27	3.60
Total Closure Liability / Financial Guarantee	18.85	20.74

Note: Conversion to US dollars has been undertaken using an exchange rate of 1.10 USD/EUR, consistent with the exchange rate assumptions applied elsewhere in the financial model.

Table 21-7 summarises the estimated closure and rehabilitation costs totalling €15.58 million (US$17.14 million), including progressive rehabilitation activities undertaken during operations and post-closure monitoring and maintenance obligations. The closure schedule assumes that approximately 30% of the total closure liability is incurred progressively during operations through rehabilitation activities, with the remaining 70% incurred at the end of mine life. The timing of these expenditures is summarised in Table 21-8.

Table 21-8: Progressive Rehabilitation and Closure Cost Schedule

Period	Progressive Rehabilitation (% of Total Closure Liability)	Cumulative Rehabilitation (%)
Years 1-5	0%	0%
Years 6-10	5%	5%
Years 11-15	10%	15%
Years 16-20	15%	30%
Post-Closure Period	70%	100%

21.1.6 Exclusions

The following items are excluded from the capital estimate:

- Project financing costs and interest during construction.
- Escalation and inflation of costs and commodity prices.
- Corporate costs.
- Future exploration expenditures.
- Foreign exchange fluctuations.
- Import duties, VAT, and sales tax.
- Costs associated with future project expansions beyond the current PFS scope.

21.2 Operating Costs

21.2.1 Basis of Operating Cost Estimate

Operating costs have been developed from detailed, first-principles mining and processing cost models. Mining cost estimates are based on planned equipment operating hours, labour requirements, consumable consumption, maintenance schedules, and energy usage.

Process plant operating costs were derived from metallurgical testwork results, design criteria, vendor information, and benchmark operating data. The estimate is expressed in flat, real US dollar terms, so it does not account for inflation.

21.2.2 Life-Of-Mine Operating Costs

Total LOM on-site operating costs are estimated at US$2.03 billion, comprising mining, processing, G&A costs, water treatment, waste management, backfill operations, and progressive rehabilitation. Additional off-site costs associated with concentrate transportation, treatment and refining charges (TC/RCs) and concentrate penalties total approximately

US$0.89 billion over the LOM, of which Penalties account for approximately 57% of the total, followed by transportation and sales costs (32%) and concentrate TC/RC (10%).

Table 21-9 provides summary of the Project operating costs.

Table 21-9: Life-of-Mine Operating Costs

Cost Category	Cost (US$ million)
On-site Costs	
Mining	882
Processing	708
General and Administrative	70
Water Treatment, Waste Management and Backfill	363
Progressive Rehabilitation	5
Total On-Site Operating Costs	**2,028**
Off-site Costs	
Treatment and Refining Charges (TC/RC)	92
Concentrate Penalties	506
Transportation and Sales	287
Total Off-Site Costs	**886**

21.2.2.1 On-Site Operating Costs

Mining costs represent approximately 44% of total site operating costs and include underground development, production drilling, blasting, loading, hauling, ground support, ventilation, pumping, labour, maintenance, and power consumption.

Unit costs for materials and supplies were sourced from either 2026 quotations or inflated 2025 quotations, vendor input where available, and the Mining Cost Service. This information is incorporated into the cost model and includes items such as:

- Explosives and blasting consumables;
- Ground support supplies and consumables; and
- Drilling consumables.

OEM-provided data on maintenance parts and overhaul costs were utilised to quantify and qualify maintenance cost estimates for the critical mobile equipment. Labour rates were provided by Emerita and include employee benefits. Burden costs, and fuel, and power pricing assumptions were confirmed by Emerita.

On-site operating processing costs include labour, reagents, consumables, maintenance materials and operating spares, mobile equipment, power, associated infrastructure, utilities, and laboratory costs incurred in producing copper, lead, zinc, and pyrite concentrates.

21.2.2.2 Off-Site Operating Costs

As of the effective date of this report, no commercial off-take agreements or definitive smelter terms have been established for the Project. Smelter TC/RC assumptions applied herein are based on benchmarked market terms considered representative of comparable concentrate products at the time of the study.

Benchmarking undertaken for the PFS indicates that copper concentrate treatment charges are highly cyclical and can be subject to significant short-term volatility. Recent market conditions have demonstrated the potential for treatment charges to decline to exceptionally low levels, with premium, high-quality concentrates occasionally attracting highly favourable commercial terms. In certain circumstances, treatment charges may become effectively neutral or negative, reflecting strong smelter demand and tight concentrate supply.

Notwithstanding this potential upside, the QP considers the use of such anomalous market conditions inappropriate for evaluating the long-term economics of a project requiring an extended development period prior to production. Over the longer term, market conditions are expected to revert towards more typical historical levels as concentrate supply and smelting capacity rebalance.

Accordingly, a long-term treatment charge of US$40/dmt has been adopted as a prudent and reasonable assumption for the purposes of the economic evaluation. The selected value is considered representative of achievable long-term market terms and avoids undue reliance on short-term market distortions.

For zinc concentrates, a long-term treatment charge of US$85/t concentrate has been adopted. This assumption reflects benchmark terms observed for clean zinc concentrates and is considered representative of achievable commercial conditions over the long term.

For lead concentrates, a long-term treatment charge of US$5/t concentrate has been adopted.

No formal off-take agreements or commercial terms have been established for the sale of pyrite concentrate. Based on the independent market assessment completed by Claight Corporation (2026), pyrite concentrate is principally marketed to copper smelters and sulphuric acid producers, with commercial value derived from contained sulphur and, where applicable, precious metal credits rather than through a standardised benchmark pricing mechanism. The study notes that strong sulphuric acid demand, constrained sulphur supply, and ongoing shortages of copper concentrate have supported increased demand for pyrite concentrates, particularly within China and Europe.

Claight further concludes that long-term pyrite market fundamentals remain favourable, supported by growth in sulphuric acid demand from fertilizer production, battery metals processing, and energy transition sectors. China currently represents the dominant market for pyrite-based sulphuric acid production and is expected to remain a key driver of demand. The study also notes that pyrite can provide an attractive alternative feedstock for smelters seeking to supplement sulphur requirements and offset pressure from low copper concentrate treatment charges.

The treatment and refining charge assumptions adopted for the Project are summarised in Table 21-10.

Table 21-10: Benchmark Treatment and Refining Charges Adopted in the Financial Model

Concentrate Treatment Charges: Base Metals	Treatment Charge (US$/dmt)	Refining Charge (US$/oz)		Refining Charge US$/lb
		Au	Ag	Cu
Zinc Concentrate	85.0	nil	nil	n/a
Lead Concentrate	5.0	15.00	0.50	n/a
Copper Concentrate	40.0	nil	nil	0.02
Treatment and Refinery Charges: Pyrite Concentrate	**Treatment Charge (US$/dmt)**	**Refining Charge (US$/oz)**		
		Au	**Ag**	
Pyrite Concentrate	Nill	5.0	0.40	

Penalties for Deleterious Elements

Deleterious element penalties for base metals concentrates have been estimated by Emerita using concentrate assay data from the testwork programmes and penalty schedules benchmarked in the independent concentrate marketing study (Cuadri, 2025).

La Romanera is expected to provide the majority of plant feed throughout the LOM, contributing approximately 83% of total mill feed during most years of operation, and therefore represents the principal determinant of concentrate quality.

Mineralogical and metallurgical testwork completed to date indicates that concentrates from La Infanta and El Cura also contain elevated concentrations of certain deleterious elements. However, representative concentrate quality predictions have not been developed for the planned LOM blended feed schedule, and sufficient metallurgical testwork data, including variability testwork, is not currently available to reliably forecast annual deleterious element concentrations in the final concentrate products. Consequently, a detailed assessment of deleterious element penalty thresholds and associated smelter charges for the forecast blended concentrates could not be completed at the current stage of the study.

In the absence of representative LOM blended concentrate quality predictions, penalty assumptions have been based principally on the predicted concentrate characteristics of La Romanera, supplemented by benchmarked industry penalty schedules and the findings of the Claight marketing study. Given the predominance of La Romanera feed in the production profile, this approach is considered reasonable at the PFS level. Additional metallurgical testwork and concentrate quality modelling are required to confirm blended concentrate specifications and refine deleterious element penalty assumptions in future phases of project development.

With regards to the pyrite concentrate, penalty and commercial assumptions have been developed separately based on the independent pyrite concentrate market assessment completed by Claight (2026). The study reviewed expected pyrite concentrate specifications, marketability, potential end-users, and applicable commercial terms for pyrite concentrate products. Unlike copper, zinc and lead concentrates, pyrite concentrate is not commonly traded under standardised benchmark treatment charge and penalty structures, and commercial

outcomes are typically negotiated on a case-by-case basis with reference to sulphur grade, impurity levels, moisture content, logistics and prevailing sulphuric acid market conditions.

Given the current level of metallurgical testwork and the absence of representative LOM blended pyrite concentrate quality forecasts, the adopted pyrite concentrate penalty assumptions are considered preliminary and appropriate for a PFS-level evaluation. The assumptions reflect the findings of the Claight study (2026) and the QP's assessment of reasonable long-term market conditions; however, additional metallurgical testwork, concentrate quality modelling and future marketing discussions with potential off-takers will be required to further refine the commercial assumptions and confirm any deleterious element penalties applicable to the final pyrite concentrate product.

Summary of the penalty assumptions applied in the economic analysis is provided in Table 21-11 below.

Table 21-11: Summary of Deleterious Element Penalty Assumptions Applied in the Economic Analysis

Concentrate	Unit	Total	Sb	Hg	Fl	As	Other
Zn Concentrate	US$/t conc.	**191.20**	–	171.00	–	–	20.20
Pb Concentrate	US$/t conc.	**101.70**	–	38.40	–	–	63.30
Cu Concentrate	US$/t conc.	**860.60**	211.50	540.00	–	14.50	94.60
Pyrite Concentrate	US$/t conc.	**8.00**	–	–	–	8.00	–

Concentrate Transportation and Handling

All four concentrates are assumed to be transported by road from the Project site to the Port of Huelva, located approximately 80 km from the operation, for subsequent shipment to third-party smelters. The Port of Huelva has been selected as the base-case export route due to its proximity to the Project and established bulk concentrate handling infrastructure.

Transportation and sales costs have been estimated based on the delivery of concentrates from the Project site to the Port of Huelva for export to third-party smelters. Transport costs have been assumed at €7.89/t of concentrate, while port handling charges have been estimated at €7.97/t of concentrate, for a combined logistics cost of €15.86/wmt concentrate. These rates have been benchmarked against comparable concentrate logistics operations in the Iberian Peninsula and are considered appropriate for the assumed transport route and handling requirements. For economic evaluation purposes, costs denominated in euros have been converted to United States dollars using an exchange rate of 1.10 US$/EUR, resulting in an equivalent logistics cost of approximately US$17.45/wmt concentrate. The resulting transportation and sales costs represent approximately US$287 million over the LOM.

21.2.2.3 Unit Operating Costs

At the LOM processing throughput of approximately 23.4 Mt, the Project’s operating cost structure is summarised in Table 21-12.

Mining, processing, and off-site concentrate treatment costs represent the principal operating cost drivers and therefore have the greatest influence on Project economics.

The Project's operating cost structure is dominated by mining and processing activities, which together account for approximately 79% of total unit operating costs.

Additional costs are associated with water and mine waste treatment, paste backfill, and G&A costs required to support production. The resulting LOM operating cost is estimated at US$86.48/t ore processed.

Table 21-12: Life-of-Mine Unit Operating Costs (Year 1 – Year 21)

Cost Category	Cost (US$/t Ore Processed)
Mining Operating Costs	37.61
Processing Costs	30.20
Contact Water Treatment	3.52
Capital Recovery Charge for Water Treatment Plant	6.06
Mine waste / ATEM	0.15
Tailings / IPS	0.53
Paste Backfill	5.24
G&A	2.97
Progressive rehabilitation	0.22
Total Operating Costs	**86.49**

22.0 Economic Analysis

22.1 Forward-Looking Information

The economic analysis presented in this Technical Report has been prepared at a PFS level and is based on the technical, operating, cost, and commercial assumptions developed for the Project as of the effective date of the Report. The analysis is intended to evaluate the economic performance of the PFS development case and should be considered in the context of the level of engineering definition, estimating accuracy, and uncertainty associated with this stage of Project development.

The financial model incorporates assumptions relating to the mine plan and production schedule, processing rates and metallurgical performance, commodity prices and exchange rates, capital and operating costs, sustaining and closure expenditures, royalties and taxation, working capital, and other commercial parameters applicable to the Project. These inputs are estimates of future conditions and performance and are therefore subject to change as additional technical work is completed and the Project definition advances.

Actual Project outcomes may differ from those estimated in the PFS as a result of changes in technical performance, Project scope and schedule, market conditions, capital and operating costs, commodity prices, exchange rates, fiscal or regulatory requirements, and other factors affecting the development and operation of the Project. Changes in these assumptions may have a material effect on the cash flows and economic indicators presented in this section.

22.2 Financial Model Parameters

22.2.1 Assumptions

The economic analysis was developed using an annual, unlevered cash flow model based on the mine production schedule, process design criteria, capital and operating cost estimates, and commercial assumptions developed for the PFS. The principal financial model parameters are as follows:

- Model basis: annual, unlevered project cash flow, excluding financing costs and the effects of any future debt or equity financing structure.
- Project timeline: the Project schedule is expressed relative to the commencement of operations rather than by calendar year (Table 22-1).

Table 22-1: Project Timeline

Project Phase	Project Period					
	-5	-4	-3	-2	-1	1–21
Mine development	■	■	■	■	■	
Construction			■	■	■	
First ore mined					■	
Ore Processed						■

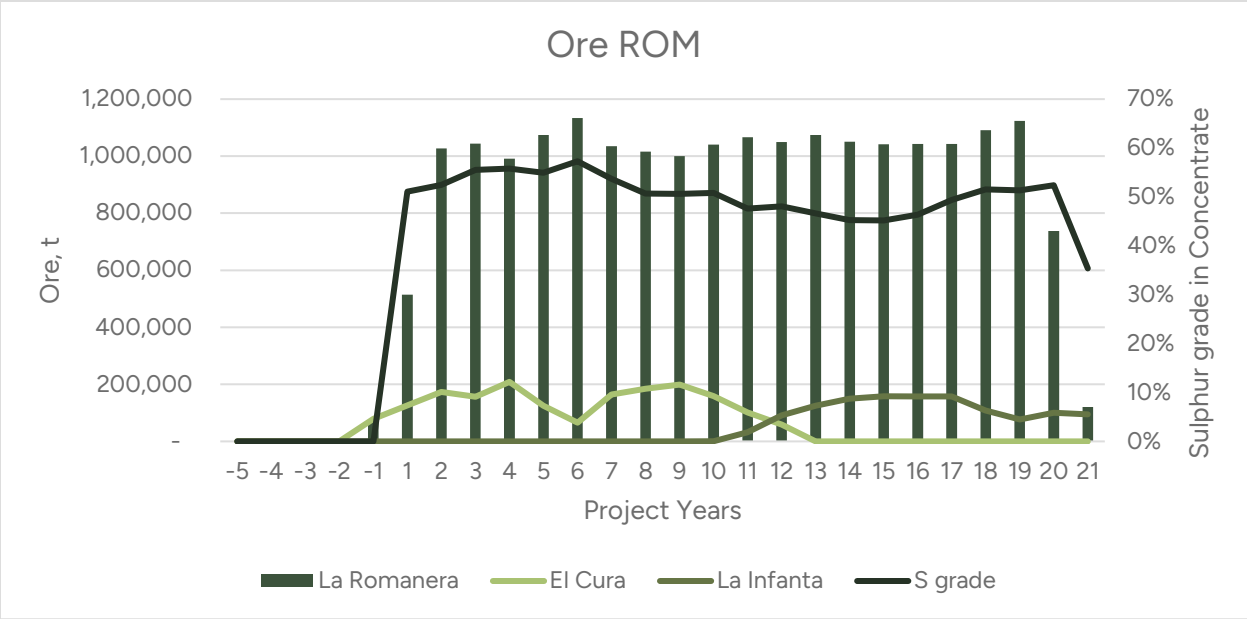
- Cost base: Q2 2026.
- Currency: constant United States dollars (US$), with no inflation or escalation being considered.
- Foreign exchange: EUR/USD = 1.10.
- Discounting convention: all cash flows discounted to start of mine development period (Year -5).
- Discount rate: 8% real.
- Ownership basis: 100% Project ownership basis.
- Plant throughput: 1,200 ktpa.
- Revenue derived from copper, lead, zinc, and pyrite concentrates.
- Working capital: based on 30 days accounts receivable, 45 days inventory, and 30 days accounts payable.
- Spanish taxation includes a 25% Corporate Income Tax rate, 3% municipal tax, and applicable mining tax provisions (see 22.2.5 for more details)
- Royalties: No general production-based mineral royalty is understood to be applicable under Spanish mining legislation.

Detailed assumptions relating to commodity prices, concentrate terms, operating costs, capital costs, taxation, closure costs, and working capital are discussed in the corresponding sections of this chapter.

22.2.2 Production

The financial model is based on the LOM production schedule comprising ore feed from the La Romanera, El Cura, and La Infanta deposits. La Romanera is the principal source of plant feed, with production from El Cura and La Infanta supplementing the feed over the LOM. Stockpiled ore is reclaimed where required to balance mine production and maintain the scheduled plant throughput. A summary of the production schedule over the mine life is presented in Figure 22-1.

Figure 22-1: LOM Ore Feed Production by Deposit and Sulphur Grade



The process plant design and metallurgical performance assumptions are principally based on the La Romanera metallurgical testwork. For the financial model, the process mass balance has been recalculated using the updated LOM production schedule and the resulting blended plant-feed tonnages and head grades from the three deposits. The resulting recoveries, concentrate grades, and concentrate production form the basis of the payable metal and revenue calculations. Further metallurgical testwork on the blended ore feeds is planned at the next stage of project development to confirm these assumptions.

The financial model forecasts production of four saleable concentrates: copper, lead, zinc, and pyrite concentrates. Table 22-2 summarises the principal production assumptions applied in the financial model, including LOM and peak concentrate production, concentrate grades, and metallurgical recoveries. Detailed metallurgical modelling and the process mass balance are presented in Section 17.0.

Table 22-2: Summary of Concentrate Production, Grades, and Metallurgical Recoveries

Concentrate	Average Annual Tonnage, dmt Yr 2 - Yr 19	LOM, dmt	LOM, wmt	Concentrate Grade	Recoveries of Primary Commodity to Concentrate (%)
Zinc concentrate	43,489	845,652	919,187	50.1% Zn	79%
Lead concentrate	26,120	514,778	559,541	26.76% Pb	52%
Copper concentrate	10,633	213,080	234,153	20.43% Cu	41%
Pyrite concentrate	694,620	13,573,653	14,753,970	50.67% S	87%
Concentrates Produced	**774,863**	**15,147,162**	**16,466,852**		

22.2.3 Commodity Prices

Pyrite concentrate pricing is based on the Project-specific market study. The Project is expected to produce a pyrite concentrate containing more than 48% sulphur, which is considered a premium-grade product in the target market. Accordingly, the financial model applies the pricing developed in the market study for this product specification, with a Consensus (Base Case) price of US$274/t. The basis for the pyrite concentrate pricing and alternative market scenarios are discussed in Section 19, and the summary of the long-term prices applied in the economic analysis is shown in Table 22-3.

Table 22-3: Long-Term Pyrite Concentrate Price Assumptions

Pyrite Concentrate Price	US$/t
Consensus (Base Case Long-Term)	**274**
Oversupply / Conservative	217
Extended ME Conflict	348
Reserves	215

The Base Case metal price assumptions for copper, zinc, and gold are based on the long-term consensus forecasts available as of September 2026. The supporting price assumptions for lead and silver are based on internal forecasts informed by available market information.

Long-term Consensus prices represent the average of broker estimates compiled for the respective forecast periods.

Table 22-4 provides long-term price assumptions used in the economic analysis.

Table 22-4: Long-Term Metal Price Assumptions

Long term Metal Prices	Mineral Reserves	Mineral Resources	Consensus (Base Case Long Term)	Sept. Av. Spot
Copper Price (US$/t)	12,120	13,775	11,470	14,483
Copper Price (US$/lb)	5.5	6.2	5.2	6.6
Lead Price (US$/t)	2,200	2,425	2,050	1,871
Lead Price (US$/lb)	1.0	1.1	0.9	0.8
Zinc Price (US$/t)	2,975	3,415	2,980	4,020
Zinc Price (US$/lb)	1.3	1.5	1.4	1.8
Gold Price (US$/oz)	3,000	3,500	**3,750**	4,322
Silver Price (US$/oz)	55	65	**52**	65

22.2.4 Concentrate Payabilities

Revenue from the copper, lead, and zinc concentrates is calculated from the contained payable metals, applying the respective metal payabilities and applicable treatment and refining charges. The financial model also incorporates applicable concentrate transport and other selling costs and, where relevant, penalties associated with concentrate quality.

The payability, treatment charge, refining charge, and other commercial assumptions applied in the financial model are based on benchmark market terms and publicly available information for comparable concentrates. No binding offtake agreements have been assumed at this stage of the Project.

Pyrite concentrate revenue is modelled separately using the concentrate price discussed in Section 22.4.1 and Section 19.

A summary of the concentrate payability assumptions applied in the financial model is presented in Table 22-5.

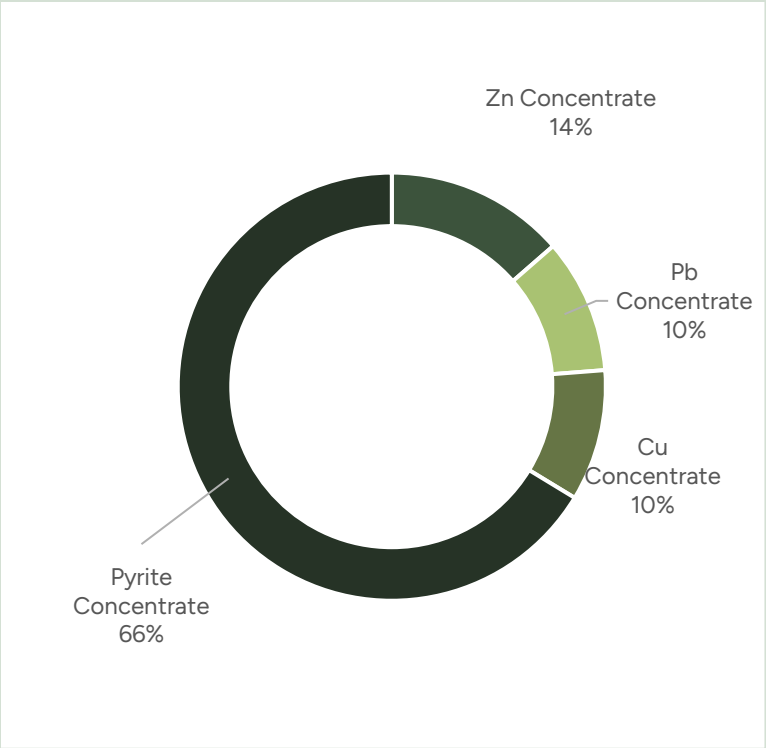
Table 22-5: Summary of Concentrate Payability Assumptions Applied in the Financial Model

Concentrate	Payable Metal	Deduction	Payability
Copper	Cu	1 unit	96.50%
	Ag	Nil	90.00%
	Au	Nil	90.00%[1]
Lead	Pb	3 units	Lesser of (Pb less 3 units) or 95.00% of contained Pb
	Ag	50 g/t	95.00% of remaining Ag
	Au	1 g/t	95.00% of remaining Au
	Cu	Nill	20.00% of contained Cu
Zinc	Zn	8 units[2]	85.00%[2]
	Ag	93.3 g/t[3]	70.00%[3]
	Au	1.0 g/t	70.00%
Pyrite	Au	1 g/t	90.00% of remaining Au
	Ag	25 g/t	90.00% of remaining Ag

Notes:
1. Gold payability in copper concentrate is subject to the applicable grade threshold incorporated in the financial model.
2. Zinc payability is subject to the applicable minimum concentrate-grade threshold.
3. Silver payability in zinc concentrate is subject to the applicable minimum grade and deduction thresholds.

The Project benefits from multiple revenue streams from the production of zinc, lead, copper, and pyrite concentrates, including payable gold and silver contained within the base-metal concentrates. On a LOM basis, pyrite concentrate represents approximately 66% of Project NSR, with zinc, lead, and copper concentrates contributing approximately 14%, 10%, and 10%, respectively, as illustrated in Figure 22-2.

Figure 22-2: Project NSR Contribution by Concentrate Type



22.2.5 Taxation

The financial model applies a Spanish Corporate Income Tax (CIT) rate of 25% and a 3% municipal tax. The model also incorporates applicable mining tax provisions under Articles 90 to 94 of Ley 27/2014, including accelerated depreciation of qualifying mining assets and the depletion allowance. The depletion allowance is applied in determining taxable income prior to the application of the 25% CIT rate.

22.2.6 Capital Cost Summary

Initial capital costs are estimated at US$566.7 million, including mine development, process plant and infrastructure, indirect costs, Owner's costs, and contingency. Capital expenditures are scheduled in accordance with the Project development and construction schedules, with expenditure commencing in Year -5 to reflect the underground mine development required in advance of production. Process plant and associated infrastructure expenditure is concentrated principally over the subsequent construction period.

In addition to initial capital, the financial model includes approximately US$279.5 million of sustaining capital over the LOM and approximately US$12.0 million of post-mining closure costs, resulting in total Project capital expenditure of approximately US$858.2 million.

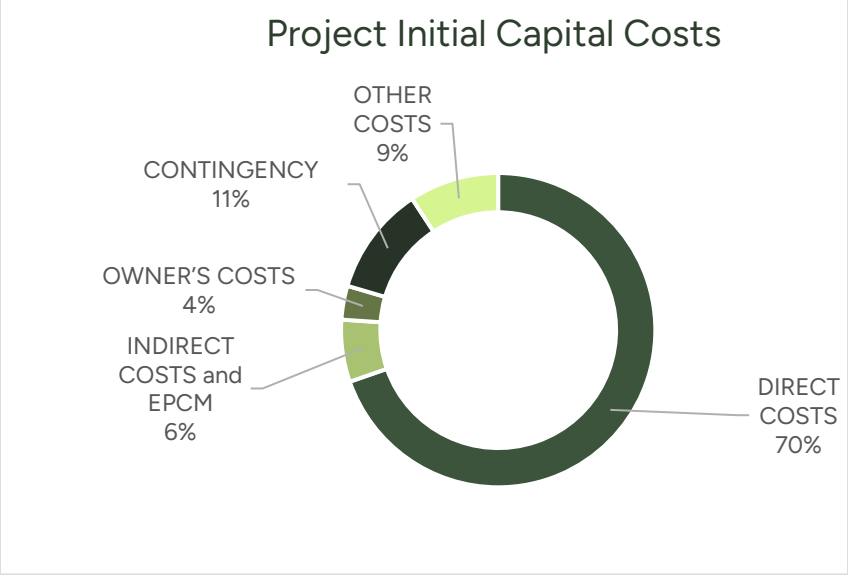
A summary of the LOM capital costs incorporated in the financial model is presented in Table 22-6.

Table 22-6: Life-of-Mine Capital Cost Summary

Category	Cost (US$ million)
Direct Costs	394.7
Indirect Costs and Engineering, Procurement and Construction Management (EPCM)	36.3
Owner's Costs	19.7
Contingency	63.6
Other Costs	52.4
Total Initial Capital Costs	566.7
Sustaining Capital	279.5
Closure Costs (Post-mine activities)	12.0
TOTAL PROJECT CAPITAL	**858.2**
Note: Totals may not sum precisely due to rounding.	

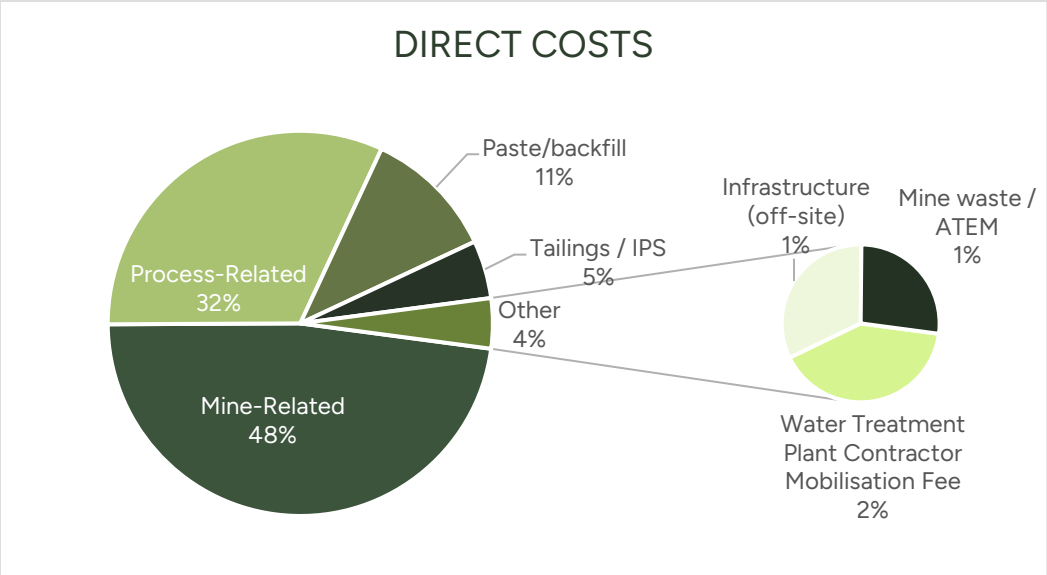
The distribution of initial capital costs is illustrated in Figure 22-3.

Figure 22-3: Project Initial Capital Cost Distribution



Direct costs represent approximately 70% of initial capital. Mine-related costs form the largest component at approximately 48% of direct costs, followed by process-related costs at approximately 32%. The remaining direct capital comprises paste/backfill, tailings and IPS, water treatment, mine waste/ATEM and off-site infrastructure, as illustrated in Figure 22-4. Indirect costs and Engineering, Procurement and Construction Management (EPCM), Owner's costs, contingency, and other costs account for the balance of initial capital.

Figure 22-4: Project Direct Capital Cost Distribution



22.2.7 Operating Cost Summary

LOM on-site operating costs are estimated at approximately US$2.03 billion, comprising mining, processing, G&A, water and waste management, and backfill, and progressive rehabilitation costs. Mining and processing represent the principal on-site operating cost components.

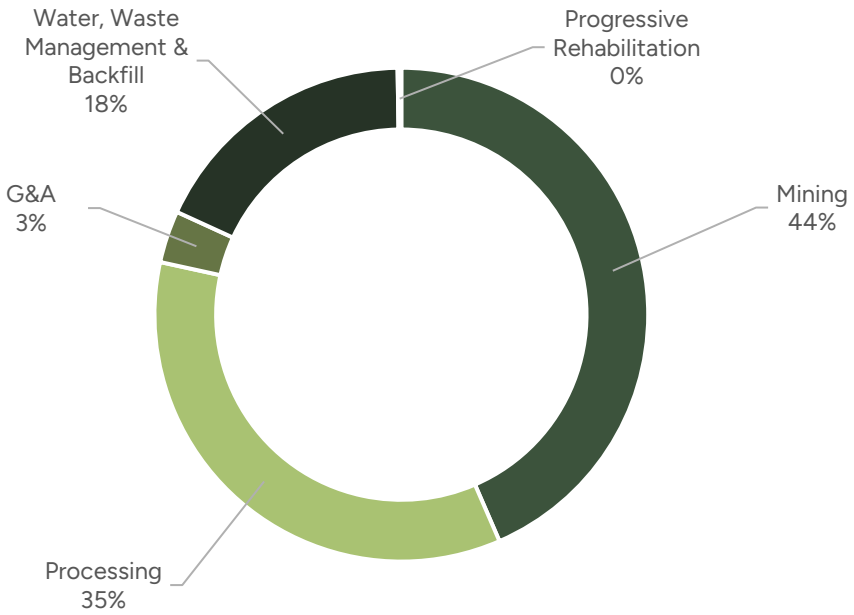
All operating costs incurred prior to the commencement of production are capitalised in the financial model and included within initial capital costs.

A summary of the LOM on-site operating costs incorporated in the financial model is presented in Table 22-7 and Figure 22-5.

Table 22-7: Life-of-Mine On-site Operating Cost Summary

Cost Category	US$ million
Mining	882
Processing	708
G&A	70
Water and Waste Management and Backfill	363
Progressive Rehabilitation	5
Onsite Operating Costs	**2,028**

Figure 22-5: LOM On-site Operating and Off-site Commercial Costs Split



In addition, the financial model incorporates approximately US$886 million of off-site and commercial costs associated with treatment and refining charges (TC/RC), concentrate penalties, and transportation and sales (Table 22-8). These costs are deducted in determining Project NSR.

Table 22-8: Life-of-Mine Off-site and Commercial Cost Summary

Off-site Commercial Cost Category	Cost (US$ million)
TC/RC	92
Penalties	506
Transportation and Sales	287
Offsite and Commercial Costs	**886**

22.3 Cash Flow Analysis

The Project cash flow model has been developed on an annual basis over the LOM using the production, revenue, operating cost, capital cost, and taxation assumptions described above. The economic analysis is presented on an unlevered, real, after-tax basis, with the valuation date corresponding to the commencement of Project development in Year -5.

At the Base Case commodity price assumptions, the Project generates an after-tax NPV of approximately US$776 million at an 8% real discount rate and an after-tax internal rate of return (IRR) of 23.51%. The corresponding payback period is approximately 6 years and 11 months from the commencement of Project development, equivalent to approximately 1 years and 11 months following the commencement of production.

Initial capital expenditure is estimated at approximately US$567 million.

At an 8% discount rate, the Project has a Profitability Index (PI) of 2.37.

Table 22-9 summarises the principal Base Case economic results, while Table 22-10 and Figure 22-6 illustrate the annual and cumulative after-tax cash flow profile over the LOM.

Table 22-9: Summary of Base Case Economic Results

Cash Flow Waterfall	Cost (US$ million)
Gross Payable Revenue	7,473
Mining	(882)
Processing	(708)
G&A	(70)
Water, Waste Management & Backfill	(363)
Progressive Rehabilitation	(5)
TC/RC	(92)
Penalties	(506)
Transportation and Sales	(287)
Earnings Before Interest, Taxes, Depreciation, and Amortisation **(EBITDA)**	4,559
Tax	(1,037)
Project Capital Costs	(858)
Including Initial Capex	(567)
Post-Tax-Free Cash Flow	2,664
Payback Period from Initial Investment	6 years, 11 Months
Payback Period from Production Commencement	1 years, 11 Months
NPV (real, after-tax) @8%	776
IRR (real, after-tax)	23.51%
Profitability Index (PI)	2.37
NPV/Initial Capex Ratio	1.37

Figure 22-6: Project Post-Tax-Free Cash Flow and Cumulative Cash Flow

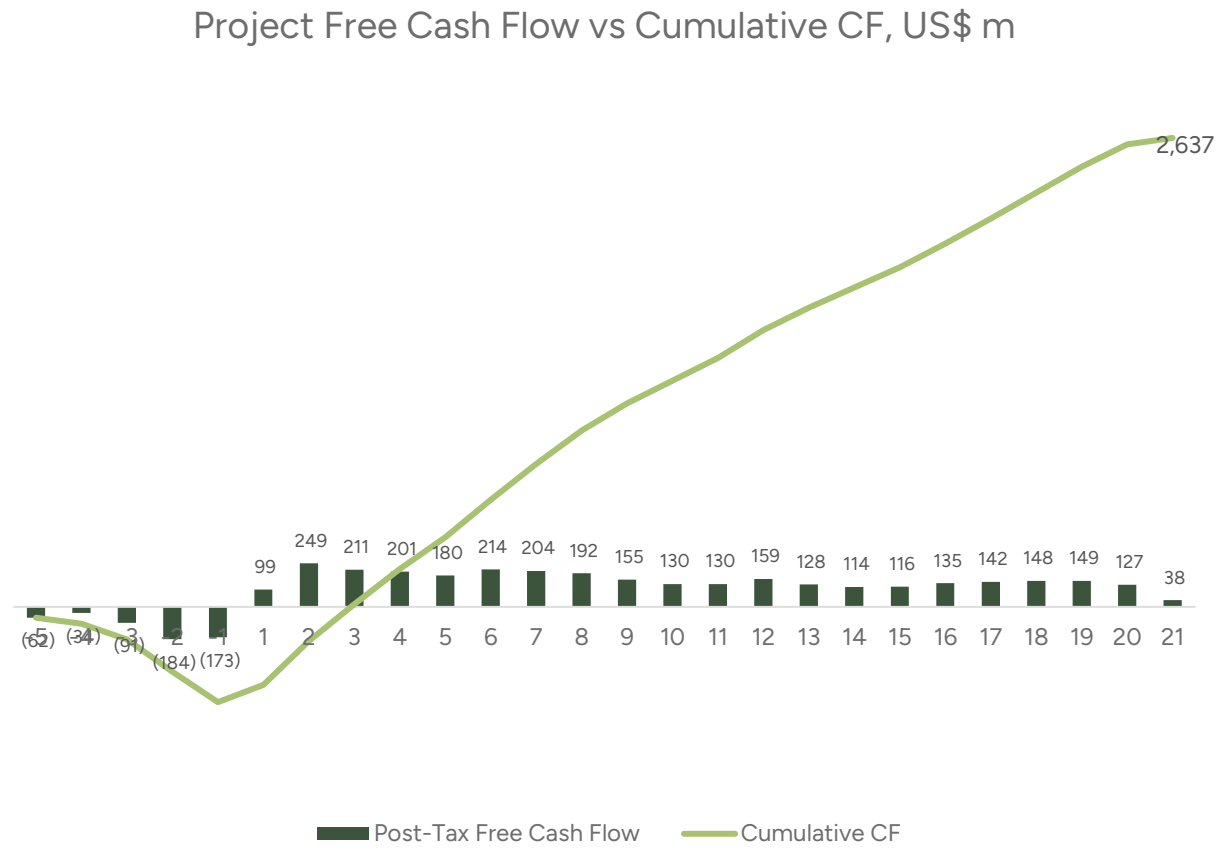


Table 22-10: After-Tax Cash Flow Summary

Cash Flow Summary	Units	Total LOM	-5	-4	-3	-2	-1	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24
Gross Payable Revenue	US$ M	7,473	-	-	-	-	-	274	431	426	465	430	474	448	419	373	353	332	378	319	308	323	337	354	355	339	270	66	-	-	-
Total Opex	US$ M	(2,028)	-	-	-	-	-	(71)	(100)	(100)	(98)	(100)	(102)	(105)	(104)	(105)	(103)	(108)	(106)	(105)	(101)	(99)	(101)	(105)	(107)	(102)	(75)	(31)	-	-	-
Off-site costs	US$ M	(886)	-	-	-	-	-	(31)	(50)	(50)	(54)	(46)	(45)	(47)	(45)	(42)	(41)	(40)	(43)	(40)	(40)	(44)	(47)	(49)	(49)	(40)	(33)	(11)	-	-	-
EBITDA	US$ M	4,559	-	-	-	-	-	172	281	276	313	284	327	297	270	226	209	184	229	174	166	180	189	200	199	197	162	24	-	-	-
Initial Capex	US$ M	(567)	(62)	(34)	(90)	(184)	(173)	(24)	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Sustaining Capex	US$ M	(280)	(0.04)	(0.04)	(0.04)	(0.06)	(0.09)	(27.70)	(20.77)	(20.93)	(23.13)	(29.20)	(19.54)	(13.95)	(8.22)	(14.62)	(25.83)	(8.73)	(6.92)	(8.91)	(12.87)	(18.53)	(6.58)	(7.02)	(2.38)	(1.23)	(1.23)	(0.95)	-	-	-
Closure	US$ M	(12)	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	(1.20)	(3.00)	(6.00)	(1.80)
Working Capital Movements	US$ M	(0)	-	-	-	-	-	(21.29)	(11.37)	0.42	(3.10)	2.31	(3.94)	2.06	2.54	3.64	1.52	1.60	(3.58)	4.67	1.08	(0.94)	(0.78)	(1.31)	(0.39)	0.62	5.74	20.52	-	-	-
Tax	US$ M	(1,037)	-	-	-	-	-	-	-	(44.27)	(86.23)	(77.64)	(89.17)	(80.44)	(72.91)	(60.14)	(54.75)	(47.17)	(59.03)	(42.58)	(41.02)	(44.35)	(46.45)	(49.08)	(48.71)	(47.93)	(40.10)	(4.81)	-	-	-
Unlevered Post-Tax-Free Cash Flow	**US$ M**	2,664	(62)	(34)	(91)	(184)	(173)	99	249	211	201	180	214	204	192	155	130	130	159	128	114	116	135	142	148	149	127	38	(3)	(6)	(2)

Production Summary	Units	Total LOM	-5	-4	-3	-2	-1	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24
Total Ore Mined	t'000	23,448	-	-	-	-	155	641	1,200	1,200	1,200	1,200	1,200	1,200	1,200	1,200	1,200	1,200	1,200	1,200	1,200	1,200	1,200	1,200	1,200	1,200	837	215	-	-	-
ROMANERA TONNES	t'000	20,394	-	-	-	-	76	515	1,027	1,044	991	1,075	1,134	1,035	1,016	1,000	1,041	1,066	1,050	1,074	1,050	1,042	1,043	1,043	1,092	1,124	737	120	-	-	-
El Cura	t'000	1,802	-	-	-	-	79	127	173	156	209	125	66	165	184	200	159	102	59	-	-	-	-	-	-	-	-	-	-	-	-
Infanta	t'000	1,251	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0	32	91	126	150	158	157	157	108	76	100	95	-	-	-
Total Ore Feed to Flotation	t'000	23,448	-	-	-	-	-	797	1,200	1,200	1,200	1,200	1,200	1,200	1,200	1,200	1,200	1,200	1,200	1,200	1,200	1,200	1,200	1,200	1,200	1,200	837	215	-	-	-
Grades Processed																															
Zn		50	-	-	-	-	1.22	1.97	2.83	2.99	3.34	2.33	2.68	2.90	2.39	1.90	1.82	1.71	1.96	1.70	1.53	1.77	2.55	2.86	2.60	1.70	2.33	2.78	-	-	-
Cu		11	-	-	-	-	0.71	0.56	0.50	0.46	0.53	0.45	0.33	0.33	0.39	0.40	0.42	0.40	0.41	0.40	0.45	0.53	0.46	0.47	0.51	0.42	0.49	0.89	-	-	-
Pb		25	-	-	-	-	0.88	1.26	1.39	1.22	1.34	1.12	1.22	1.27	1.07	0.97	0.90	0.86	1.09	0.97	0.89	1.01	1.25	1.35	1.28	0.88	1.19	1.61	-	-	-
Au		23	-	-	-	-	1.07	1.27	1.19	1.22	1.46	1.48	1.83	1.51	1.17	0.98	0.94	0.85	1.04	0.79	0.71	0.76	0.68	0.74	0.87	1.02	1.09	0.56	-	-	-
Ag		1,169	-	-	-	-	55.45	63.10	65.06	59.95	59.89	53.11	54.34	58.39	69.80	61.75	53.44	49.06	58.46	45.29	42.23	43.82	44.75	49.85	43.93	40.92	52.96	43.41	-	-	-
S		735	-	-	-	-	31.91	34.66	35.05	37.10	37.26	36.72	38.28	35.88	33.88	33.84	33.94	31.80	32.12	31.16	30.24	30.20	30.98	32.97	34.45	34.29	35.01	23.65	-	-	-
Contained Metal Processed																															
Zn	t	538,653	-	-	-	-	1,898	12,652	33,982	35,930	40,100	27,944	32,211	34,811	28,667	22,740	21,793	20,474	23,480	20,391	18,397	21,213	30,598	34,309	31,208	20,373	19,500	5,983	-	-	-
Cu	t	104,949	-	-	-	-	1,100	3,568	5,986	5,534	6,362	5,348	4,001	3,964	4,700	4,754	5,038	4,806	4,927	4,771	5,366	6,383	5,567	5,619	6,145	4,998	4,098	1,915	-	-	-
Pb	t	263,939	-	-	-	-	1,361	8,101	16,715	14,636	16,120	13,499	14,648	15,242	12,892	11,662	10,832	10,325	13,057	11,584	10,677	12,089	15,055	16,205	15,310	10,522	9,943	3,468	-	-	-
Au	kg	25,092	-	-	-	-	166	812	1,432	1,467	1,751	1,779	2,192	1,812	1,402	1,172	1,124	1,020	1,249	945	854	912	818	889	1,045	1,221	909	120	-	-	-
Ag	kg	1,247,552	-	-	-	-	8,617	40,479	78,073	71,938	71,862	63,726	65,202	70,058	83,751	74,091	64,122	58,861	70,147	54,345	50,678	52,573	53,699	59,826	52,721	49,100	44,350	9,333	-	-	-
S	t	7,937,589	-	-	-	-	49,587	222,361	420,605	445,139	447,076	440,638	459,289	430,564	406,516	406,039	407,215	381,613	385,410	373,863	362,931	362,382	371,699	395,656	413,443	411,529	293,188	50,846	-	-	-

Concentrate Production and NSR	Units	Total LOM	-5	-4	-3	-2	-1	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21
Concentrates Produced dmt	**dmt**	**15,147,162**	**-**	**-**	**-**	**-**	**-**	**512,076**	**792,718**	**790,808**	**801,939**	**775,677**	**781,857**	**787,026**	**774,284**	**762,715**	**760,177**	**756,630**	**766,928**	**758,901**	**755,254**	**764,437**	**783,334**	**791,538**	**785,990**	**757,313**	**543,066**	**144,493**
Zinc concentrate	dmt	845,652	-	-	-	-	-	22,844	53,350	56,408	62,954	43,870	50,570	54,650	45,006	35,700	34,213	32,142	36,862	32,013	28,882	33,303	48,036	53,863	48,994	31,984	30,614	9,393
Lead concentrate	dmt	514,778	-	-	-	-	-	18,453	32,599	28,546	31,440	26,328	28,569	29,727	25,144	22,744	21,126	20,137	25,467	22,593	20,824	23,577	29,363	31,605	29,859	20,521	19,392	6,763
Copper concentrate	dmt	213,080	-	-	-	-	-	9,477	12,153	11,236	12,917	10,857	8,123	8,049	9,542	9,652	10,229	9,757	10,003	9,687	10,895	12,959	11,303	11,409	12,476	10,147	8,321	3,889
Pyrite concentrate	dmt	13,573,653	-	-	-	-	-	461,302	694,616	694,618	694,629	694,621	694,596	694,600	694,592	694,619	694,608	694,594	694,596	694,608	694,654	694,597	694,631	694,661	694,661	694,661	484,738	124,448
Concentrates Shipped wmt	**wmt**	**16,466,852**	**-**	**-**	**-**	**-**	**-**	**556,718**	**861,795**	**859,709**	**871,827**	**843,257**	**849,942**	**855,559**	**841,727**	**829,154**	**826,401**	**822,541**	**833,737**	**825,008**	**821,059**	**831,064**	**851,585**	**860,504**	**854,486**	**823,287**	**590,388**	**157,104**
Zinc concentrate	wmt	919,187	-	-	-	-	-	24,830	57,989	61,313	68,428	47,685	54,967	59,403	48,919	38,804	37,188	34,937	40,068	34,797	31,393	36,199	52,213	58,547	53,255	34,765	33,277	10,210
Lead concentrate	wmt	559,541	-	-	-	-	-	20,058	35,434	31,029	34,174	28,618	31,053	32,311	27,331	24,722	22,963	21,888	27,681	24,557	22,635	25,628	31,916	34,353	32,456	22,305	21,079	7,352
Copper concentrate	wmt	234,153	-	-	-	-	-	10,414	13,355	12,347	14,194	11,931	8,926	8,845	10,486	10,606	11,241	10,722	10,992	10,645	11,972	14,241	12,421	12,537	13,709	11,150	9,144	4,273
Pyrite concentrate	wmt	14,753,970	-	-	-	-	-	501,416	755,017	755,020	755,031	755,023	754,995	755,001	754,991	755,021	755,009	754,993	754,996	755,009	755,058	754,997	755,034	755,066	755,066	755,067	526,889	135,269
Total Payable for Concentrates	**US$ M**	**7,473**	**-**	**-**	**-**	**-**	**-**	**274**	**431**	**426**	**465**	**430**	**474**	**448**	**419**	**373**	**353**	**274**	**431**	**426**	**465**	**430**	**474**	**448**	**419**	**373**	**353**	**274**
Total Payable for Zinc Concentrate	US$ M	1,145	-	-	-	-	-	34	71	74	82	61	69	73	63	51	48	45	52	44	40	45	62	70	63	44	41	12
Total Payable for Lead Concentrate	US$ M	739	-	-	-	-	-	28	46	42	45	40	44	44	45	39	35	32	39	31	29	31	33	36	34	30	27	6
Total Payable for Copper Concentrate	US$ M	852	-	-	-	-	-	36	50	47	52	46	42	41	45	42	41	39	43	37	39	44	40	42	44	38	32	11
Total Payable for Pyrite Concentrate	US$ M	4,737	-	-	-	-	-	176	264	263	287	283	319	290	266	239	228	216	243	206	200	202	202	206	214	226	170	36
Off-Site Costs	**US$ M**	(886)	-	-	-	-	-	(31)	(50)	(50)	(54)	(46)	(45)	(47)	(45)	(42)	(41)	(40)	(43)	(40)	(40)	(44)	(47)	(49)	(49)	(40)	(33)	(11)
Total Smelter Deductions	US$ M	(92)	-	-	-	-	-	(3)	(6)	(6)	(7)	(5)	(5)	(6)	(5)	(4)	(4)	(4)	(4)	(4)	(3)	(4)	(5)	(6)	(5)	(4)	(3)	(1)
Total Penalties	US$ M	(506)	-	-	-	-	-	(18)	(30)	(29)	(32)	(26)	(25)	(26)	(25)	(23)	(23)	(22)	(24)	(22)	(23)	(25)	(27)	(29)	(29)	(22)	(19)	(7)
Total Transport Costs	US$ M	(287)	-	-	-	-	-	(10)	(15)	(15)	(15)	(15)	(15)	(15)	(15)	(14)	(14)	(14)	(15)	(14)	(14)	(14)	(15)	(15)	(15)	(14)	(10)	(3)
Total NSR	**US$ M**	6,587	-	-	-	-	-	243	381	376	411	384	428	402	374	331	312	292	335	279	268	279	290	305	306	299	237	55
Zn Concentrate	US$ M	895	-	-	-	-	-	27	56	57	63	48	54	57	50	41	38	36	41	35	31	35	48	54	49	35	32	9
Pb Concentrate	US$ M	670	-	-	-	-	-	26	41	38	41	37	40	40	41	36	32	30	36	28	26	28	29	32	30	28	24	6
Cu Concentrate	US$ M	654	-	-	-	-	-	27	39	36	40	36	34	33	36	34	32	30	33	28	29	32	30	32	32	29	24	8
Pyrite Concentrate	US$ M	4,368	-	-	-	-	-	163	245	244	268	264	300	271	247	221	210	197	224	188	181	184	183	187	195	207	156	33

Operating Costs Summary	Units	Total LOM	-5	-4	-3	-2	-1	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21
Mining	US$ M	(882)	-	-	-	-	-	(34)	(41)	(41)	(41)	(42)	(45)	(48)	(45)	(46)	(45)	(48)	(47)	(47)	(43)	(41)	(42)	(45)	(48)	(45)	(33)	(15)
Processing	US$ M	(708)	-	-	-	-	-	(24)	(36)	(36)	(36)	(36)	(36)	(36)	(36)	(36)	(36)	(36)	(36)	(36)	(36)	(36)	(36)	(36)	(36)	(36)	(25)	(6)
G&A	US$ M	(70)	-	-	-	-	-	(2)	(4)	(4)	(4)	(4)	(4)	(4)	(4)	(4)	(4)	(4)	(4)	(4)	(4)	(4)	(4)	(4)	(4)	(4)	(2)	(1)
Water, Waste Management & Backfill	US$ M	(363)	-	-	-	-	-	(11)	(20)	(20)	(18)	(18)	(17)	(17)	(19)	(19)	(18)	(20)	(19)	(18)	(18)	(18)	(19)	(19)	(18)	(16)	(14)	(9)
Progressive Rehabilitation	US$ M	(5)	-	-	-	-	-	-	-	-	-	-	(0)	(0)	(0)	(0)	(0)	(0)	(0)	(0)	(0)	(0)	(1)	(1)	(1)	(1)	(1)	-
Royalty (MET)	US$ M	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Total On-Site Costs	US$ M	**(2,028)**	**-**	**-**	**-**	**-**	**-**	**(71)**	**(100)**	**(100)**	**(98)**	**(100)**	**(102)**	**(105)**	**(104)**	**(105)**	**(103)**	**(108)**	**(106)**	**(105)**	**(101)**	**(99)**	**(101)**	**(105)**	**(107)**	**(102)**	**(75)**	**(31)**
TC/RC	US$ M	(92)	-	-	-	-	-	(3)	(6)	(6)	(7)	(5)	(5)	(6)	(5)	(4)	(4)	(4)	(4)	(4)	(3)	(4)	(5)	(6)	(5)	(4)	(3)	(1)
Penalties	US$ M	(506)	-	-	-	-	-	(18)	(30)	(29)	(32)	(26)	(25)	(26)	(25)	(23)	(23)	(22)	(24)	(22)	(23)	(25)	(27)	(29)	(29)	(22)	(19)	(7)
Transportation and Sales	US$ M	(287)	-	-	-	-	-	(10)	(15)	(15)	(15)	(15)	(15)	(15)	(15)	(14)	(14)	(14)	(15)	(14)	(14)	(14)	(15)	(15)	(15)	(14)	(10)	(3)
Total Off-site Costs	US$ M	(886)	-	-	-	-	-	(31)	(50)	(50)	(54)	(46)	(45)	(47)	(45)	(42)	(41)	(40)	(43)	(40)	(40)	(44)	(47)	(49)	(49)	(40)	(33)	(11)
Total Operating Costs (On-site and Off-site)	**US$ M**	**(2,914)**	**-**	**-**	**-**	**-**	**-**	**(102)**	**(151)**	**(150)**	**(152)**	**(146)**	**(147)**	**(152)**	**(149)**	**(147)**	**(144)**	**(148)**	**(149)**	**(145)**	**(141)**	**(143)**	**(149)**	**(155)**	**(155)**	**(142)**	**(107)**	**(41)**

Capital Costs	Units	Total LOM	-5	-4	-3	-2	-1	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24
DIRECT COSTS	**US$ M**	**394.7**	**46.1**	**22.7**	**64.6**	**132.8**	**111.9**	**16.7**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**
Mine-Related	US$ M	189.1	45.8	22.2	34.0	50.1	36.9	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Process-Related	US$ M	126.6	-	-	19.0	50.6	50.6	6.3	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Mine waste / ATEM	US$ M	4.5	-	-	0.7	1.6	1.6	0.7	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Tailings / IPS	US$ M	19.3	-	-	2.9	6.7	6.7	2.9	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Paste/backfill	US$ M	43.8	-	-	6.6	15.3	15.3	6.6	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
WTP Contractor Advanced Mobilisation Fee	US$ M	6.8	-	-	-	6.8	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Off-Site Infrastructure	US$ M	4.7	0.2	0.5	1.4	1.6	0.7	0.2	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
INDIRECT COSTS and EPCM	**US$ M**	**36.3**	**-**	**-**	**5.4**	**14.0**	**14.0**	**2.8**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**
OWNER'S COSTS	**US$ M**	**19.7**	**2.3**	**1.1**	**3.2**	**6.6**	**5.6**	**0.8**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**
CONTINGENCY	**US$ M**	**63.6**	**6.9**	**3.4**	**10.5**	**21.0**	**18.9**	**2.9**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**
OTHER COSTS	**US$ M**	**52.4**	**6.6**	**6.7**	**6.7**	**9.6**	**22.5**	**0.3**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**
TOTAL INITIAL CAPITAL COSTS	**US$ M**	**566.7**	**61.9**	**33.9**	**90.5**	**184.0**	**172.8**	**23.6**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**
SUSTAINING CAPITAL	**US$ M**	**279.5**	**0.0**	**0.0**	**0.0**	**0.1**	**0.1**	**27.7**	**20.8**	**20.9**	**23.1**	**29.2**	**19.5**	**13.9**	**8.2**	**14.6**	**25.8**	**8.7**	**6.9**	**8.9**	**12.9**	**18.5**	**6.6**	**7.0**	**2.4**	**1.2**	**1.2**	**0.9**	**-**	**-**	**-**
Closure	**US$ M**	**12.0**	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	1.2	3.0	6.0	1.8
Total LOM Capex	**US$ M**	**858.2**	**61.9**	**33.9**	**90.5**	**184.1**	**172.9**	**51.3**	**20.8**	**20.9**	**23.1**	**29.2**	**19.5**	**13.9**	**8.2**	**14.6**	**25.8**	**8.7**	**6.9**	**8.9**	**12.9**	**18.5**	**6.6**	**7.0**	**2.4**	**1.2**	**1.2**	**2.1**	**3.0**	**6.0**	**1.8**

22.4 Sensitivity Analysis

Project risks and opportunities can be identified in both economic and non-economic terms. Key economic risks and opportunities were examined by running cash flow sensitivities: commodity prices, on-site and off-site operating costs, and initial capital costs.

22.4.1 Commodity Price Sensitivity Analysis

The Project generates revenue from four saleable concentrates, with pyrite concentrate representing the largest contribution to LOM NSR. The sensitivity analysis has been structured to separately assess the impact of pyrite concentrate pricing and metal price assumptions on Project economics.

Pyrite concentrate price sensitivity is assessed using the pricing scenarios developed in the market study, comprising the Consensus, Oversupply/Conservative, and Extended Middle East Conflict cases. For each pyrite pricing scenario, the metal price deck for copper, lead, zinc, gold, and silver is held constant at the Consensus (Base Case Long-term Prices) assumptions. This isolates the impact of changes in the pyrite concentrate price on Project economics. The results of this analysis are presented in Table 22-11 and Figure 22-7.

Conversely, metal price sensitivity is assessed using the Reserves, Consensus, and Resources metal price decks. In each case, the pyrite concentrate price is held constant at the Consensus price of US$274/dmt, thereby isolating the effect of changes in the metal price deck. The results of this analysis are presented in Table 22-12 and Figure 22-8.

All other technical and economic assumptions are held constant between the sensitivity cases.

Table 22-11: Project Sensitivity to the Pyrite Concentrate Prices

Parameter	Units	Consensus	Oversupply / Conservative	Extended Middle East Conflict
Concentrate Price	US$/t	274	217	348
Gross Revenue Payable	US$ m	7,473	6,705	8,484
Mining	US$ m	(882)	(882)	(882)
Processing	US$ m	(708)	(708)	(708)
G&A	US$ m	(70)	(70)	(70)
Water, Waste Management & Backfill	US$ m	(363)	(363)	(363)
Progressive Rehabilitation	US$ m	(5)	(5)	(5)
Royalty (MET)	US$ m	-	-	-
TC/RC	US$ m	(92)	(92)	(92)
Penalties	US$ m	(506)	(506)	(506)
Transportation and Sales	US$ m	(287)	(287)	(287)
EBITDA	US$ m	4,559	3,791	5,570
Tax	US$ m	(1,037)	(822)	(1,320)
Capital Costs	US$ m	-	-	-
incl. Initial Capex	US$ m	(858)	(858)	(858)
Post-Tax-Free Cash Flow	US$ m	(567)	(567)	(567)
NPV (real, after-tax) 8%	US$ m	2,664	2,111	3,392
IRR	US$ m	776	580	1,035
PI	x	1.37	1.02	1.83
Payback Period from Initial Investment from Valuation Date	Years	6 years, 11 months	7 years, 4 months	6 years, 6 months
Payback Period from Production Start	Years	1 years, 11 months	2 years, 4 months	1 year, 6 months

Table 22-12: Project Sensitivity to Metal Prices (keeping Pyrite at Consensus Price level)

	Units	Reserves	Emerita Consensus (Base Case)	Sept. Av. Spot
Copper Price	US$/t	12,120	**11,470**	14,483
Lead Price	US$/t	2,200	**2,050**	1,871
Zinc Price	US$/t	2,975	**2,980**	4,020
Gold Price	US$/oz	3,000	**3,750**	4,322
Silver Price	US$/oz	55	**52**	65
Pyrite Concentrate Price	US$/t	*274*	***274***	*274*
Gross Revenue Payable	US$ m	7,412	7,473	8,357
Mining	US$ m	(882)	(882)	(882)
Processing	US$ m	(708)	(708)	(708)
G&A	US$ m	(70)	(70)	(70)
Water, Waste Management & Backfill	US$ m	(363)	(363)	(363)
Progressive Rehabilitation	US$ m	(5)	(5)	(5)
Royalty (MET)	US$ m	-	-	-
TC/RC	US$ m	(92)	(92)	(92)
Penalties	US$ m	(506)	(506)	(506)
Transportation and Sales	US$ m	(287)	(287)	(287)
EBITDA	US$ m	4,498	4,559	5,443
Tax	US$ m	(1,020)	(1,037)	(1,284)
Capital Costs	US$ m	-	-	-
incl. Initial Capex	US$ m	(858)	(858)	(858)
Post-Tax-Free Cash Flow	US$ m	(567)	(567)	(567)
NPV (real, after-tax) 8%	US$ m	2,620	2,664	3,300
IRR	%	752	776	1,019
PI	X	1.33	1.37	1.80
Payback Period from Initial Investment from Valuation Date	Years	6 years, 12 months	**6 years, 11 months**	6 years, 6 months
Payback Period from Production Start	Years	1 year, 12 months	**1 year, 11 months**	1 year, 6 months

Figure 22-7: Pyrite Concentrate Price Impact Analysis - NPV 8% (Post-tax) US$ m

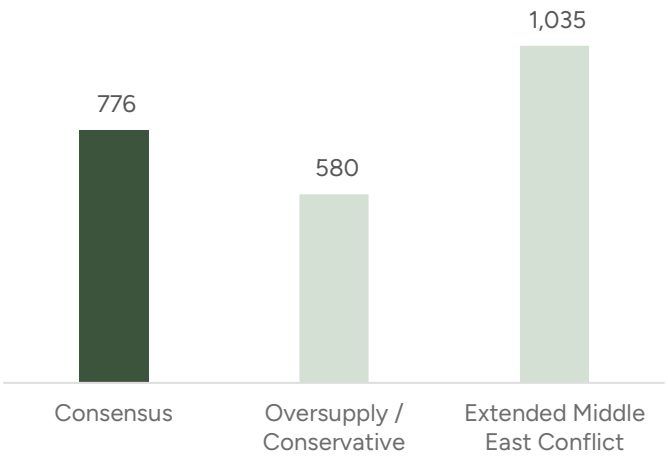
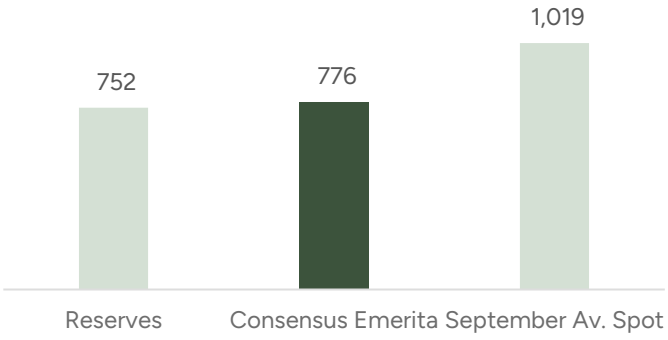


Figure 22-8: Metal Price Sensitivity. Pyrite concentrate Price @ $274/dmt - NPV 8% (Post-tax) US$ m



22.4.2 Project Costs Sensitivity Analysis

Project cost sensitivities were evaluated by varying selected parameters from -30% to +30% in 5% increments, while holding all other technical and economic assumptions constant.

The analysis considers variations in on-site operating costs, off-site operating costs, initial capital costs and pyrite concentrate pricing, with the resulting impacts on after-tax NPV at an 8% real discount rate and IRR presented in Table 22-13, Figure 22-9, and Figure 22-10.

Table 22-13: After-Tax Sensitivity Analyses

Sensitivity Analysis - NPV @ 8% (US$ M)													
Change in Parameter	-30%	-25%	-20%	-15%	-10%	-5%	**0%**	5%	10%	15%	20%	25%	30%
On-site operating costs	933	907	881	855	829	802	**776**	750	724	698	672	646	620
Off-site operating cost	845	834	822	811	799	788	**776**	765	753	742	730	719	707
Initial Capital Cost	886	868	850	832	813	795	**776**	758	740	721	703	685	665
Pyrite Concentrate Price	**491**	**539**	**586**	**634**	**681**	**729**	**776**	**824**	**872**	**919**	**967**	**1,014**	**1,062**
Copper Price	737	743	750	756	763	770	**776**	783	790	796	803	810	816
Lead Price	757	760	763	767	770	773	**776**	780	783	786	790	793	796
Zinc Price	692	706	720	734	748	762	**776**	791	805	819	833	847	861
Gold Price	696	710	723	736	750	763	**776**	790	803	816	830	843	856
Silver Price	687	702	717	732	747	762	**776**	791	806	821	836	851	866
Sensitivity Analysis - Project IRR (%)													
Change in Parameter	-30%	-25%	-20%	-15%	-10%	-5%	**0%**	5%	10%	15%	20%	25%	30%
On-site operating costs	26%	25%	25%	25%	24%	24%	**24%**	23%	23%	22%	22%	22%	21%
Off-site operating cost	25%	24%	24%	24%	24%	24%	**24%**	23%	23%	23%	23%	23%	22%
Initial Capital Cost	30%	29%	28%	26%	25%	24%	**24%**	23%	22%	21%	20%	20%	19%
Pyrite Concentrate Price	**19%**	**20%**	**21%**	**21%**	**22%**	**23%**	**24%**	**24%**	**25%**	**26%**	**26%**	**27%**	**27%**
Copper Price	23%	23%	23%	23%	23%	23%	**24%**	24%	24%	24%	24%	24%	24%
Lead Price	23%	23%	23%	23%	23%	23%	**24%**	24%	24%	24%	24%	24%	24%
Zinc Price	22%	22%	23%	23%	23%	23%	**24%**	24%	24%	24%	24%	25%	25%
Gold Price	22%	22%	23%	23%	23%	23%	**24%**	24%	24%	24%	24%	25%	25%
Silver Price:	22%	22%	23%	23%	23%	23%	**24%**	24%	24%	24%	24%	25%	25%

The sensitivity analysis indicates that Project economics are most sensitive to pyrite concentrate pricing. Variations in pyrite pricing result in a substantially greater impact on NPV than comparable changes in operating costs, capital costs, or off-site costs, reflecting the significant contribution of pyrite concentrate revenue to overall Project cash flow.

The analysis also demonstrates that the Project remains economically viable down to a pyrite concentrate **breakeven** price of approximately **US$52.21/t,** which is significantly below the Base Case assumption of US$274/t.

Figure 22-9: After-Tax Sensitivity Analysis (NPV @8%)

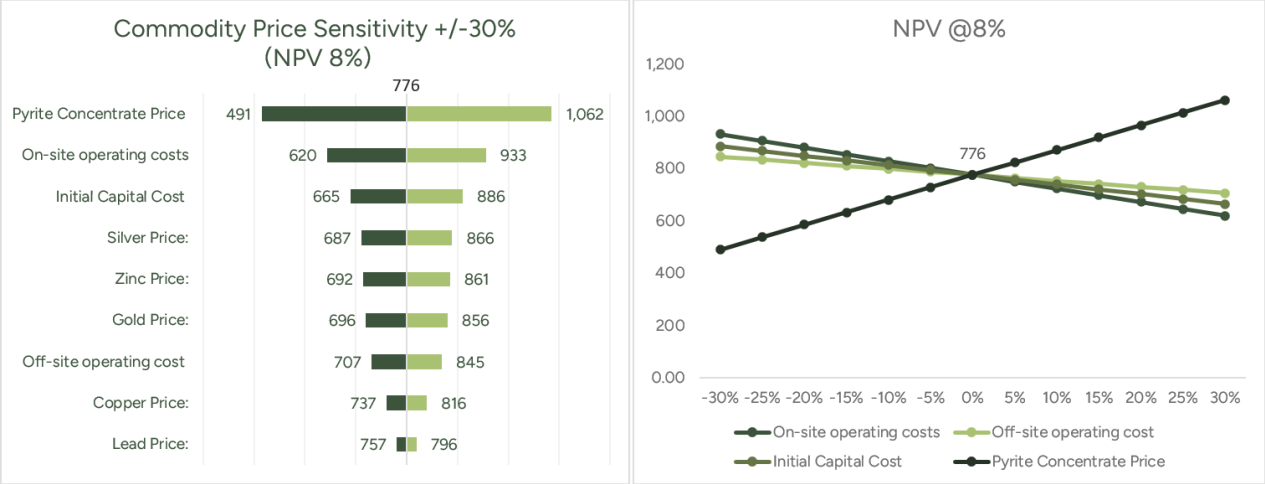
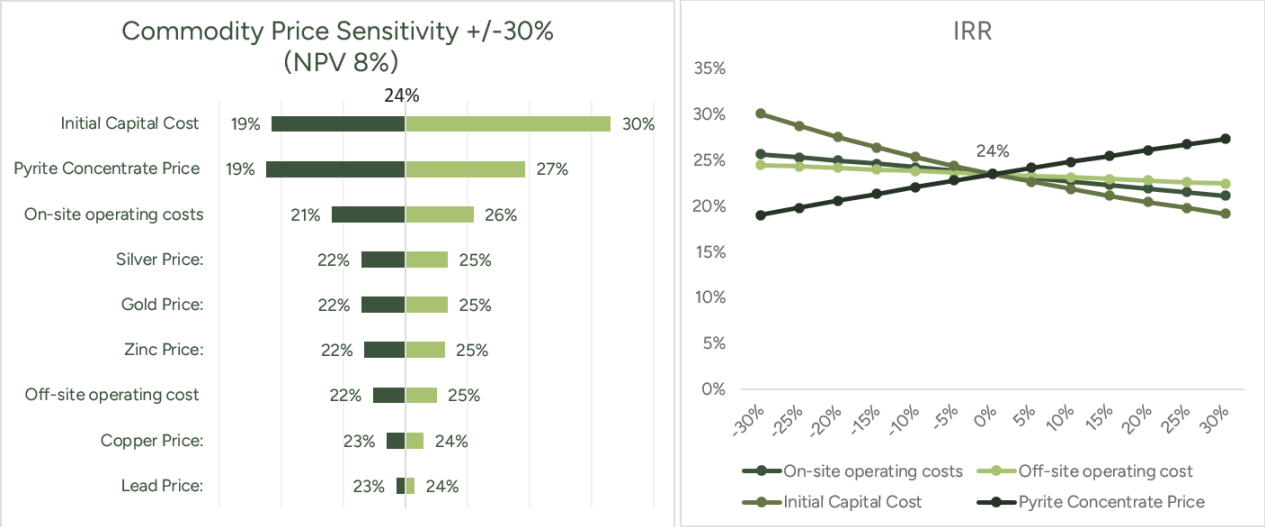


Figure 22-10: After-Tax Sensitivity Analysis (IRR)



23.0 Adjacent Properties

SLR is not aware of any adjacent or nearby mineral occurrences, exploration projects, or mining activities.

24.0 Other Relevant Data and Information

24.1 Post-Flotation Process (PFP)

The Post-Flotation Process (PFP) was investigated as a potential opportunity to recover additional value from the gold and silver remaining in the flotation tailings following production of the base-metal concentrates. A range of process configurations and feed options was evaluated through scoping-level testwork and technical trade-off studies. Based on the information currently available, direct sale of the pyrite concentrate has been selected as the preferred option for the PFS, as it provides a simpler route to market with lower technical complexity and development risk. The PFP nevertheless remains a potential future value-enhancement opportunity and is currently at the technology selection and development stage.

The original PFP concept considered treating the final selective-flotation tailings through a combination of thermal oxidation or roasting, acid leaching and the CLEVR® Process developed by Dundee Sustainable Technologies. The objective was to recover gold and silver as doré, together with potential additional copper and zinc recovery from the acid-leaching stage. The CLEVR® Process provides a cyanide-free alternative for precious-metal recovery and operates under acidic conditions.

As the metallurgical programme progressed, the PFP concept was refined to reduce the mass requiring downstream treatment and to concentrate the pyrite-associated gold and silver. The potential PFP feed was therefore progressively evaluated as the complete flotation tailings, a combined bulk Cu-Pb and pyrite concentrate and, ultimately, a dedicated pyrite concentrate. This development work demonstrated that a straightforward rougher-flotation stage could produce a potentially marketable pyrite concentrate while recovering a significant proportion of the gold and silver not reporting to the base-metal concentrates.

Both pyrometallurgical and hydrometallurgical treatment technologies were investigated for the PFP. The alternatives evaluated included thermal oxidation and roasting, as well as the Neutral Albion Leach (NAL) process followed by either the CLEVR® Process or conventional cyanide leaching. These studies provided useful information on the amenability of the material to oxidative treatment and the potential for improving downstream gold and silver recovery.

A trade-off study was subsequently completed comparing two development alternatives: direct sale of the pyrite concentrate without further treatment and on-site treatment through a PFP incorporating NAL and cyanide leaching to produce doré. The direct-sale assumptions used in the trade-off study were based on the pyrite concentrate marketing assessment prepared for Emerita by Claight (2026).

Initial amenability testwork was conducted by Core/Glencore, the owners of the NAL technology, using La Romanera final flotation tailings, which represented the PFP feed contemplated at that stage of process development. As the sulphur content of the flotation tailings and the subsequently produced pyrite concentrate is similar, the results were considered reasonably representative for the scoping-level comparison. The testwork demonstrated the technical potential of oxidative treatment to improve gold and silver extraction and provided a basis for evaluating the NAL-based PFP alternative.

Under the technical, economic and marketing assumptions adopted for the PFS, direct sale of the pyrite concentrate was identified as the preferred development option. This route enables the Project to realise value from the sulphur and associated precious metals while avoiding the additional capital cost, operating complexity and development requirements of an on-site PFP.

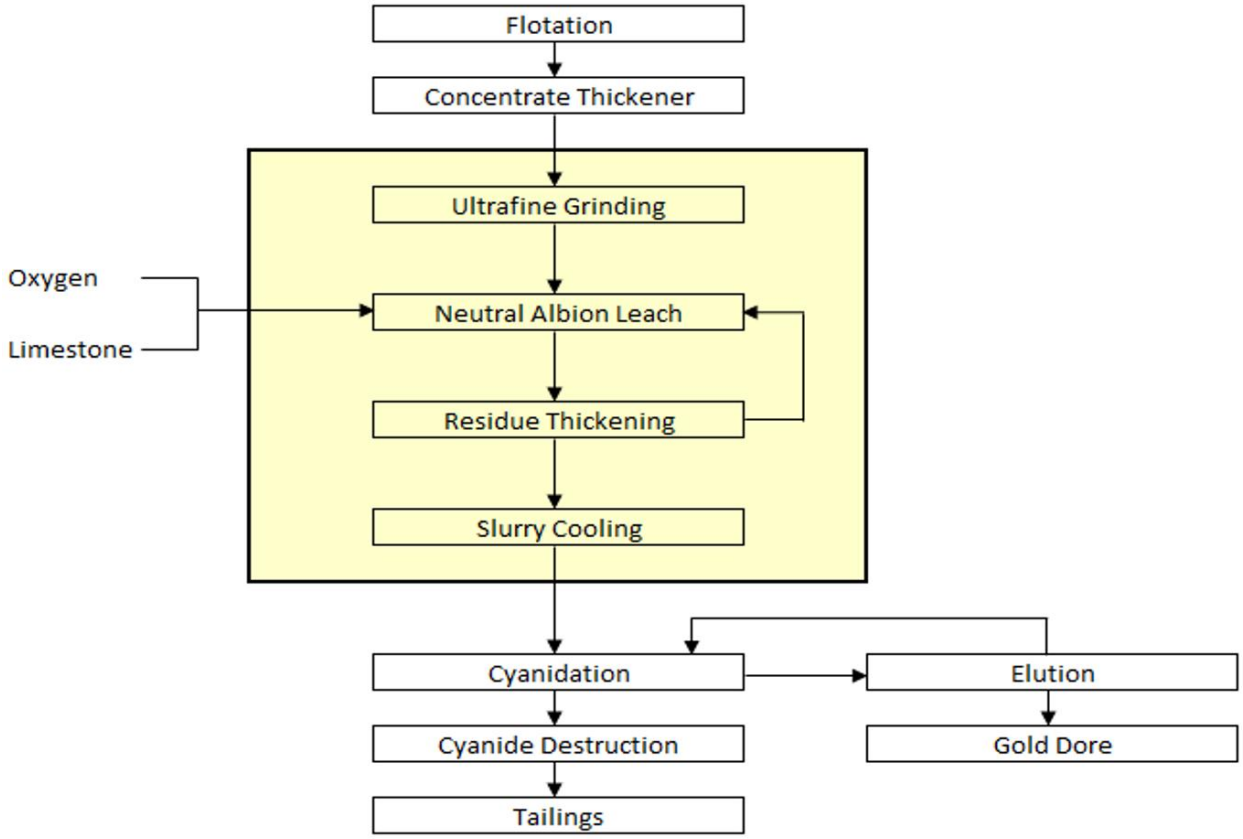
The PFP remains available as a potential future optimisation opportunity, subject to further technology selection, confirmatory testwork and economic assessment.

24.1.1 Neutral Albion Leach Amenability Testwork

The Neutral Albion Leach (NAL) process comprises ultrafine grinding (UFG) of the pyrite-bearing feed, followed by oxidative leaching with oxygen and limestone in specialised reactors. Oxidation of the sulphide minerals liberates the associated gold and silver for subsequent cyanide leaching. Following solid-liquid separation in a counter-current decantation (CCD) circuit, the gold and silver-bearing solution would be treated through a Merrill-Crowe circuit to produce doré, while the final leach residue would be detoxified and filtered for disposal in a dry-stack facility.

Figure 24-1 presents a generalised block flow diagram of the NAL process, a commercial technology owned by Core/Glencore.

Figure 24-1: Neutral Albion Schematic Block Flow Diagram



The principal reaction representing the oxidation and neutralisation of pyrite is:

$$4\ FeS_2 + 15\ O_2 + 18\ H_2O + 8\ CaCO_3 \rightarrow 4\ FeO{\cdot}OH + 8\ CaSO_4{\cdot}2H_2O + 8\ CO_2$$

NAL amenability testwork was conducted by Core between August and December 2025 using a sample of La Romanera final flotation tailings containing 1.26 g/t Au, 34.1 g/t Ag and 44.5% total sulphur, with pyrite representing approximately 74.4% of the sample. The as-received material returned indicative LeachWELL™ gold and silver recoveries of 24.8% and 38.3%, respectively.

Following ultrafine grinding to a P80 of 8 µm, recoveries increased to 37.4% Au and 65.2% Ag, demonstrating an initial recovery benefit from ultrafine grinding alone.

Oxidative leaching was subsequently conducted on the P80 8 µm material for 72 hours under typical NAL conditions at an average temperature of approximately 94°C, an initial slurry density of 8.7% w/w solids and a target pH of 5.5. Kinetic samples were collected after 12, 24, 36 and 48 hours to evaluate the relationship between residence time, sulphide sulphur oxidation (SOx) and indicative gold and silver recovery. The test achieved approximately 100% SOx after 72 hours, with indicative LeachWELL™ recoveries of approximately 94.0% Au and 94.9% Ag.

The results successfully demonstrated the amenability of the La Romanera flotation tailings to treatment by the Albion Process™, increasing indicative gold recovery from 24.8% to approximately 94% and silver recovery from 38.3% to approximately 95%. The kinetic results also showed that a significant proportion of the potential precious-metal recovery was achieved at substantially lower oxidation levels and shorter residence times, providing a positive basis for further process optimisation.

Two operating points were selected for the PFS trade-off assessment: an 80.8% SOx case after 48 hours and a 22.8% SOx case after 12 hours. These cases were selected to assess the balance between precious-metal recovery and the capital and operating requirements associated with residence time, oxygen consumption, limestone consumption and downstream treatment.

Direct sale of the pyrite concentrate remains the selected basis for the current PFS. However, the positive amenability results demonstrate that NAL represents a technically viable potential route for recovering additional value from the pyrite-associated gold and silver. Additional optimisation and confirmatory testwork is currently being undertaken to evaluate the influence of UFG product size (P80), target SOx and residence time on precious-metal recovery. The programme will also determine the specific grinding energy required to achieve the selected P80, providing a more robust basis for future technical and economic assessment of the technology.

24.1.1.1 80.8% SOx Rate

After 48 hours of oxidative leaching, the SOx rate was determined to be 80.8%. LeachWELL™ testing of the oxidised solids returned indicative gold and silver recoveries of 94.1% and 91.0%, respectively. These results demonstrate that high precious-metal recoveries can be achieved without requiring complete sulphide oxidation.

A conventional 48-hour bottle-roll cyanidation test with carbon was subsequently conducted on the final residue produced after 72 hours of NAL treatment at approximately 100% SOx. Based on fire assays of the cyanidation residue, gold and silver recoveries were 81.0% and 98.1%, respectively. As the LeachWELL™ results at 48 hours were comparable with those obtained from the final NAL residue, the bottle-roll results were considered reasonably representative of the 80.8% SOx case for the purposes of the scoping-level trade-off assessment.

The differences between the LeachWELL™ and bottle-roll results likely reflect the different test procedures and analytical bases. For the PFS trade-off assessment, the QP adopted the average of the two result sets, corresponding to estimated recoveries of 87.5% Au and 94.6% Ag for the 80.8% SOx case. The ongoing confirmatory programme will include standardised cyanidation testing at the selected oxidation levels to refine the recovery assumptions and establish a consistent basis for future process design.

The principal parameters developed by Zenito for the 80.8% SOx trade-off case included:

- Limestone addition 2.95t/t SOx.
- Oxygen addition of 87.7 t/h.
- Solids reporting to cyanide leaching of 227.5 t/h.
- Cyanide consumption of 5 kg/t (operating benchmark supplied by Core/Glencore).

For cyanide detoxification following solid-liquid separation, the PFS assessment assumed that 20% of total cyanide would be present as weak-acid-dissociable (WAD) cyanide requiring treatment, with most free cyanide recovered and recycled to the leach circuit. An SMBS consumption of approximately 6 kg to 7 kg per kilogram of WAD cyanide was adopted for the trade-off assessment.

24.1.1.2 22.8% SOx Rate

After 12 hours of oxidative leaching, the SOx rate was determined to be 22.8%. Despite the comparatively low degree of sulphide oxidation, LeachWELL™ testing returned indicative gold and silver recoveries of **82.0% and 68.8%,** respectively. These results demonstrate a strong and rapid metallurgical response and indicate that a substantial proportion of the gold, and a significant proportion of the silver, can be made recoverable at relatively short residence times.

For the scoping-level trade-off assessment, predicted fire-assay-based recoveries were estimated by applying the relationship observed between the LeachWELL™ and bottle-roll results for the higher-oxidation case. The average of the LeachWELL™ and predicted fire-assay values resulted in recoveries of 70.6% Au and 71.5% Ag being adopted for the 22.8% SOx case.

The principal parameters developed by Zenito for this case included:

- Limestone addition 2.95t/t SOx.
- Oxygen addition of 21.8 t/h.
- Solids reporting to cyanide leaching of 132.2 t/h.
- Cyanide consumption of 5 kg/t (operating benchmark).
- SMBS consumption assumed same as for 80.8% SOx rate.

The favourable recovery achieved after only 12 hours indicates that an optimised NAL flowsheet may not require the maximum oxidation level evaluated during the original amenability programme. The additional testwork currently in progress will therefore assess a range of P80 values, SOx targets and residence times to identify the most favourable balance between precious-metal recovery, UFG energy consumption, oxygen demand, limestone consumption and reactor capacity. An IsaMill™ Signature Plot, or equivalent specific-energy test, will be used to quantify the energy required for ultrafine grinding and support a more robust assessment of the potential NAL operating conditions.

24.1.2 Dundee Sustainable Technologies Process Testwork

Dundee Sustainable Technologies Inc. (DST) evaluated an alternative PFP flowsheet combining oxidative thermal treatment, sulfuric-acid washing and the CLEVR® Process. The proposed treatment route was developed to remove sulphur, recover copper and zinc through acid leaching and subsequently recover gold and silver using a cyanide-free oxidative leaching process.

The principal stages of the DST flowsheet comprise:

- Oxidative thermal treatment to oxidize the sulfide minerals and remove sulphur.
- Sulfuric-acid washing of the calcine to solubilize copper and zinc and recovery of copper and zinc from the pregnant leach solution, together with acid regeneration and recycling.
- Gold and silver extraction from the treated calcine using the CLEVR® Process.

The CLEVR® Process is an oxidative chloride-bromide leaching technology operated under acidic conditions. Sodium hypochlorite is used as the oxidant and the oxidation-reduction potential is controlled to maintain the dissolved precious metals in solution. The process provides a cyanide-free alternative for the recovery of gold and silver following thermal oxidation and, where applicable, acid washing.

Three phases of development work were undertaken by DST using representative IBW ROM and flotation-tailings samples supplied by Emerita. The third testwork mandate used ROM material to validate the treatment sequence developed during the earlier mandates and included sample characterization, oxidative thermal treatment, acid washing, CLEVR® leaching and exploratory acid regeneration.

Oxidative thermal treatment was conducted in a laboratory tubular furnace under aerobic conditions. The tests were conducted for two hours over a temperature range of 540°C to 600°C, with an average material temperature of approximately 550°C. The treatment resulted in a mass reduction of 24.6% and achieved 99.1% sulfide removal. These results demonstrate a strong response to oxidative thermal treatment and confirm the effectiveness of this stage for producing a low-sulfide calcine suitable for subsequent hydrometallurgical treatment.

A sulfuric-acid wash was subsequently conducted on the oxidized calcine at 21% w/w solids, an acid concentration of 15% w/w in the liquid phase, a temperature of 70°C to 75°C and a residence time of two hours. Eight individual tests were undertaken.

The acid-washing stage achieved copper and zinc extractions of 76.0% and 77.5%, respectively. Iron extraction was limited to 16.8%, demonstrating favorable selectivity for copper and zinc dissolution relative to iron. These results support the potential recovery of additional base-metal value from the thermally treated material.

Under the standard CLEVR® conditions, the oxidized calcine achieved gold and silver extractions of 76.5% and 71.8%, respectively, after one hour of leaching. The oxidized and acid-washed material achieved gold and silver extractions of 74.1% and 64.7%, respectively, under the standard conditions tested.

The results demonstrate that the thermally oxidized IBW material is amenable to gold and silver recovery through the CLEVR® Process. The comparable gold extraction obtained before and after acid washing also indicates that copper and zinc can be recovered during the acid-washing stage without materially reducing the subsequent gold-extraction response.

The DST program demonstrated the technical potential of an integrated pyrometallurgical and hydrometallurgical treatment route for IBW material. The tests achieved extensive sulfide oxidation, selective extraction of copper and zinc and encouraging gold and silver recoveries through a cyanide-free leaching process. Direct sale of the pyrite concentrate remains the selected basis for the current PFS; however, the DST flowsheet represents a potential future opportunity to recover additional base and precious metals value. Further optimization, continuous or pilot-scale testing, and an integrated techno-economic assessment would be required before considering the technology for future project implementation.

24.1.3 Flowsheet Options - Post-Flotation Processing (PFP)

During the PFS, various processing flowsheet options were considered to evaluate the further processing of the pyrite concentrate on site as part of the Project. The option evaluation study resulted in the specification of pyrite concentrate sales as the preferred project base case scenario, and only this scenario is therefore presented within this PFS report.

The preferred flowsheet decision was made based on currently available input information and assumptions. Should these inputs change following further technical development, metallurgical testwork, and/or changed market conditions, this decision could be revisited in the future.

Further detail of the options considered can be found in Appendix 24-1.

25.0 Interpretation and Conclusions

25.1 Geology and Mineral Resources

- There is a good understanding of the geology and the nature of the polymetallic mineralization at the IBW Project. The drill assays, logging, and geological model have enabled the three-dimensional (3D) delineation of the volcanogenic massive sulphide (VMS) lenses that form the basis of the Mineral Resource estimate.
- The samples used in modelling and estimation are representative of the mineralization and there is no evidence that the drilling or sample collection process has introduced a bias that could materially impact the accuracy and reliability of the results.
- The sample preparation, analysis, and security procedures have been conducted in accordance with acceptable industry standards, and the assay results are suitable for use in Mineral Resource estimation.
- Database verification procedures for the IBW Project comply with industry standards and are adequate for the purposes of Mineral Resource estimation.
- Canadian Institute of Mining, Metallurgy and Petroleum (CIM) Definition Standards for Mineral Resources and Mineral Reserves (CIM (2014) definitions) were used for Mineral Resource classification.
- Mineral Resource reporting is based on a conceptual operating scenario comprising underground mining via long-hole open stoping (LHOS), on-site selective flotation of copper (Cu), lead (Pb), zinc (Zn), and pyrite concentrates, and off-site third-party treatment and refining of the flotation concentrates.
- Mineral Resources are reported within underground reporting shapes using a net smelter return (NSR) cut-off value of US$69.30/t for La Romanera, US$79.20/t for El Cura, and US$85.30/t for La Infanta.
- As of July 17, 2026, the IBW Project Mineral Resources are estimated as follows:
    - Indicated Mineral Resources total approximately 26.1 million tonnes (Mt) grading approximately 2.27% Zn, 1.12% Pb, 0.45% Cu, 52 grams per tonne (g/t) silver (Ag), 1.04 g/t gold (Au), and 33.2% sulphur (S) and containing approximately 593 thousand tonnes (kt) Zn, 292 kt Pb, 116 kt Cu, 43,525 thousand ounces (koz) Ag, 871 koz Au, and 8,663 kt S.
    - Inferred Mineral Resources total approximately 9.9 Mt grading approximately 2.13% Zn, 1.00% Pb, 0.50% Cu, 36 g/t Ag, 0.50 g/t Au, and 22.7% S and containing approximately 212 kt Zn, 100 kt Pb, 50 kt Cu, 11,547 koz Ag, 161 koz Au, and 2,256 kt S.
- This updated Mineral Resource estimate supersedes the previous February 26, 2025, Mineral Resource estimate for the IBW Project. The Indicated Mineral Resources provide a basis for mine planning and Mineral Reserve estimation.
- Emerita has continued to drill at the El Cura and La Infanta deposits through 2026. New results have been reported from 11 drillholes at El Cura and 7 drillholes at La Infanta since the MRE database cut-off date (January 16, 2026). The results show potential to upgrade portions of the current Inferred Resources to Indicated and increase Mineral

Resources through extensions to interpreted higher-grade trends that remain open down-plunge.

25.2 Mining and Mineral Reserves

- Mineral Reserves were estimated in accordance with CIM (2014) definitions. The disclosure of the Mineral Reserve estimate uses the NI 43-101 guidelines and is exclusive of Inferred Mineral Resources.
- As of July 17, 2026, the IBW Project Mineral Reserves are estimated as follows:
  - Probable Mineral Reserves total approximately 23.4 Mt grading approximately 2.30% Zn, 1.13% Pb, 0.45% Cu, 53 g/t Ag, 1.07 g/t Au, and 33.85% S and containing approximately 539 kt Zn, 264 kt Pb, 105 kt Cu, 40,109 koz Ag, 807 koz Au, and 7,938 kt S.
- The mining plan includes underground mining of the La Romanera, El Cura, and La Infanta deposits. The La Romanera and El Cura deposits lie beneath a Natura 2000 protected area, precluding open pit mining. The La Infanta deposit is better suited to underground mining because of the narrow width of the mineralisation, which would result in high open pit stripping ratios.
- The shape, thickness, orientation, and geotechnical competence of the deposits support the use of LHOS mining methods for all deposits, with cemented or uncemented backfill to maximise mining recoveries.
- The La Romanera deposit accounts for approximately 87% of the IBW Project Reserve base and is therefore responsible for sustaining the majority of production over the life-of-mine (LOM). El Cura and La Infanta account for 8% and 5% of the Reserve base, respectively, and are included to support and supplement the process feed from La Romanera at a limited capacity.
- Mining at El Cura and La Infanta is scheduled to occur sequentially, allowing equipment and resources to be shared between operations. Strategically, it is preferable to schedule mining at El Cura prior to La Infanta for operational and economic reasons.
- The mine plan can support a global combined production rate of 1.2 million tonnes per annum (Mtpa), which is sustainable for 18 complete years of full-scale operation before ramping down over the subsequent two years of resource depletion. Prior to achieving full production, approximately 5 years of pre-production development are necessary to develop La Romanera and El Cura to a point where production activities can commence, followed by one year of mine production ramp-up. Opportunities to increase production rates that were not evaluated as part of the PFS may exist.
- Access to the La Romanera and El Cura deposits can be achieved via a 6.3 kilometre (km) decline from a surface portal located outside the Natura 2000 protected area to minimise surface disturbance. Adherence to the mining plan and financial assessment presented herein is reliant on meeting (or exceeding) the development rate assumed for the La Romanera decline to ensure timely access to the deposit.
- Railveyor has been chosen as the primary bulk material handling system for the IBW project and is well-suited to the La Romanera and El Cura deposits, providing a cost-effective material haulage solution along the extensive haulage route.

- Trade-off studies confirmed that a twin decline to the La Romanera deposit (i.e., a service ramp running parallel to a haulage ramp to house the Railveyor) is preferable to a single decline for operational reasons and provides marginal capital cost savings.
- The La Romanera deposit is divided into three mining horizons to facilitate early access to high-value ore and maintain production flexibility. Approximately 85% of the La Romanera deposit lies within Horizons 1 and 2 and can be fed to the Railveyor via an orepass system. The remainder in Horizon 3 requires truck haulage to reach the Railveyor, which can be accommodated by a 5.0 mH x 5.0 mW service ramp. A 30-t truck and a 14-t load-haul-dump (LHD) were considered suitable for the required production intensity.
- The mine workings at La Romanera can be adequately ventilated with a single 5.0 m diameter fresh air raise and a single 4.0 m diameter exhaust raise extending to the surface above the deposit. The approval of the surface ventilation infrastructure within the Natura 2000 area needs to be addressed during permitting, or alternative ventilation measures will need to be investigated, which will likely incur additional cost.

25.3 Mineral Processing

- The process plant is designed to process 1.2 Mtpa using standard comminution and flotation to produce four saleable concentrates: copper, lead, zinc, and pyrite.
- The run of mine (ROM) feed will be delivered to the ROM stockpile by Railveyor. The ore will be blended by using a front-end loader (FEL). This FEL will feed the jaw crusher which will operate approximately 12 hours per day (h/d), 365 days per annum.
- The process plant, including semi-autogenous grinding (SAG) mill, ball mill, and tower mill; four flotation circuits; and dewatering of concentrates and tailings will be operated 24 h/d, 365 days per annum for approximately 8,000 hours per annum.

25.4 Infrastructure

- The proposed infrastructure has been designed to support the planned 1.2 Mtpa underground mining and processing operation through an integrated network of mining, processing, transportation, utilities, and support facilities.
- The site layout efficiently integrates the mine portals, process plant, residue storage facilities, water infrastructure, and site services, minimizing transport distances and supporting operational efficiency.
- Existing access via the HU-5401 road and proximity to regional infrastructure provide suitable logistical support for construction and operations.
- Electrical power requirements are expected to be met through a new grid connection to the Puebla de Guzmán electrical network, with available regional capacity significantly exceeding current Project demand.
- The proposed water supply strategy, supported by water recycling from process and tailings dewatering circuits, provides a practical basis for long-term operational water requirements.
- Mine waste and filtered tailings management strategies prioritize underground reuse, paste backfill, and dry-stack storage, reducing surface storage requirements and supporting responsible environmental management.

- The Project incorporates modern process control, communications, utility, and support infrastructure that are expected to support safe, efficient, and reliable operations throughout the life of mine.
- Further work at Feasibility Study level is required to finalize water permitting, confirm waste management and tailings storage strategies, and complete detailed engineering design.
- Based on the current PFS design, no material infrastructure constraints have been identified that would prevent development of the Project as planned.
- Overall, the proposed infrastructure is considered technically feasible and adequate to support the planned mining and mineral processing operations over the life of the Project.

25.5 Environment

- The Project's existing permit applications are based on the 2023 Project concept and will require updating to reflect the current PFS design.
- Although the Project's designation as being of Strategic Interest by the Government of Andalusia supports coordinated administrative review, the outstanding environmental, mining, water, discharge, restoration, road and municipal approvals, together with land access agreements, remain material to the Project schedule.
- The principal environmental risks relate to water management, historical acid rock drainage and metal contamination, biodiversity and the Natura 2000 designation, mining waste and closure. Although most surface infrastructure is outside the Andévalo Occidental Special Area of Conservation (ZEC), the proposed ventilation infrastructure within the protected area remains a material permitting risk.
- The environmental and social baseline is sufficiently developed to support the PFS, although additional work will be required to support permitting and the next stage of design.
- Local support is generally positive, reflecting anticipated employment and regional development benefits. Maintaining stakeholder confidence will depend on effective management of environmental performance, land access, local livelihoods and expectations regarding Project benefits. Cultural heritage, occupational health and safety, emergency response, rehabilitation and closure requirements have been identified and incorporated at a preliminary level but will require further development as the Project design and permitting process advance.

25.6 Capital and Operating Costs

Initial capital costs are estimated at US$566.7 million, including mine development, process plant and infrastructure, indirect costs, owners' costs, and contingency. Capital expenditure commences in Year -5 to support underground mine development ahead of production. In addition, the Project includes approximately US$279.5 million of sustaining capital and US$12.0 million of closure costs over the life of mine, resulting in total capital expenditure of approximately US$858.2 million.

Life-of-mine on-site operating costs are estimated at approximately US$2.03 billion and comprise mining, processing, G&A, water and waste management, backfill, and progressive rehabilitation, with mining and processing representing the largest cost components. The average operating cost is estimated at US$86.49/t of ore processed.

Off-site and commercial costs are estimated at approximately US$0.89 billion and include TC/RCs, concentrate penalties, transportation, and sales costs. Based on life-of-mine processing of approximately 23.4 Mt.

The capital and operating cost estimates have been developed using a combination of engineering design information, vendor quotations, contractor pricing, benchmark data, and first-principles estimating methodologies. The level of estimate definition is consistent with PFS requirements and reflects the engineering maturity achieved at this stage of project development.

Initial capital, sustaining capital, closure costs, and operating costs have been estimated to an accuracy range considered reasonable for a PFS. Appropriate contingency allowances have been applied to account for the remaining uncertainties associated with engineering development, procurement, construction, and operational assumptions.

The principal areas of cost uncertainty relate to final equipment pricing, construction market conditions, labour costs, power pricing, concentrate transportation costs, treatment and refining charges, and potential penalties associated with concentrate quality specifications. These uncertainties are typical of projects at the PFS stage and are expected to reduce as the Project advances through further engineering and commercial activities.

Overall, the Qualified Persons consider the capital and operating cost estimates to provide a reasonable basis for assessment of the Project’s economic viability and for advancement to the next stage of study.

25.7 Risks

Discipline	Project Element	Risk Name	Risk Description	Consequence(s) Description	Inherent Risk		Mitigation(s)	Mitigated Risk	
					Rating	Qualitative Result		Rating	Qualitative Result
Mining and Mineral Reserves	2.B	Development advance rate	Inability to meet the development advance rates required of the PFS mine schedule	Delays in providing adequate feed to the mill leading to revenue reductions	C3	High	The mine plan is scheduled using benchmarked operational advance rates on an equivalent-meter basis (i.e., advance rates for larger profiles are reduced accordingly). Ore drive development is reduced to 25m/mo to allow provision for grade control activities. Multi-heading Jumbo assignment generally adopts an advance rate of 50m/mo (~3 rounds/week) with isolated priority headings set at 75m/mo at the start of the schedule to prioritise the establishment of early mine infrastructure. Advance rates of 100-150m/mo are applied only to single-face mode development, i.e. blasting can occur at any time during the work shift to maximise face cycle time. Such rates are considered highly sustainable with modern mining equipment under reasonable operating conditions.	D3	Medium
Mining and Mineral Reserves	2.C	Mining production rate	Inability to meet the mine production ramp-up/sustained production rates used for economic modelling	Delays in providing adequate feed to the mill leading to revenue reductions	C4	High	The mining plan includes a detailed representation of the operational stope sequencing, with stope cycle delays derived from first principles and benchmarked assumptions. Mine access and operational interactions for all stopes have been planned in detail and simulated using industry-standard mine-planning software. Mine scheduling delays are introduced for contingency, and to provide adequate time for geological definition to assist production forecasting. 1.2 Mtpa is also considered a reasonably conservative production target, given the potential of the Romanera deposit.	D3	Medium
Mining and Mineral Reserves	2.D	Decline development rate	Delays in surface decline development.	Delayed ramp-up. Reduction in project NPV.	C3	High	Conduct hydro/Geotech drilling along decline profile to confirm drifting conditions. Allocate the decline development phase to a mining contractor, with mining rates embedded into contractual obligations.	D3	Medium
Mining and Mineral Reserves	2.H	Production rate	Increase mining production rate from 1.2Mtpa	Higher mining throughputs leading to increased project revenues and potentially higher NPVs.	C3	High	Conduct a trade-off considering increased cash flows versus higher project CAPEX.	C2	Medium
Mining and Mineral Reserves	2.K	Rockfill / CRF reliance and mine productivity	Residual rockfill and CRF requirements must be integrated with the mine production schedule. The all-CRF Infanta sensitivity would require approximately 0.744 Mt CRF and results in approximately 0.72 Mt LOM deficit of fill-grade rock/aggregate.	Additional haulage and placement fleet, level congestion, competition between ore and fill transport, ventilation demand and CRF cycle times may reduce mine productivity and increase OPEX. External rock/aggregate may also be required.	C4	High	Retain paste fill at Infanta in the selected PFS basis; use CRF only where specifically required by Mining; explicitly test residual rockfill/CRF demand against haulage capacity, level access, fleet and ventilation in the integrated Mining schedule.	D3	Medium
Infrastructure and Tailings	4.	ATEM peak occupancy and waste routing	The current Mining schedule indicates that peak surface mine-waste inventory may exceed the existing 0.844 Mm3 ATEM capacity if all surface-routed waste is passed through ATEM.	Potential approximately 0.30 Mm3 temporary capacity shortfall, additional rehandling/haulage, additional temporary storage requirement and associated water-management, permitting and operating-cost impacts.	C3	High	Integrate the annual waste-routing and fill schedule; maximise direct-to-underground routing and accelerated ATEM drawdown where practicable. Retain approximately 1.20 Mm3 temporary-capacity sensitivity if schedule reconciliation demonstrates that the existing ATEM cannot maintain the required operating inventory.	C2	Medium

Discipline	Project Element	Risk Name	Risk Description	Consequence(s) Description	Inherent Risk		Mitigation(s)	Mitigated Risk	
					Rating	Qualitative Result		Rating	Qualitative Result
Environment, Social and Permitting	5.A	Natura 2000 (Andévalo Occidental Special Area of Conservation)	Construction of ventilation shafts within the Natura 2000 protected area; Discharge of water into watercourses in Natura 2000.	Delays in implementation schedule; Permit rejection or delays (const. and op.); Stakeholder / NGO objections; Costly or challenging offset commitments; Loss, degradation or fragmentation of habitat.	B4	Very High	Provision of a biodiversity offset (plus Habitats Regulation Assessment); Avoid and minimise impacts to biodiversity and water resources; Engage with relevant stakeholders (regulatory bodies) on permitting process and requirements within Natura 2000 sites; Engage with other relevant stakeholders (communities, NGOs); Restoration of habitats (habitats of community interest etc); Critical Habitat Assessment.	C3	High
Environment, Social and Permitting	5.B	Land acquisition and access	Acquisition or leasing of land required for all surface infrastructure, access and biodiversity offsets.	Unknown cost associated with purchasing or leasing land; Unrealistic expectations by landowners; Extended lease or purchase negotiations.	A3	High	Engage with landowners; Understand landowner expectations; Independent evaluation. Audit for impact on physical structures.	C2	Medium
Environment, Social and Permitting	5.C	Land acquisition and livelihood	Disruption to land-based livelihoods due to land access restrictions and land acquisition for surface infrastructure and offsets.	Loss of trust, grievances, could cause delays in permitting, could impact land purchases and lease agreements.	A3	High	Stakeholder Engagement Plan; Social baseline; Livelihood Restoration Plan if required; Grievance Mechanism.	C2	Medium
Environment, Social and Permitting	5.E	Surface water resources	Contamination of surface water from the Project (acid mine drainage, metal leaching, runoff of chemicals, sedimentation); Impacts to Andévalo Reservoir and watercourses within the Project area.	Degradation of existing surface water resources; Community or landowner grievances; Legal and reputational consequences.	B4	Very High	Undertake seasonal baseline surface water sampling; Undertake surface and groundwater impact assessment; Confirm water treatment plant, wastewater treatment plant and discharge limits (quality and quantity); Consider re-use / recycling of water within water management plan (e.g. within processing plant).	C3	High
Environment, Social and Permitting	5.F	Dust, traffic, noise and vibration	Increased dust, traffic, noise and vibration during construction and operation.	Existing land users (grazing, agriculture, other land uses); Impacts to biodiversity (flora, fauna, habitat degradation and fragmentation); Degradation of surface water resources (contamination, sedimentation); Land owner grievances.	A3	High	Air quality, noise and traffic studies (baseline and IA); Traffic management plan.	C2	Medium
Environment, Social and Permitting	5.G	Project related influx	Reduced health and wellbeing due to increased demand on services, increase in anti-social behaviour, price inflation.	Perceived expectation on EMERITA to fund any new infrastructure or expansion of existing infrastructure.	B3	High	Understanding of current capacity of existing infrastructure in the region and needs, Stakeholder engagement, local employment and management of influx.	C2	Medium
Environment, Social and Permitting	5.H	Unmet expectations	Unmet expectations of communities in terms of project benefits and jobs.	Loss in trust (increase in grievances), increase of the evaluation price of land purchases and leases, delay of permitting process.	B3	High	Stakeholder Engagement Plan; Local employment and local upskilling.	C2	Medium
Environment, Social and Permitting	5.I	Obtaining critical permits	Not obtaining all critical permits required to commence construction and operation (water supply and discharge, land access, temporary water diversion, exploitation etc).	Rejection or delays to permit approval process due to current challenging regulatory approach in Spain and national and local regulatory bodies; Permits granted with unrealistic or unreasonable expectations.	B4	Very High	Develop a permitting strategy; Benchmark permitting timeframes; Engage with stakeholders; Undertake all required specialist studies (inc. ESIA); Stakeholder Engagement Plan.	D3	Medium
Processing and Metallurgy	3.H	Concentrate Quality	Impact of penalty elements on concentrates quality.	Concentrates may be subject to further penalty deductions affecting revenues.	D4	High	Conduct variability sample testwork programme to confirm impact of penalty elements such as mercury and initiate discussions with potential smelters and traders.	D3	Medium
Infrastructure and Tailings	4.A	Performance of the backfill	Proposed backfill solution has not been tested	Backfill system may not meet the requirements of the project and may lead to increase in CAPEX and OPEX.	C4	High	Undertake the required testwork to increase confidence in the backfill solution	D3	Medium

26.0 Recommendations

26.1 Geology and Mineral Resources

1 Optimise exploration and resource development drilling by focusing on the following tasks:

   a) Infill drilling underground reporting shapes containing Inferred Mineral Resources, to upgrade material to Indicated, prioritising areas according to mineable stope optimiser (MSO) stope NSR value.

   b) Testing open extensions to underground reporting shapes at depth and along strike.

2 Consider targeted close-spaced drilling in areas that are expected to have the greatest impact on early LOM production.

3 Confirm primary sulphide mineralogy of stopes at the base of the weathering profile, via diagnostic leach assays for pulps from key drillhole intersections. Consider targeted infill drilling to delineate the top of fresh rock contact, proximal to any stopes that are early in the LOM schedule.

4 Following variability testwork on the PFS flotation flowsheet, develop a geometallurgical model of metallurgical recovery, payability, and hardness variability to refine block NSR calculations and support future technical evaluations.

5 Expand duplicate sample types to include a coarse duplicate submitted to the primary laboratory and a pulp duplicate submitted to an umpire laboratory.

6 Refine IBW Project certified reference materials (CRMs) to include polymetallic sulphide materials with higher sulphur grades for La Romanera and El Cura, and higher copper grades for El Cura.

7 Complete chlorine (Cl) and fluorine (F) assays for a selection of pulps, to assess whether geochemical proxies can be developed to model these potential penalty elements.

26.2 Mining and Mineral Reserves

1 Conduct studies to increase mine production rates in support of higher mill throughput. Higher mining rates provide economies of scale and reduce unit costs, potentially leading to an increased Mineral Reserve base. If the increased cash flows from the elevated throughput can be supported by the higher CAPEX requirements, improvements in project net present value (NPV) may also result.

2 Undertake survey work on the historical mine workings close to the surface. Based on current information, the workings pose a negligible impact on the PFS mine design and Reserve estimate (only appearing to cross the delineated stope set at the very top of the La Romanera deposit at the end of the mine life). However, it is recommended that their position be accurately confirmed to eliminate doubt and remove any potential future safety hazard.

3 Following detailed metallurgical testwork, investigate mine scheduling strategies to optimise a ROM blend that stabilises ore feed grades and material types to the mill.

4 Following the acquisition of geotechnical and hydrogeological data, conduct a detailed analysis to define advance rates for the twin decline to La Romanera. The analysis should delineate areas of poor ground and/or expected water infiltration and advance rates should be reduced accordingly. Conversely, areas of favourable conditions should be identified to produce a comprehensive, qualified estimate of expected arrival time at the mining deposit.

5 Conduct material handling studies to guide detailed material pass design with the following objectives:

   a) Confirm current material pass geometries via rock fragmentation analysis (empirical or otherwise).

   b) Inform detailed material pass design, placement, and layout.

   c) Provide geotechnical assessments for support recommendations and rehabilitation requirements.

   d) Provide optimal strategies for material management (number of material passes, separate ore and waste passes, material blending opportunities, etc.).

6 Investigate more efficient and cost-effective ways to return waste material to the underground for backfill (possibly using Railveyor), including longer-term, higher-capacity underground waste storage, such as designated waste storage stopes.

7 Undertake studies to optimise the backfill material balance to address the limited quantities of tailings for pastefill and the limited volumes of waste rock for rockfill/ cemented rockfill (CRF), such as flexing the primary/secondary stope width ratio and reviewing the backfill barricade construction method (shotcreted fill fence versus shotcreted rock bumper).

8 Optimise ventilation raise diameters for CAPEX reduction and energy saving potential, including trade-off studies on the application of ventilation on demand (VOD) systems and the adoption of battery electric vehicles (BEVs).

9 Conduct a mine water balance study following hydrogeological testwork and update the mine dewatering and water management system design accordingly.

10 Investigate the technical and regulatory means of placing primary ventilation fans underground at La Romanera. The current design assumes they are on the surface within the Natura 2000 area, which will need to be addressed during permitting. Underground installation would be preferable for reducing surface disturbance and noise; however, it may require local mine regulatory approval.

11 Expand the permit boundary slightly south of the La Infanta deposit (approximately 50 m). The current southern boundary restricts space for the decline and footwall infrastructure, compromising stand-off distances to production areas. This limited space may lead to sub-optimal mine design once a detailed geotechnical appraisal is completed.

12 Re-evaluate the material handling system for La Infanta. The current assumption of using Railveyor implies a relatively high CAPEX per tonne, with minimal LOM OPEX savings. Truck haulage may offer a more flexible option at lower CAPEX.

26.3 Mineral Processing

1 Address gaps in current metallurgical knowledge in the next stage of study through the following testwork:

   a) Variability sample testwork on a suitable number of samples from all three deposits (ore hardness and metallurgical response variability, generation of recovery head grade relationships).

   b) Additional locked cycle tests (LCTs) on new composite samples for each deposit representing the lower head grades as defined in the PFS Mineral Resource estimate.

   c) Additional flotation testwork for pyrite concentrate production (only limited open circuit testwork has been conducted to date).

   d) Thickening and filtration testwork on bulk samples of the concentrates and final tailings (only benchmark data used to date).

2 Further define the impact of the deleterious elements based on the future variability sample testwork and conduct discussions with relevant traders and smelters.

3 Explore reducing the comminution equipment costs by replacing the combination of SAG + ball mill by a combined high pressure grinding roll (HPGR) + stirred media detritor (SMD) as the ore properties may be favourable for an HPGR circuit. An HPGR supplier has indicated a substantial reduction in OPEX by reducing milling energy consumption by approximately 31% compared to the currently specified equipment. This results in a carbon emissions reduction of 44% based on energy savings and no requirement for steel grinding media. Testwork could be carried out at supplier's facilities to verify/de-risk the proposed circuit.

4 Evaluate the final mining production schedule grades against the process plant design head grades, as well as any process plant bottlenecks, especially potential bottlenecks due to higher grade ROM feed in the flotation and filtering circuits.

26.4 Infrastructure

1 Secure Grid Power Connection

   a) Obtain a new grid connection via the Red Eléctrica de España network from the Puebla de Guzmán substation.

   b) Finalise a power supply agreement with a regional power provider.

   c) Maintain and convert the existing 30 megawatt (MW) reservation into a long-term supply arrangement sufficient for project demand.

   d) Ensure power infrastructure is sized for approximately 26.8 MW installed load and annual consumption of approximately 153 GWh, including mining and processing infrastructure.

2 Advance Water Permitting

   a) Progress permitting for water abstraction from the Andévalo Reservoir system with the Confederación Hidrográfica del Guadiana which, if granted, will be effective in 2028.

b) Obtain the required planning reserve, environmental approvals (AAU), mining concession, and water concession before water rights can be granted.

c) Secure the proposed water allocation of approximately 1.51 hm^3 per year for project start-up requirements.

d) Continue negotiations with the agricultural community for interim water access from the Guadiana River until the expected granting of the Industrial Water Permit allocation in January 2028.

3 Develop Site Access and Logistics Infrastructure

a) Construct the main access road network and internal 9 m wide haul and service roads linking the following surface infrastructure:

i. Process plant

ii. Mine portals

iii. Tailings dewatering area

iv. Mine waste storage facilities (*Acopio Temporal de Estériles de Mina*, ATEM)

v. Integrated Process Residue Storage Facility (*Instalación de Pasta Seca,* IPS)

vi. Administrative facilities

b) Plan for regional traffic impacts associated with concentrate transport, particularly pyrite shipments, which will account for the majority of truck movements.

4 Establish Site Operational Facilities

a) Construct administration offices, laboratory facilities, personnel buildings, and maintenance workshops early in project development

b) Provide fully equipped analytical laboratories supporting:

i. Process control

ii. Environmental monitoring

iii. Fire assay

iv. Metallurgical analysis

5 Implement Water Management Infrastructure

a) Develop the raw water, treated water, and stormwater pond systems.

b) Implement process water recycling systems to reduce long-term freshwater demand.

6 Install drainage and stormwater attenuation facilities to manage runoff from the process plant area.

7 Support High Production Logistics

8 Design transport and loading systems to accommodate annual production of:

a) Pyrite concentrate

b) Copper concentrate

c) Lead concentrate

d) Zinc concentrate

9 Ensure road and port logistics can support approximately 104 concentrate truck movements per day.

26.5 Environment

1 Reconcile the current PFS design, mine schedule, infrastructure layout, process mass balance, waste storage requirements, and backfill strategy with the exploitation permit, AAU, Restoration Plan, and supporting permit applications.

2 Maintain an integrated permit register and programme covering the AAU, exploitation permit, water concessions, discharge permit, restoration approval, road and municipal licences, containment pond classification, and land access agreements.

3 Complete an ESIA and ESMP aligned with applicable Spanish and EU requirements and relevant good international industry practice, incorporating all Project phases and updated specialist studies.

4 Complete seasonal surface water monitoring, groundwater baseline studies, hydrological and hydrogeological investigations, and an updated dynamic water balance before construction.

5 Finalise the integrated water management design, including clean and contact water separation, treatment requirements, discharge criteria, water reuse, storage capacity, and monitoring provisions.

6 Complete geochemical and geotechnical testwork for waste rock, tailings, and treatment residues, and confirm the design and capacity of the ATEM, IPS, and backfill systems.

7 Update the biodiversity assessment for the current Project footprint and complete the assessment of effects on the Andévalo Occidental Special Area of Conservation, including mitigation, restoration, monitoring, and any required compensation measures.

8 Complete design-specific air quality and noise assessments, supported by representative baseline monitoring and clearly defined sensitive receptors.

9 Establish contaminated soil, erosion, sediment, topsoil, spill-prevention, and rehabilitation management procedures before earthworks commence.

10 Complete the social baseline and impact assessment, including land tenure, livelihoods, vulnerable groups, community infrastructure, worker influx, community health and safety, human rights, traffic, employment, and procurement.

11 Prepare and implement a Stakeholder Engagement Plan, community grievance mechanism, land access strategy, local employment and procurement plan, and transparent communications programme.

12 Complete a traffic and road safety assessment for the HU-5401 and other affected roads, incorporating construction and operational traffic, community access, and emergency-response requirements.

13 Protect identified archaeological sites, provide archaeological monitoring of relevant earthworks, and implement a formal chance-find procedure and worker training programme.

14 Finalise Project-specific occupational health and safety, emergency response, security, contractor-management, and workforce training arrangements before construction.

15 Prepare a Project-wide Non-Mining Waste Management Plan addressing waste classification, segregation, storage, transport, disposal, traceability, and contractor responsibilities.

16 Update the closure and restoration plan to reflect the current PFS design, actual waste inventories, final landforms, progressive rehabilitation, post-closure monitoring, and long-term water management requirements.

17 Update closure costs and financial provisions and include adequate budgets for permitting baseline studies, mitigation, monitoring, stakeholder engagement, rehabilitation, and post-closure obligations.

26.6 Capital and Operating Costs

1 Focus on reducing key areas of cost uncertainty prior to completion of subsequent study phases.

2 Complete further design development to improve estimate accuracy and support progression toward a Feasibility Study level estimate.

3 Continue engagement with vendors to obtain budget quotations for major equipment and construction contracts to further refine capital cost assumptions and reduce contingency requirements.

4 Use ongoing metallurgical testwork results to better define blended concentrate specifications and support more robust estimates of treatment charges, refining charges, and deleterious element penalties.

5 Advance discussions with potential smelter and concentrate purchasers to validate the treatment, refining, transportation, and penalty assumptions adopted in the PFS.

6 Refine closure and rehabilitation planning in consultation with the relevant regulatory authorities, with updates to closure cost estimates and rehabilitation schedules incorporated into future project analyses.

27.0 References

Almodóvar, G.R., Yesares, L., Sáez, R., Toscano, M., González, F. and Pons, J.M. 2019. Massive sulphide ores in the Iberian Pyrite Belt: Mineralogical and textural evolution, Minerals, 9(11), 653.

Amnesty International. 2025. Spain 2024/25, available at Amnesty International Spain Report (accessed October 8, 2026).

Azor, A. 2023. Preliminary Report on the Visit to the Romanera Polymetallic Sulphide Project, Andévalo, Huelva, unpublished report.

Barrie, C.T. and Hannington, M.D. 1999. Classification of volcanic-associated massive sulphide deposits based on host-rock composition, in Volcanic-associated Massive Sulphide Deposits: Processes and Examples in Modern and Ancient Settings, edited by C.T. Barrie and M.D. Hannington, Reviews in Economic Geology, Vol. 8, Littleton, Colorado: Society of Economic Geologists, pp. 1-11.

Capes, G. and Milne, D. 2008. A compilation of dilution graph data for open stope hangingwall design, in Proceedings of the First Southern Hemisphere International Rock Mechanics Symposium (SHIRMS 2008), Perth: Australian Centre for Geomechanics, pp. 149-162.

Canadian Institute of Mining, Metallurgy and Petroleum (CIM). 2014. CIM Definition Standards for Mineral Resources and Mineral Reserves. Adopted by CIM Council on May 10, 2014.

Carter, T.G. 2014. Guidelines for Use of the Scaled Span Method for Surface Crown Pillar Stability Assessment.

Claight. 2026. Global Pyrite Concentrate Market Study, Strategic Market Intelligence, June 2026. Prepared for Emerita Resources Corporation.

Conde, C. 2016. Geology and Hydrothermal Evolution of Massive Sulphides of the Iberian Pyrite Belt, Spain. Ph.D. Dissertation, Universidad de Salamanca, Salamanca, Spain.

Cuadri y de la Corte, S.C.P. 2025. Commercial Options for the Emerita IBW Polymetallic Ores, prepared for Emerita Resources Corporation. June 15, 2025.

Datamine. 2026. Datamine Studio UG 4.2 Online Help Files. Available at Datamine Studio UG Documentation (accessed October 8, 2026).

Decree 18/2015. 2015. Approving the Regulations Governing the Regime Applicable to Contaminated Soils. Junta de Andalucía. January 27, 2015.

Deere, D.U. and Deere, D.W. 1988. The Rock Quality Designation (RQD) Index in Practice, in Rock Classification Systems for Engineering Purposes. ASTM STP 984, pp. 91-101.

Donaire, T., Pascual, E., Sáez, R. and Toscano, M. 2020. Facies architecture and palaeoenvironmental constraints of subaqueous felsic volcanism in the Iberian Pyrite Belt: The Paymogo Volcano-Sedimentary Alignment, Journal of Volcanology and Geothermal Research, 405, 107045.

Donaire, T., Sáez, R. and Pascual, E. 1998. Geology and magmatic evolution of the Paymogo volcanic axis, Geogaceta, 24.

Emerita Resources Corporation. 2024. Emerita Achieves Strong Metallurgical Results from Ongoing Testing Program at La Romanera Deposit Including 64.3% Gold Recovery, news release, December 20, 2024. Available at emeritaresources.com.

Emerita Resources Corporation. 2025. Self-Protection Plan for the Development Project for the Processing of a Concession Derived from Research Permit "La Romanera" No. 15,029, proprietary internal report.

Emerita Resources Corporation. 2026a. Corporate Presentation, Developing High Grade Polymetallic Deposits in Spain. PowerPoint presentation. (July 2026). Available at emeritaresources.com.

Emerita Resources Corporation. 2026b. *Emerita Announces That the IBW Project Has Commenced the Public Consultation Phase for the Exploitation Permit Application*, news release, May 13, 2026. Available at emeritaresources.com.

Emerita Resources Corporation. 2026c. Emerita Intersects 3.9 Metres Grading 3.8% Copper, 0.9% Lead, 1.6% Zinc, 2.81 g/t Gold and 71.26 g/t Silver at El Cura Deposit. Public Consultation Submission Phase of the AAU (Autorizacion Ambiental Unificada) Now Complete, news release, July 9, 2026. Available at emeritaresources.com.

Emerita Resources Corporation. 2026d. Emerita Intersects 7.2m Grading 1.0% Copper, 4.0% Lead, 7.5% Zinc, 0.13 g/t Gold and 83.32 g/t Silver at La Infanta Deposit; Deep Hole Extends the La Infanta Deposit Limits at Depth, news release, June 2, 2026. Available at emeritaresources.com.

Emerita Resources Corporation. 2026e. Emerita Intersects 9.2m Grading 1.4% Copper, 0.4% Lead, 1.3% Zinc, 0.41 g/t Gold and 21.48 g/t Silver at El Cura, news release, February 9, 2026. Available at es.emerita...ources.com.

Emerita Resources Corporation. 2026f. Emerita Intersects High Grade Zone of 4.9m Containing Mineralization Grading 3.5% Copper, 1.95 g/t Gold and 95.63 g/t Silver at El Cura, news release, April 22, 2026. Available at emeritaresources.com.

Emerita Resources Corporation. Ongoing. Internal Social Baseline and Risk Analysis for the Andévalo Region, proprietary internal report.

Equator Principles Association. 2020. The Equator Principles, available at Equator Principles (accessed October 8, 2026).

ESGold Corp. 2025. ESGold Reports over 90.9% Gold Recovery Using Dundee Sustainable Technologies Non-Cyanide CLEVR Process™ on Montauban Project Stockpiled Tailings, news release.

European Bank for Reconstruction and Development. 2019. Environmental and Social Policy Performance Requirements, available at EBRD Performance Requirements (accessed October 8, 2026).

Franklin, J.M., Gibson, H.L., Jonasson, I.R. and Galley, A.G. 2005. Volcanogenic massive sulphide deposits, in Economic Geology 100th Anniversary Volume, 1905-2005, edited by J.W. Hedenquist, J.F.H. Thompson, R.J. Goldfarb and J.P. Richards, Littleton, Colorado: Society of Economic Geologists, pp. 523-560.

Leistel, J.M., Marcoux, E., Thieblemont, D., Quesada, C., Sánchez, A., Ruiz de Almodovar, G., Pascual, E. and Sáez, R. 1998. The volcanic-hosted massive sulphide deposits of the Iberian Pyrite Belt, Mineralium Deposita, 33, pp. 2-30.

Quesada, C. 1991. Geological constraints on the Paleozoic tectonic evolution of tectonostratigraphic terranes in the Iberian Massif, Tectonophysics, 185(3-4), pp. 225-245.

Quesada, C. 1998. A reappraisal of the structure of the Spanish segment of the Iberian Pyrite Belt, Mineralium Deposita, 33, pp. 31-44.

Schermerhorn, L.J.G. 1971. An outline of the stratigraphy of the Iberian Pyrite Belt, Boletín Geológico y Minero, 82, pp. 239-268.

Tornos, F. 2006. Environment of formation and styles of volcanogenic massive sulphides: The Iberian Pyrite Belt, Ore Geology Reviews, 28(3), pp. 259-307.

Tornos, F. and Heinrich, C.A. 2008. Shale basins, sulfur-deficient ore brines, and the formation of exhalative base metal deposits, Chemical Geology, 247, pp. 195-207.

Wardell Armstrong International. 2023. NI 43-101 Technical Report on the La Romanera and La Infanta Polymetallic Deposits, Spain, prepared for Emerita Resources Corporation. Filed on SEDAR+.

Wardell Armstrong International. 2025. NI 43-101 Technical Report on the Iberian Belt West Project, Spain, prepared for Emerita Resources Corporation. Filed on SEDAR+.

World Bank Group. 2007a. Environmental, Health and Safety Guidelines for Mining, available at World Bank Mining EHS Guidelines (accessed October 8, 2026).

World Bank Group. 2007b. Environmental, Health and Safety General Guidelines, available at World Bank General EHS Guidelines (accessed October 8, 2026).

28.0 Date and Signature Date

This report titled “NI 43-101 Technical Report for the Iberian Belt West Project, Spain” with an effective date of October 8, 2026, was prepared and signed by the following authors:

(Signed & Sealed) *Name*

Dated at London UK
October 14, 2026

Frank Browning, MSc, FGS, CGeol

(Signed & Sealed) *Name*

Dated at London UK
October 14, 2026

James W.G. Turner, MCSM, MIMMM, CEng

(Signed & Sealed) *Name*

Dated at London UK
October 14, 2026

Christopher Penna, CEng

(Signed & Sealed) *Name*

Dated at London UK
October 14, 2026

Liam Johnson, RPEQ, MAusIMM CP (Geotech)

(Signed & Sealed) *Name*

Dated at London UK
October 14, 2026

Christopher Paul Stinton, CEng IMMM

(Signed & Sealed) *Name*

Dated at London UK
October 14, 2026

Arturo Gutierrez del Olmo, PhD. (Mining), Eur Ing, MIMMM

(Signed & Sealed) *Name*

Dated at London UK
October 14, 2026

Alison Brianna Allen, BSc, MSc, CEnv, FIMMM, MISEP

(Signed & Sealed) *Name*

Dated at London UK
October 14, 2026

Veronika Luneva, MAussIMMM, MSc, IMC (CFA UK Level 4)

29.0 Certificate of Qualified Person

29.1 Frank Browning

I, Frank Browning, MSc, FGS, CGeol, as an author of this report entitled “NI 43-101 Technical Report for the Iberian Belt West Project, Spain” with an effective date of October 8, 2026, prepared for Emerita Resources, do hereby certify that:

1. I am Principal Resource Geologist with SLR Consulting Limited, of 3rd Floor, Summit House, 12 Red Lion Square, London, UK, WC1R 4QH.
2. I am a graduate of University College London in 2011 with a MSci in Earth Sciences, Camborne School of Mines in 2016, with a MSc in Mining Geology, and Edith Cowan University in 2019, with a PGCert in Geostatistics.
3. I am a registered member of the Geological Society of London as a Fellow and Chartered Geologist (Reg.# 1031973). I have worked as a geologist for a total of 15 years since my graduation. My relevant experience for the purpose of the Technical Report is:
    - Estimation of Mineral Resources for a number of polymetallic sulphide deposits, including within the Iberian Pyrite Belt.
    - Preparation of NI 43-101 Technical Reports.
    - Performance as an exploration, development and resource geologist for international mining companies and consulting firms.
4. I have read the definition of "qualified person" set out in National Instrument 43-101 (NI 43-101) and certify that by reason of my education, affiliation with a professional association (as defined in NI 43-101) and past relevant work experience, I fulfill the requirements to be a "qualified person" for the purposes of NI 43-101.
5. I visited the Iberian Belt West Project on January 21, 2026; May 3-5, 2023; March 16, 2023; and October 25-27, 2022.
6. I am responsible for Sections 1.1.1.1, 1.1.2.1,1.3.1-6,1.3.8, 4-12, 14, 25.1, and 26.1 of the Technical Report.
7. I am independent of the Issuer applying the test set out in Section 1.5 of NI 43-101.
8. My prior involvement with the property that is the subject of the Technical Report, includes being a named qualified person of previous Technical Reports with effective dates of April 30, 2025, and May 4, 2023.
9. I have read NI 43-101, and the Technical Report has been prepared in compliance with NI 43-101 and Form 43-101F1.
10. At the effective date of the Technical Report, to the best of my knowledge, information, and belief, the Section Nos. in the Technical Report for which I am responsible contain all scientific and technical information that is required to be disclosed to make the Technical Report not misleading.

Dated 09th day of October 2026

(Signed) *Frank Browning*

Frank Browning, MSc, FGS, CGeol

29.2 James W.G. Turner

I, James W.G. Turner, MCSM, MIMMM, CEng, as an author of this report entitled “NI 43-101 Technical Report for the Iberian Belt West Project, Spain” with an effective date of October 8, 2026 prepared for Emerita Resources, do hereby certify that:

1. I am Technical Director, Mineral Processing with SLR Consulting Limited, of 3rd Floor, Summit House, 12 Red Lion Square, London, UK, WC1R 4QH.
2. I am a graduate of Camborne School of Mines in 1984 with a BSc (Hons) in Minerals Engineering, and in 1993, with a MSc in Minerals Engineering.
3. I am a registered member of the Institute of Materials, Minerals & Mining (Reg.# 0046967) and a Chartered Engineer with the Engineering Council. I have worked as a mineral processing engineer for a total of 43 years since my graduation, circa 30 years in world-wide site-based operations and circa 13 years as a consultant with three international consultancy companies. I have extensive experience specialising in gold CIP/CIL/heap/dump leaching and base metal gravity and flotation processes, including laboratory testwork, process design and operations.
4. I have read the definition of "qualified person" set out in National Instrument 43-101 (NI 43-101) and certify that by reason of my education, affiliation with a professional association (as defined in NI 43-101) and past relevant work experience, I fulfill the requirements to be a "qualified person" for the purposes of NI 43-101.
5. I have not visited the Iberian Belt West Project.
6. I am responsible for Sections 1.1.1.3, 1.1.2.3,1.3.7, 13, 24, 25.3 and 26.3 of the Technical Report.
7. I am independent of the Issuer applying the test set out in Section 1.5 of NI 43-101.
8. My prior involvement with the property that is the subject of the Technical Report, includes being a named qualified person of a previous Technical Report with an effective date of April 30, 2025.
9. I have read NI 43-101, and the Technical Report has been prepared in compliance with NI 43-101 and Form 43-101F1.
10. At the effective date of the Technical Report, to the best of my knowledge, information, and belief, the Section Nos. in the Technical Report for which I am responsible contain all scientific and technical information that is required to be disclosed to make the Technical Report not misleading.

Dated 9th day of October 2026

(Signed) *James W.G. Turner*

James W.G. Turner, MCSM, MIMMM, CEng

29.3 Christopher Penna

I, Christopher Penna, CEng, as an author of this report entitled “NI 43-101 Technical Report for the Iberian Belt West Project, Spain” with an effective date of October 8, 2026 prepared for Emerita Resources, do hereby certify that:

1. I am Associate Director, Mining & Mineral Resources, with SLR Consulting Limited, of 3rd Floor, Summit House, 12 Red Lion Square, London, UK, WC1R 4QH.
2. I am a graduate of University of Exeter, Camborne School of Mines, UK, in 2009 with a MEng (Hons) in Mining Engineering.
3. I am a registered member of the Institute of Materials, Minerals & Mining (Reg.# 0454050) and a Chartered Engineer with the Engineering Council holding QMR status. I have worked as a mining engineer for a total of 17 years since my graduation. My relevant experience for the purpose of the Technical Report is:
    - 17 years of hard rock mining experience across operations and consulting, predominantly gained from underground mining environments.
    - Mineral Reserves estimations for comparable mining projects, and the preparation of mining sections for pre-feasibility studies, feasibility studies, JORC and NI 43-101 Technical Report.
    - Over 10 years of operational experience in transverse and longitudinal Long Hole Open Stoping.
4. I have read the definition of "qualified person" set out in National Instrument 43-101 (NI 43-101) and certify that by reason of my education, affiliation with a professional association (as defined in NI 43-101) and past relevant work experience, I fulfill the requirements to be a "qualified person" for the purposes of NI 43-101.
5. I visited the Iberian Belt West Project on January 20-22, 2026.
6. I am responsible for Sections 1.1.1.2, 1.1.2.2, 1.3.9, 1.3.10, 15, 16.2-5, 16.7-9, , 25.2, and 26.2 of the Technical Report.
7. I am independent of the Issuer applying the test set out in Section 1.5 of NI 43-101.
8. I have had no prior involvement with the property that is the subject of the Technical Report.
9. I have read NI 43-101, and the Technical Report has been prepared in compliance with NI 43-101 and Form 43-101F1.
10. At the effective date of the Technical Report, to the best of my knowledge, information, and belief, the Section Nos. in the Technical Report for which I am responsible contain all scientific and technical information that is required to be disclosed to make the Technical Report not misleading.

Dated 9th day of October 2026

(Signed) *Christopher Penna*

Christopher Penna, CEng

29.4 Liam Johnson

I, Liam Johnson, RPEQ, MAusIMM CP (Geotech), as an author of this report entitled “NI 43-101 Technical Report for the Iberian Belt West Project, Spain” with an effective date of October 8, 2026 prepared for Emerita Resources, do hereby certify that:

1. I am Senior Consultant – Rock Mechanics with SLR Consulting Limited, of 3rd Floor, Summit House, 12 Red Lion Square, London, UK, WC1R 4QH.
2. I am a graduate of University of New South Wales, Australia, in 2018 with a Masters of Mine Geotechnical Engineering with Excellence in 2018, and a Bachelor Of Civil Engineering/Mining Engineering (Hon. 1) in 2011.
3. I am registered as a Professional Engineer in Queensland, Australia (Reg. 19364) and a Chartered professional with AusIMM (Reg. 305428). I have worked as a Geotechnical and mining engineer for a total of 15 years since my graduation. My relevant experience for the purpose of the Technical Report is:
    - 15 years of underground hard rock geotechnical engineering experience across operations and consulting.
    - Preparation of geotechnical sections for pre-feasibility studies, feasibility studies, JORC and NI 43-101 report.
    - Operational and consulting experience in multiple underground mining methods including transverse and longitudinal longhole open stoping, cut and fill and development mining.
4. I have read the definition of "qualified person" set out in National Instrument 43-101 (NI 43-101) and certify that by reason of my education, affiliation with a professional association (as defined in NI 43-101) and past relevant work experience, I fulfill the requirements to be a "qualified person" for the purposes of NI 43-101.
5. I did not visit the Iberian Belt West Project.
6. I am responsible for Section 16.1 of the Technical Report.
7. I am independent of the Issuer applying the test set out in Section 1.5 of NI 43-101.
8. I have had no prior involvement with the property that is the subject of the Technical Report.
9. I have read NI 43-101, and the Technical Report has been prepared in compliance with NI 43-101 and Form 43-101F1.
10. At the effective date of the Technical Report, to the best of my knowledge, information, and belief, the Technical Report contains/Section Nos. in the Technical Report for which I am responsible contain all scientific and technical information that is required to be disclosed to make the Technical Report not misleading.

Dated 09th day of October 2026

(Signed) *Liam Alexander Johnson*

Liam Alexander Johnson, RPEQ, MAusIMM CP (Geotech)

29.5 Christopher Paul Stinton

I, Christopher Paul Stinton CEng IMMM, as an author of this report entitled “NI 43-101 Technical Report for the Iberian Belt West Project, Spain” with an effective date of October 8, 2026, prepared for Emerita Resources, do hereby certify that:

1. I am Principal Process Engineer with Zenito Limited, of 27 Old Gloucester Street, London, WC1N 3AX, United Kingdom.
2. I am a graduate of Birmingham University in with a Minerals Engineering, B.Sc.
3. I am registered as a Chartered Engineer in the United Kingdom (Reg.No. 369197). I have worked as a process engineer for a total of 45 years since my graduation. My relevant experience for the purpose of the Technical Report is:
    - I have 45 years’ experience ranging from testwork management through to process plant management in gold and base metal processing plants.
    - Have acted as the process engineer of projects in numerous countries in Europe, Asia and Africa.
    - QP projects in Europe, Asia, Australia and North America.
    - Have been responsible for the process design of base metal flotation plants.
4. I have read the definition of "qualified person" set out in National Instrument 43-101 (NI 43-101) and certify that by reason of my education, affiliation with a professional association (as defined in NI 43-101) and past relevant work experience, I fulfill the requirements to be a "qualified person" for the purposes of NI 43-101.
5. I have not visited the Iberian Belt West Project site.
6. I am responsible for overall preparation for Sections 1.1.1.4, 1.1.2.4, 1.3.12, 17, 18 (Excluding 18.5), 25.4, and 26.4 of the Technical Report.
7. I am independent of the Issuer applying the test set out in Section 1.5 of NI 43-101.
8. I have had no prior involvement with the property that is the subject of the Technical Report.
9. I have read NI 43-101, and the Technical Report has been prepared in compliance with NI 43-101 and Form 43-101F1.
10. At the effective date of the Technical Report, to the best of my knowledge, information, and belief, the Section Nos. 17 and 18 in the Technical Report for which I am responsible contain all scientific and technical information that is required to be disclosed to make the Technical Report not misleading.

Dated 9th day of October 2026

(Signed) *Christopher Paul Stinton*

Christopher Paul Stinton, CEng IMMM

29.6 Arturo Gutierrez del Olmo

I, Arturo Gutierrez del Olmo, PhD (Mining), Eur Ing, MIMMM, as an author of this report entitled “NI 43-101 Technical Report for the Iberian Belt West Project, Spain” with an effective date of October 8, 2026 prepared for Emerita Resources, do hereby certify that:

1. I am Technical Director, Mine Waste Engineering with SLR Consulting Limited, of 3rd Floor, Summit House, 12 Red Lion Square, London, UK, WC1R 4QH.
2. I am a graduate of Madrid School of Mines, Polytechnic University, Spain, with a MS Eng/PhD in Mining Engineering in 1992, and of Aberyswith University of Wales, UK, with a MSc in Environmental Assessment, Health and Safety at Work in 1998.
3. I hold the professional designation European Engineer (Eur Ing, 025980ES) and my national registration (02171) was granted May 7, 2001. I am a Member of the Institute of Materials, Minerals and Mining (MIMMM). I have approximately 30 years of professional experience since my graduation in mining engineering, with particular specialisation in mine waste management, tailings engineering, and underground mine backfill systems. My relevant professional experience for the purposes of this Technical Report includes:
    - Mine waste and tailings management studies, engineering design, and technical assessments for underground mining projects.
    - Development and evaluation of mine waste and tailings storage, handling, disposal, and underground reuse strategies.
    - Engineering assessment of cemented paste backfill, rockfill, and cemented rockfill systems, including material balances, processing and distribution requirements, and integration with underground mining operations.
    - Preparation and technical review of mine waste, tailings, and backfill engineering studies at scoping, Pre-Feasibility and Feasibility Study levels.
    - Development and review of associated capital and operating cost estimates, technical risk assessments, and implementation requirements.
4. I have read the definition of "qualified person" set out in National Instrument 43-101 (NI 43-101) and certify that by reason of my education, affiliation with a professional association (as defined in NI 43-101) and past relevant work experience, I fulfill the requirements to be a "qualified person" for the purposes of NI 43-101.
5. I have not personally inspected the Iberian Belt West Project property in connection with the preparation of this Technical Report.
6. I am responsible for Sections 16.6 and 18.5 of the Technical Report.
7. I am independent of the Issuer applying the test set out in Section 1.5 of NI 43-101.
8. My prior involvement with the Iberian Belt West Project comprises the preparation and technical development of the mine waste, tailings management and underground backfill components of the current Pre-Feasibility Study, including associated engineering evaluations and cost estimates.
9. I have read NI 43-101, and the Technical Report has been prepared in compliance with NI 43-101 and Form 43-101F1.

10. At the effective date of the Technical Report, to the best of my knowledge, information and belief, the portions of the Technical Report for which I am responsible contain all scientific and technical information required to be disclosed to make those portions of the Technical Report not misleading.

Dated 9th day of October 2026

(Signed) *Arturo Gutierrez del Olmo*

Arturo Gutierrez del Olmo, PhD. (Mining), Eur Ing, MIMMM

29.7 Alison Brianna Allen

I, Alison Brianna Allen, BSc, MSc, CEnv, FIMMM, MISEP, as an author of this report entitled “NI 43-101 Technical Report for the Iberian Belt West Project, Spain” with an effective date of October 8, 2026 prepared for Emerita Resources, do hereby certify that:

1. I am EU Regional Sector Lead – Environmental and Social Impact Assessments with SLR Consulting Limited, of Baldhu House, Wheal Jane Earth Science Park, Baldhu, Truro, UK, TR3 6EH
2. I graduated with a Bachelor of Science Degree in Natural Sciences from the University of East Anglia (UK) in 2001 and a Master of Science Degree in Mining Environmental Management from the Camborne School of Mines (UK) in 2008.
3. I am a Fellow of the Institute of Materials, Minerals and Mining (Membership No. 474370), Chartered Environmentalist of the Institute of Sustainability and Environmental Professionals (Membership No. 0013685), and Full Member of the Institute of Ecology and Environmental Management. I have practiced my profession continuously for the last 25 years in a variety of countries and geological environments and have prepared Environmental and Social Chapters and Impact Assessments for gold and base metals for more than 5 years. My relevant experience for the purpose of the Technical Report is:
    - ESIA Management
    - Due Diligence and Project Reviews
    - Contract Management
    - Extractives Sector E&S Management Planning
    - Environmental Risk Management
    - Environmental and social audits
    - Technical Reporting to International Mining Codes
    - ESG Reporting
4. I have read the definition of "qualified person" set out in National Instrument 43-101 (NI 43-101) and certify that by reason of my education, affiliation with a professional association (as defined in NI 43-101) and past relevant work experience, I fulfill the requirements to be a "qualified person" for the purposes of NI 43-101.
5. I am responsible for Sections 1.1.1.5, 1.1.2.5, 1.3.14, 20, 25.5, and 26.5 of the Technical Report.
6. I am independent of the Issuer applying the test set out in Section 1.5 of NI 43-101.
7. I have had no prior involvement with the property that is the subject of the Technical Report.
8. I have read NI 43-101, and the Technical Report has been prepared in compliance with NI 43-101 and Form 43-101F1.

9. At the effective date of the Technical Report, to the best of my knowledge, information, and belief, the Technical Report contains/Section Nos. in the Technical Report for which I am responsible contain all scientific and technical information that is required to be disclosed to make the Technical Report not misleading.

Dated 9th day of October, 2026

(Signed) *Alison Brianna Allen*

Alison Brianna Allen, BSc, MSc, CEnv, FIMMM, MISEP

29.8 Veronika Luneva

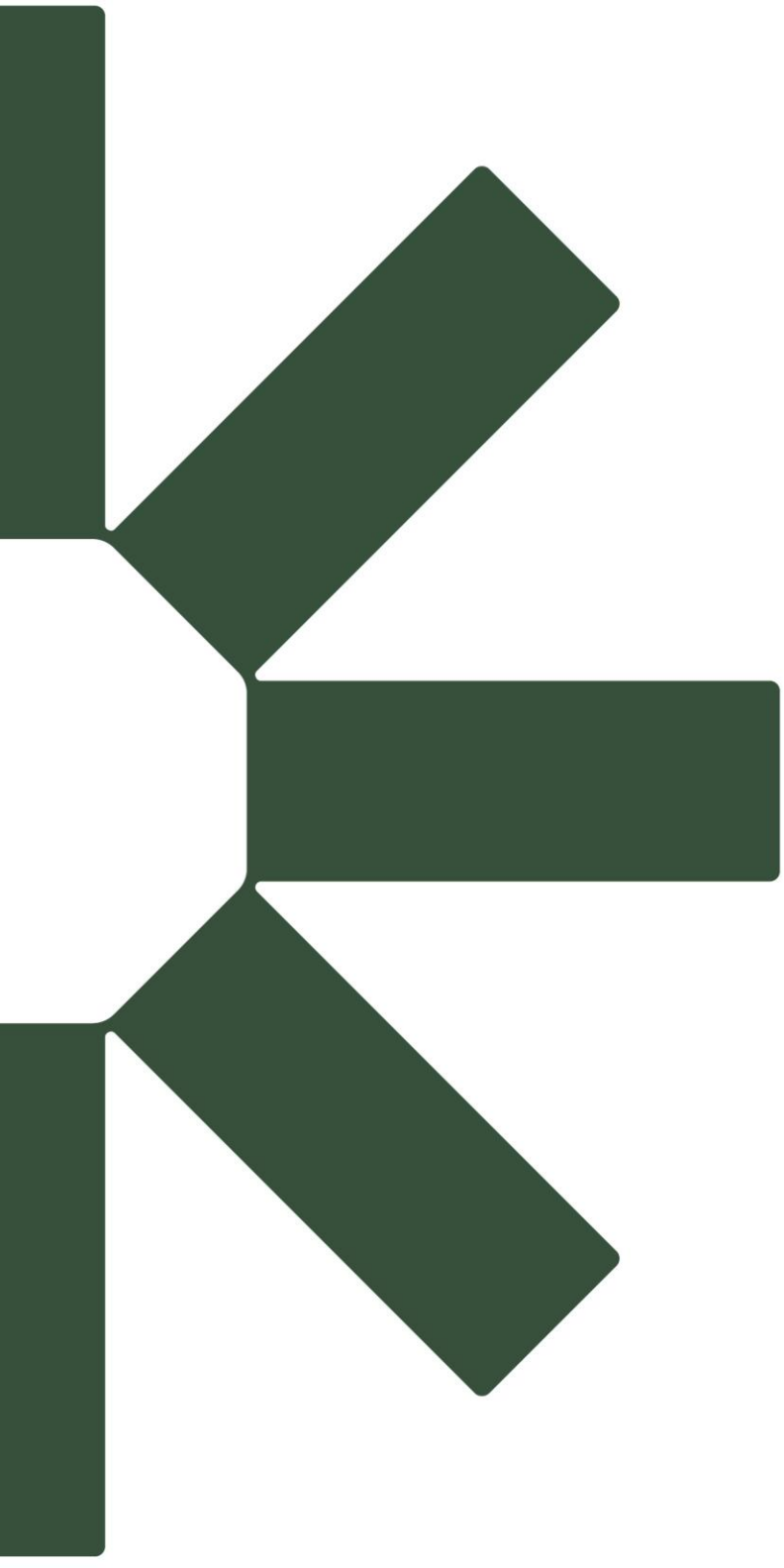
I, Veronika Luneva, MAusIMM, MSc, IMC (CFA UK Level 4), as an author of this report entitled "NI 43-101 Technical Report for the Iberian Belt West Project, Spain" with an effective date of October 8, 2026 prepared for Emerita Resources, do hereby certify that:

1. I am Mining Finance Specialist with SLR Consulting Limited, of 3rd Floor, Summit House, 12 Red Lion Square, London, UK, WC1R 4QH.
2. I am a graduate of National Research Nuclear University, Russia, and was awarded a Specialist Diploma in Managerial Economics in 2009, which is equivalent to an MSc degree.
3. I am registered as a Member of the Australasian Institute of Mining and Metallurgy (MAusIMM). I have worked in the mining industry for a total of 15 years since 2011. My relevant experience for the purpose of the Technical Report is:
    - Mineral asset valuation,
    - Technical-financial modelling,
    - Economic analysis and assessment of mining projects across a range of commodities and jurisdictions.
4. I have read the definition of "qualified person" set out in National Instrument 43-101 (NI 43-101) and certify that by reason of my education, affiliation with a professional association (as defined in NI 43-101) and past relevant work experience, I fulfill the requirements to be a "qualified person" for the purposes of NI 43-101.
5. I have not visited the Iberian Belt West Project.
6. I am responsible for overall preparation of Sections 1.1.1.6, 1.1.2.6, 1.3.15; 21, 22, 25.6, and 26.6 of the Technical Report.
7. I am independent of the Issuer applying the test set out in Section 1.5 of NI 43-101.
8. I have had no prior involvement with the property that is the subject of the Technical Report.
9. I have read NI 43-101, and the Technical Report has been prepared in compliance with NI 43-101 and Form 43-101F1.
10. At the effective date of the Technical Report, to the best of my knowledge, information and belief, the portions of the Technical Report for which I am responsible contain all scientific and technical information required to be disclosed to make those portions of the Technical Report not misleading.

Dated 9th day of October 2026

(Signed) *Veronika Luneva*

Veronika Luneva, MAusIMM, MSc, IMC (CFA UK Level 4)



Making Sustainability Happen